Millinewton Force Sensor (MFS) Based on Low Temperature Co-fired Ceramic (LTCC)

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Thick-film Group

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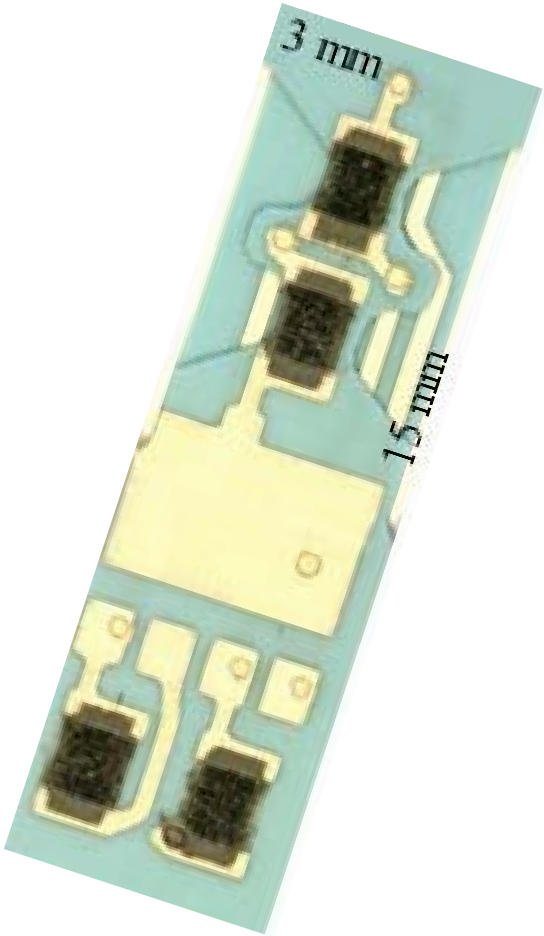
PURPOSE OF THE PRESENTATION

- Fabrication of the MFS using LTCC technology: design concept
- Measuring and comparing electrical performance with previously-fabricated MFS sensors
- Improving sensitivity by reducing LTCC materials incompatibility



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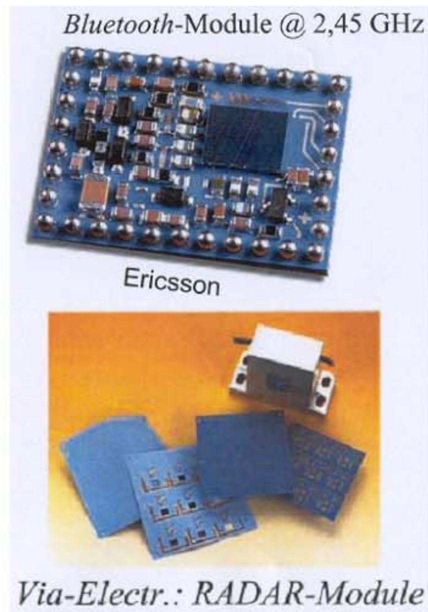
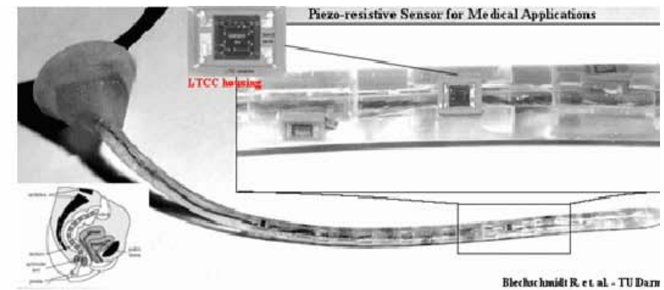
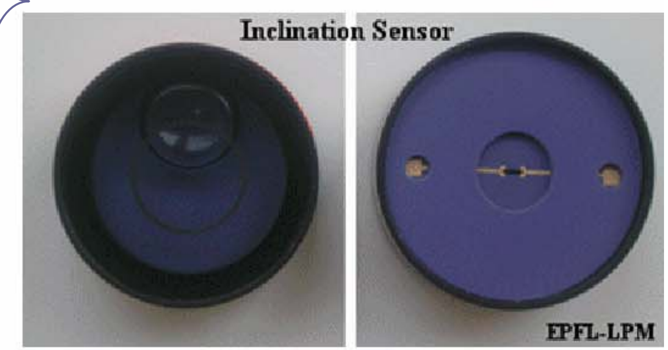
Application areas of LTCC technology have diversified







High – frequency applications (superior dielectric properties) → Sensors, micro – fluidics (ease of 3-D fabrication)

OUTLINE OF THIS PRESENTATION

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LTCC Technology for sensor applications

Design and fabrication of a novel MFS sensor

Electrical performance and comparison

→Introduction

→Advantages

→Challenges

→Theory

→Design concept and fabrication of novel MFS

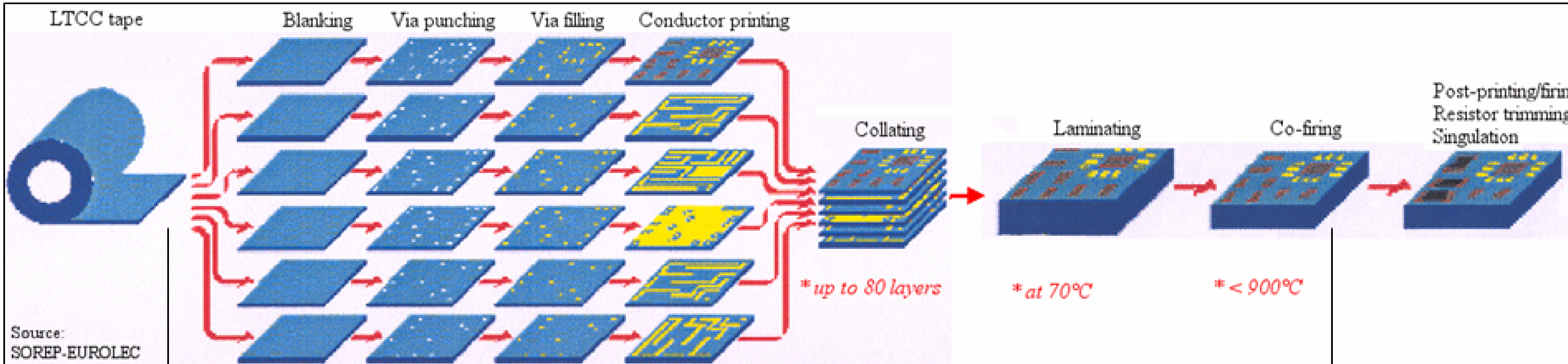
→Materials compatibility

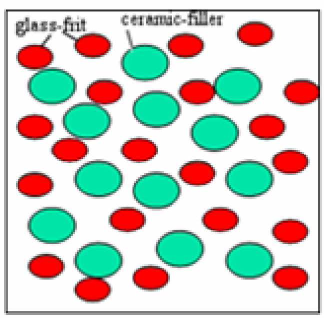
→Results

→Comparing electrical performance

→Conclusions and next steps

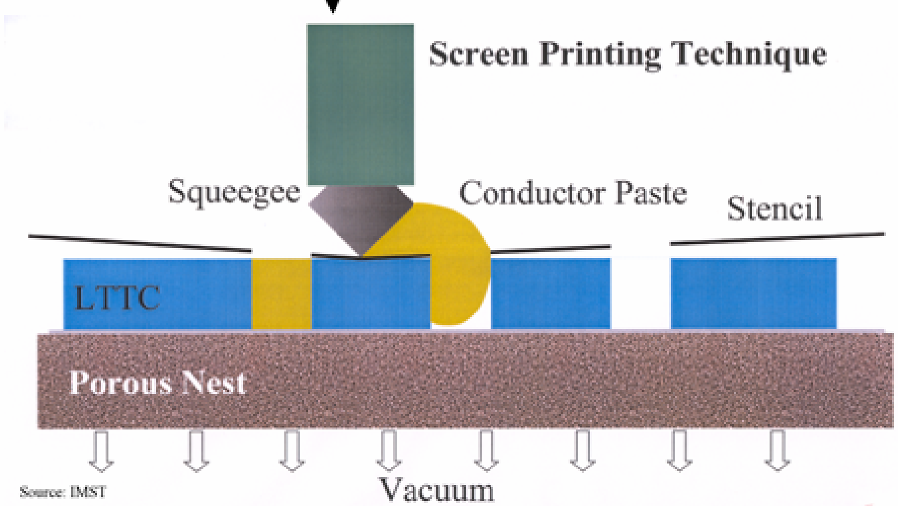
INTRODUCTION: LTCC MATERIALS SYSTEM

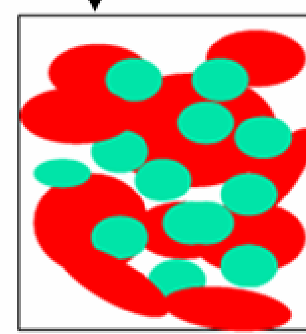




Glass-frit: low firing T
Filler: dimensional stability

... blended in organic-vehicle & cast on mylar sheets





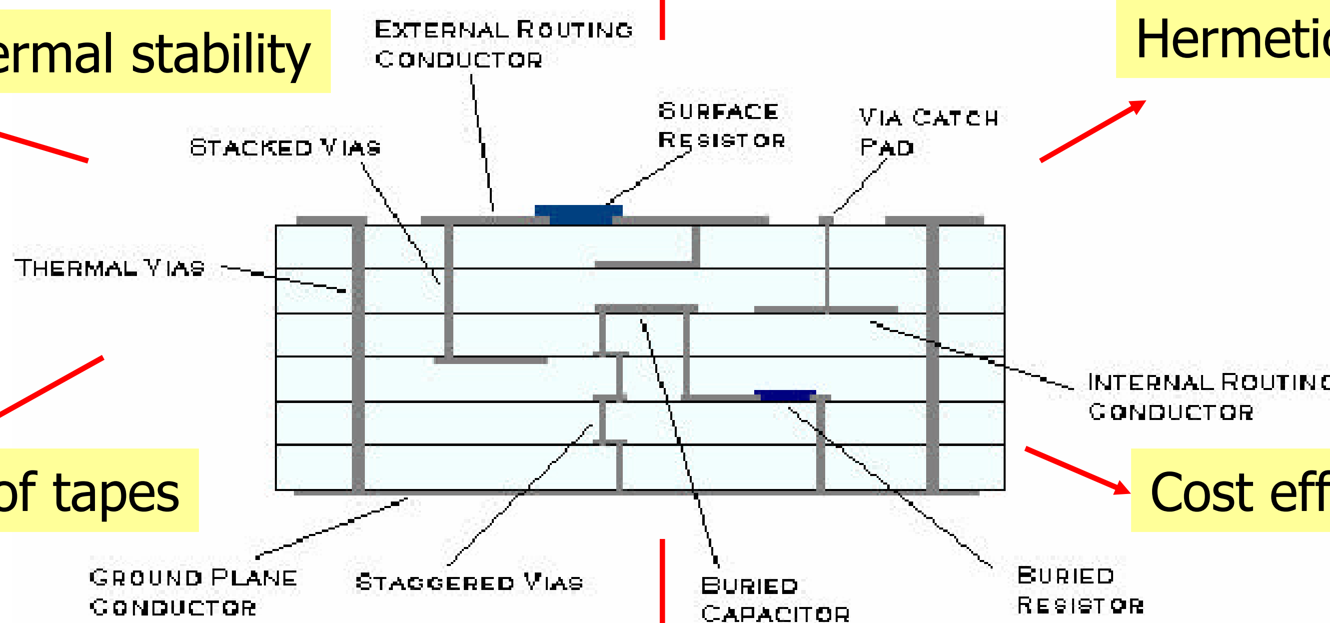
Glass wetting and ceramic rearrangement occur

ADVANTAGES OF LTCC FOR SENSOR APPLICATIONS

High density packaging

Chemical / thermal stability

Hermeticity



Machinability of tapes

Cost effective

Mechanical and electrical functions in one system

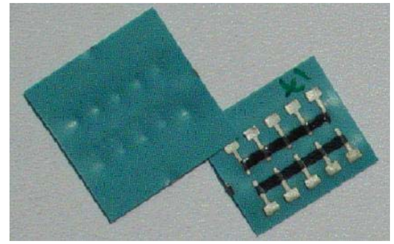
CHALLANGES

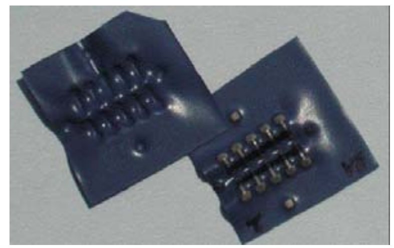
1. Physical Issues

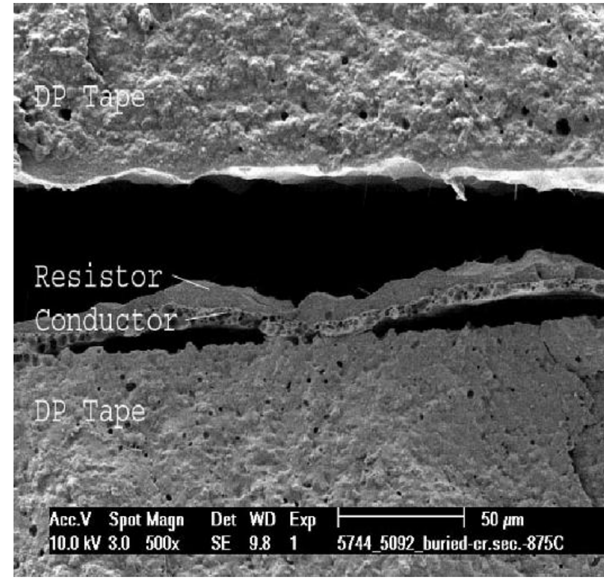
→ differential shrinkage

→ degassing

→ delamination



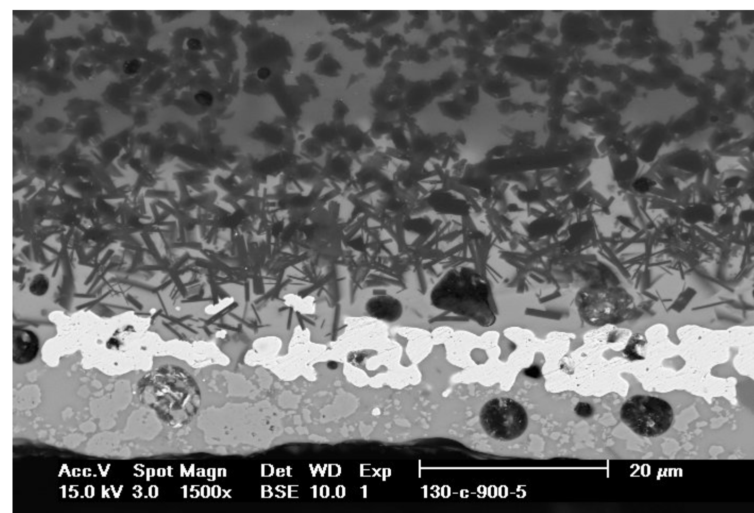




2. Chemical Issues

→ Interaction of components

→ Oxidizing /reducing conditions



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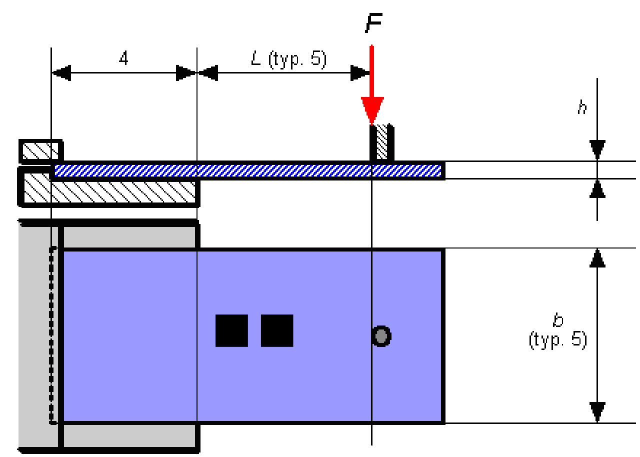
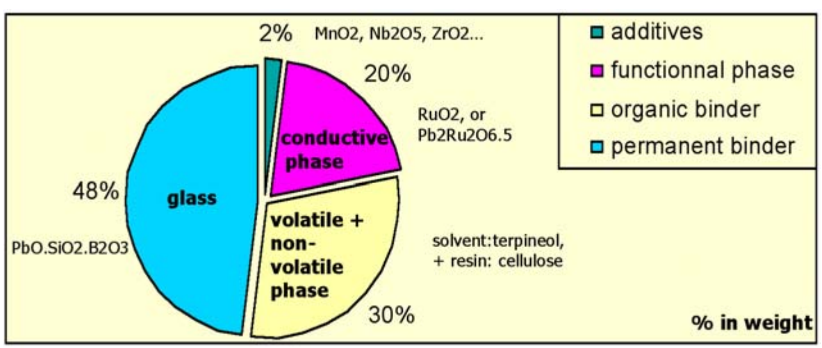
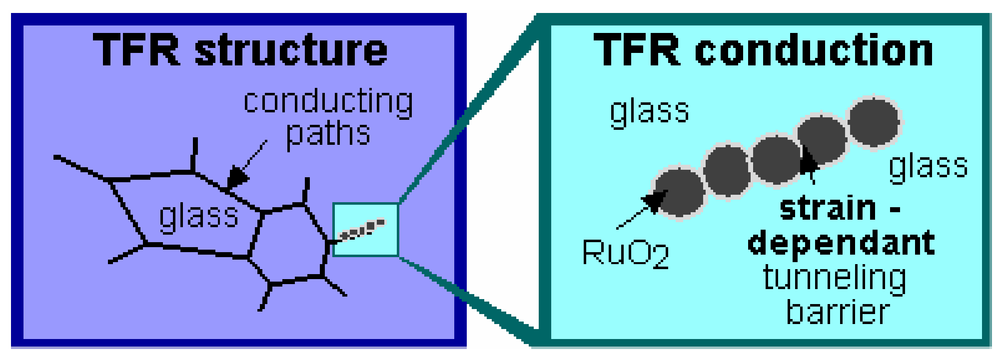
PRINCIPLE : Piezoresistivity ⟷ Force inducing resistance change

« Piezoresistor, a special-type thick-film resistor (TFR) paste, is screen-printed on the beam of the sensor »



μ-SCALE :





THEORY II
OBJECTIVE / SELECTION OF BEAM MATERIAL

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Maximum signal, $(\Delta R/R)$ ⟷ $Signal = \varepsilon_{max} G_f$

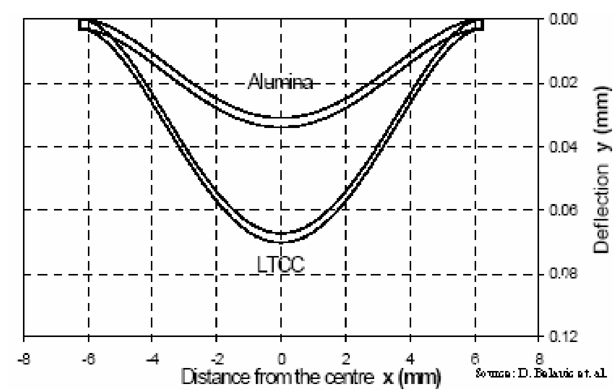
Maximum strain, ε $(\Delta l/l)$ ⟷ $E = \sigma / \varepsilon$

Maximum stress, σ_{max} ⟷ $\sigma_{max} = (6FL) / (bh^2)$

$$\varepsilon = (6FL) / (bh^2)E$$

Alumina or LTCC ?

Properties	Kyocera A-476 Al_2O_3 (96%)	DuPont LTCC 951 (fired)
Elastic modulus (GPa)	330	152
Flexural strength (MPa)	310	320
Available thickness (mm)	0.25-1.00	0.04-0.21



$$\varepsilon_{LTCC} / \varepsilon_{Al2O3} = (h^2_{Al2O3} E_{Al2O3}) / (h^2_{LTCC} E_{LTCC})$$

$\varepsilon_{LTCC} / \varepsilon_{Al2O3}$ → up to ~70 times theoretically

EXPERIMENTAL I DESIGN and PROCESSING

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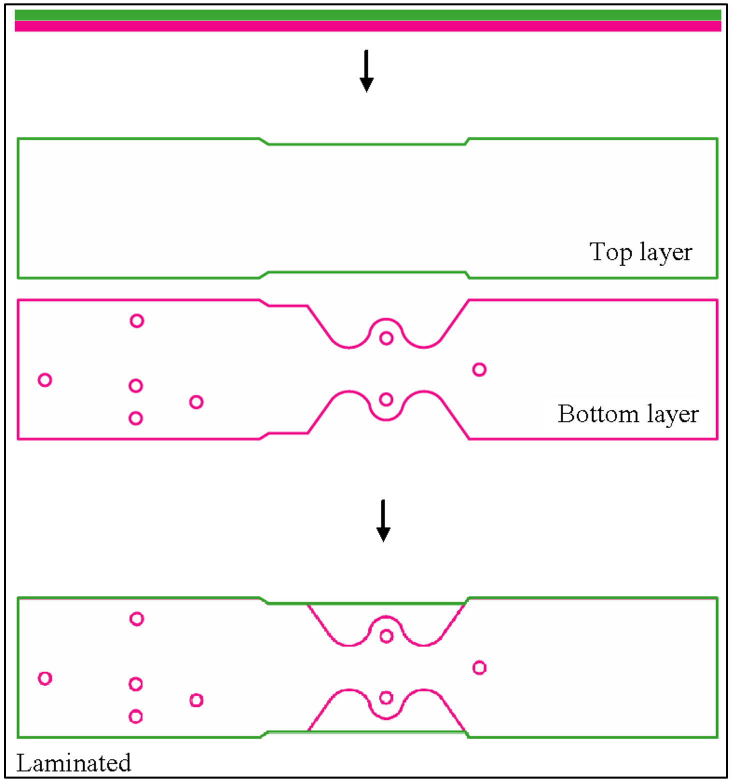
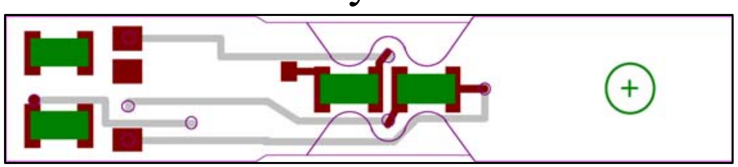


Layout



PROCESSING

1. Cutting green LTCC sheets,
2. Screen-printing inner conductors,
3. Attaching layers by gluing,
4. Screen-printing surface conductors, TFR
5. Lamination and co-firing the structure at 875°C

REMARKS

1. Top layer: under tension
   Bottom layer: under compression

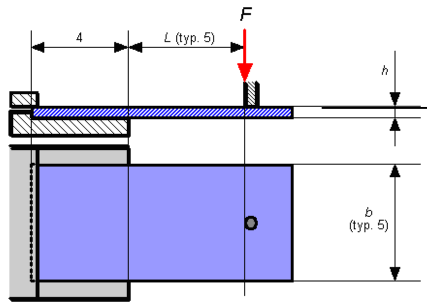
2. Bottom layer is:

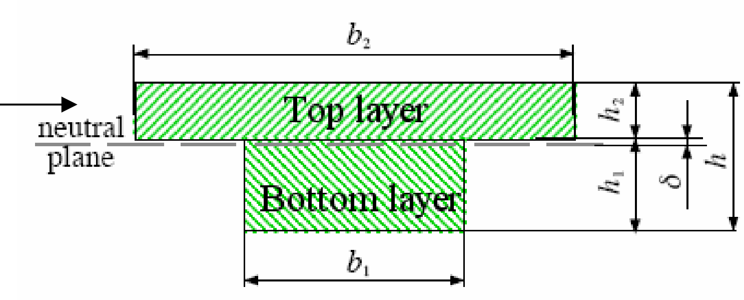
   - ideally selected thicker than top
   - narrows forming a neck

to *maximize the compressive / tensile forces* on the resistors (layout)

SELECTION OF LTCC SHEETS ←→ MAXIMIZING COMP. / TENS. STRESS

<u>CROSS SECTION :</u>





<u>FROM MATERIALS POINT :</u>

LTCC is ceramic → tensile forces are detrimental!
(crack-growth and propagation)

So, <u>minimize tensile forces</u>

<u>FROM MECHANICS POINT :</u>

$$r = \frac{-\varepsilon_{bottom}}{+\varepsilon_{top}} = \frac{-\sigma_{bottom}}{+\sigma_{top}} = \frac{h_1 - \delta}{h_2 + \delta}$$

Ratio between the compressive stress in the bot-tom and the tensile stress in the top;

So, <u>maximize « r » or (h_1 / h_2)</u>

EXPERIMENTAL II
LIMITATIONS / MATERIALS COMPATIBILITY

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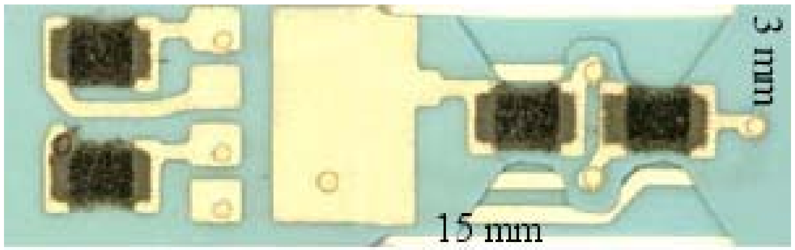
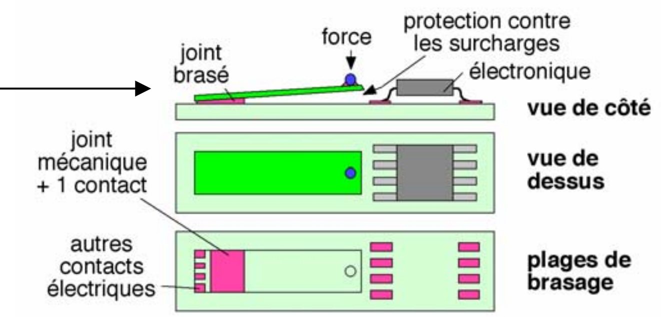
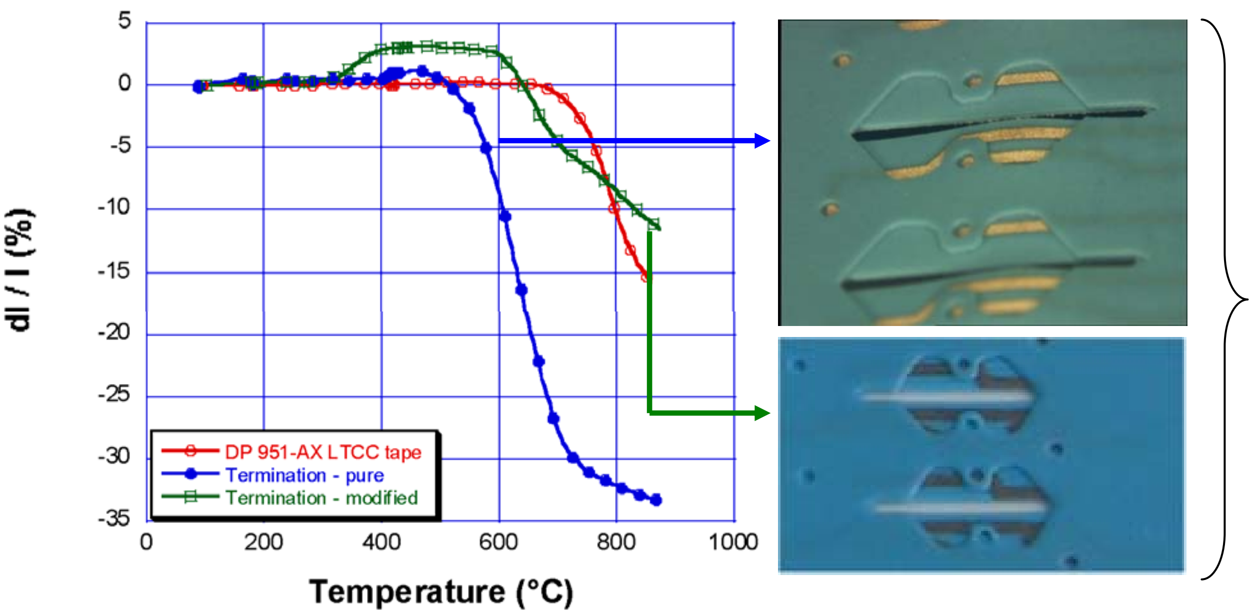




MAJOR PROBLEM: Differential Shrinkage (LTCC / Conductors)



Shrinkage-match achieved by

1. modifying commercial pastes using selected additives

2. Hiding termination between layers

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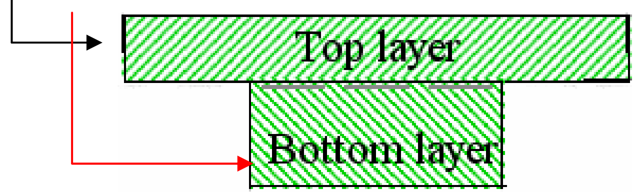
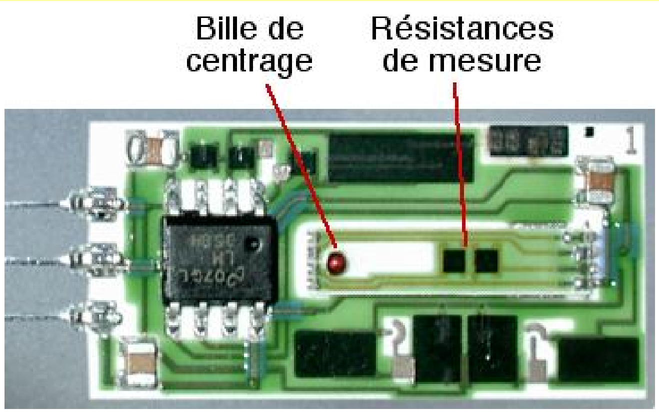
RESULTS I
MEASUREMENTS

Prepared sensors

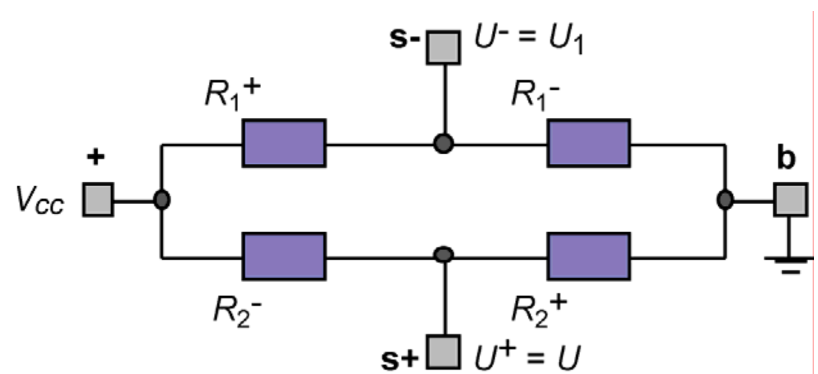
Material	Configuration	Fired thickness (mm)	Deformation	1/thickness (1/mm)	Signal (mV)
Alumina	250	0.25	-	4.00	7.5
LTCC	250 / 110	0.29	-	3.45	12
LTCC	110 / 250	0.29	-	3.45	15
LTCC	110 / 110	0.18	+	5.56	15
LTCC	110 / 50	0.13	-	7.69	40



Beam soldered on the mechanical support, Which also carries electronic components



Measurements made by applying varying weights on MFS, with a wheatstone-bridge conf.



RESULTS II
PERFORMANCE / COMPARISON

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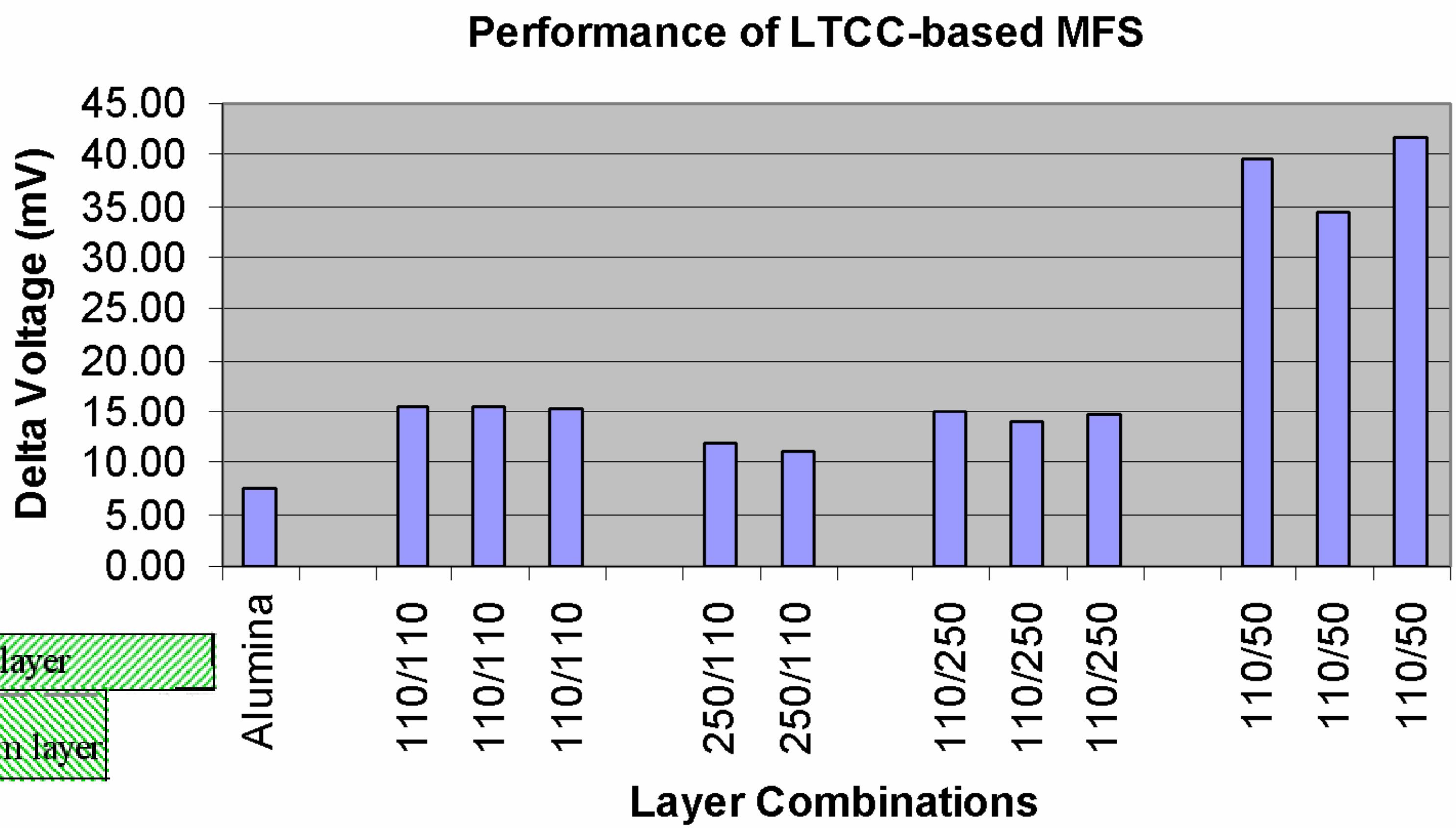
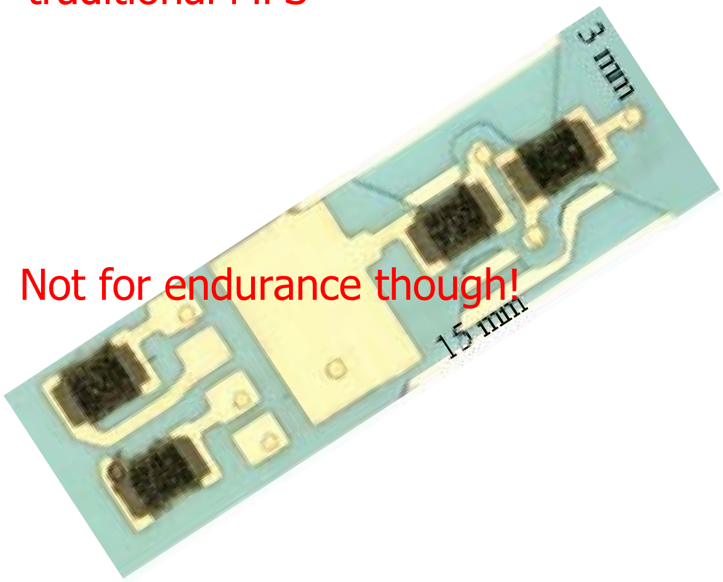


<u>Expected improvement by replacing alumina (full bridge) with LTCC (half bridge)</u>

= ~ 4x (thickness) 2x (modulus) ½ x (half-bridge) ≈ 4x ; but it reaches
~ 6x → by novel design

CONCLUSIONS

- LTCC-based MFS is fabricated, yielding a performance that is expected theoretically → ~ 6x better sensitivity than Al-based, traditional MFS



- The elastic modulus, thickness and design flexibility makes LTCC an interesting choice for force sensing → Not for endurance though!

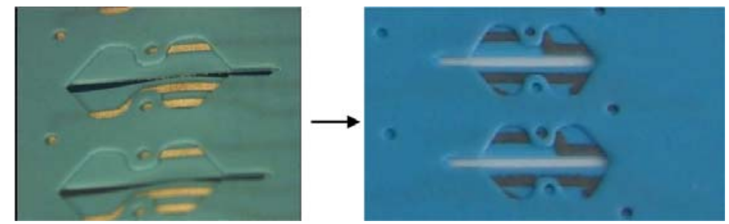
- Materials compatibility improves sensitivity by reducing deformation on the beam → Reduced deformation on the beam means stress-free TFR

NEXT STEPS

- Further reducing MFS thickness is limited by the technology:

  - LTCC tapes available
  - Materials compatibility

  → Differential shrinkage



- Novel designs with improved comp. / tens. stress distribution on the TFR

- Improving line-definition of the printed thick-film material