# - Semester Project Fabrication of glass suspended microchannel resonators 

Author:<br>Tobias Bachmann

Professor:<br>Guillermo Villanueva<br>TA:<br>Damien Maillard

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I would like to thank Prof. Villanueva for having allowed me to work on this project. It was fascinating to see how things are done on a nanoscopic level, and being able discover and work in the CMi cleanrooms was a privilege. Of course, I would like to thank Damien Maillard, who always answered the many questions I had. This project would not have been possible without his precious help.


#### Abstract

The goal of this project was to study if the fabrication of glass suspended microchannel resonators was possible. Through trial and error, the process parameters were determined, starting from the ideal dose in the dry etching process. The ideal size was determined by choosing a dose that guaranteed that all holes were properly opened, while keeping the critical dimensions (CD). This allowed us to keep holes small enough to be able to fill them later on in the process. The ideal was found to be $24 \mathrm{~mJ} / \mathrm{cm}^{2}$. The next step of the project was to determine the right cleaning methods of the microchannels. After some unfruitful attempts, a cleaning process that worked was found. Its main steps are HF $1 \%$ during 3 minutes, followed by 1 minute in a KOH 9:1 IPA bath at room temperature. Finally, sputter deposition and LPCVD were tested to close the microchannels, with both presenting some advantages and disadvantages. During this final step, the stress buildup in the $\mathrm{SiO}_{2}$ film showed, creating cracks in the membrane. For this reason, this process flow is not viable to fabricate glass suspended microchannel resonators.


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## 1 Introduction

Microchannel resonators are used to weigh particles as they flow through a hollowed out cantilever, achieving a precision to the nearest femtogram. Such precision is achieved by measuring the shift in resonance frequency of the electronically actuated cantilever. Classically fabricated using Silicon nitride, this project aims to make use of silicon oxyde. Silicon Oxyde ( $\mathrm{SiO}_{2}$ ), better known as glass, does have a higher rigidity, so a higher quality factor Q, but its main characteristic of interest is its low thermal conductivity. This allows the microresonnator to be used for calorimetry applications, as less heat is going to escape.
This presents a couple of challenges, as $\mathrm{SiO}_{2}$ has not been used to build microchannel resonators before by the ANEMS group at EPFL. More than just having to test out variable options for ourselves, $\mathrm{SiO}_{2}$ is also a challenging material to work with, as its non-conductive properties render it hard to look at in a Scanning Electron Microscope.

## 2 Process Flow

The first step in any project that takes place at CMi is to determine its process flow. The process flow from a similar project, entitled "Optimization of Channel Design and Fabrication for suspended microchannel resonators" was taken and adapted to the specific needs generated by the particularities of working with $\mathrm{SiO}_{2}$ instead of low-stress Silicon Nitride (ls-SiNx). After consultation with Damien Maillard and the CMi staff, the initial Process flow was approved and can be found in the Annex.

The most substantial differences between the processes are the cleaning of the microchannels (Steps 7, 8 and 9) after the dry-etching of the channels. Indeed, we anticipate that the $30 "$ BHF step would be detrimental to the integrity of the $\mathrm{SiO}_{2}$ layer. This is due to some chemicals having radically different etch rates in different materials.

## 3 Determination of Etch rates

To determine the length of time the wafers will have to be exposed to the chemicals, their respective etch rates will have to be determined. The first step was to research if these etch rates were already known. After some research $\square^{1}$, it was determined that it would be better to determine the etch rates experimentally, as accurate data was not available.

To determine the etch rates of certain chemical on the $\mathrm{SiO}_{2}$, two clean wafers, covered with a layer of $\mathrm{SiO}_{2}$ were used. The thickness of the $\mathrm{SiO}_{2}$ layers were measured using the FilMetrics F54 Automated Thickness Mapping Systems. The results can be seen in Table 1 below.

The next step was to expose the wafers to the different processes that we wanted to measure:

- The first process involved HF diluted to $1 \%$. The wafer was immersed in HF $1 \%$ for 3 minutes, followed by immersion in water and IPA to remove the HF.
- The second process involved $\mathrm{KOH}(40 \%)$ 9:1 IPA heated to $50^{\circ} \mathrm{C}$. The wafer was immersed for 2 minutes, followed by an immersion in water to remove the solution.

The final step in determining the etch rate of each process was to measure the thickness of the $\mathrm{SiO}_{2}$ layer again. The results can be seen in Table 1 below.

Table 1: Etch rates using the different processes

| Process | Thickness before etch (nm) | Thickness after etch (nm) | Etch duration (min) | Etch rate (nm/min) |
| :---: | :---: | :---: | :---: | :---: |
| HF 1\%, RT | $491 \pm 2$ | $473 \pm 1.7$ | 3 | 6 |
| KOH $(40 \%) 9: 1 \mathrm{IPA}, 50^{\circ} \mathrm{C}$ | $491 \pm 1.2$ | $489 \pm 1.2$ | 2 | 1 |

[^0]The observed etch rates will be used later on to determine the immersion time of the wafers during the cleaning phase of the fabrication of the microchannels.

## 4 Optimisation of process parameters

The parameters that still need to be precisely determined are the dose in step 4 of the process flow, as well as the exact time the wafers have to be in the different acids and bases in steps 7,8 and 9 .

### 4.1 Dose ( $\mathrm{mJ} / \mathrm{cm}^{2}$ )

One of the important parameters that would influence the fabrication process of the microchannels would be the dose used in the lithography process in step 3 of the process flow. To test the effects of each dose, test wafers with microchannels were created. Each set of 4 microchannels was exposed to a different dose, ranging from 16 to $32 \mathrm{~mJ} / \mathrm{cm}^{2}$, with an interval of $1 \mathrm{~mJ} / \mathrm{cm}^{2}$ between each set. Using the Scanning Electron Microscope, the size of the holes according to the dose was determined. Results can be found in Table 2 ,

Table 2: Size of holes in function of Dose

| Dose (mJ/cm2) | 32 | 31 | 30 | 29 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| width ( nm ) | 430,9 | 412,2 | 413,8 | 441,3 | 446,8 | 415,7 |  |  | 364,4 | 360,1 | 340,3 | 317,3 | 325,2 | 334,1 | 304,8 | 311,6 | 279,6 |
| height ( nm ) | 502 | 412,2 | 419,8 | 406,6 | 410,8 | 407,8 |  |  | 374,4 | 360,1 | 341,8 | 339,9 | 307 | 327,2 | 304,8 | 292,1 | 268,4 |
| average ( nm ) | 466,45 | 412,2 | 416,8 | 423,95 | 428,8 | 411,75 |  |  | 369,4 | 360,1 | 341,05 | 328,6 | 316,1 | 330,65 | 304,8 | 301,85 | 274 |

After a closer look at the data and the photos taken with the SEM, one can see that some data points do not seem correct. Indeed, the height and width of each hole should theoretically be the same. These errors were due to an astigmatism present during one of the SEM sessions. The effects of this astigmatism can be seen in Figure 1a, and can be compared to a different image where astigmatism is not present (Figure 1b). Therefore, all elements where the height and width differed more than 15 nm were removed and the results can be seen in Table 3. This gave a new table from which a Graph 2 can be drawn.

Table 3: Size of holes in function of Dose with cleaned data

| Dose $(\mathrm{mJ} / \mathrm{cm} 2)$ | 32 | 31 | 30 | 29 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| width $(\mathrm{nm})$ |  | 412,2 | 413,8 |  |  | 415,7 |  |  | 364,4 | 360,1 | 340,3 | 317,3 | 325,2 | 334,1 | 304,8 |  | 279,6 |
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On the graph, the polynomial trendline equation corresponding to the average between the width and the height of each hole can be seen. This function allows us to estimate the size of each hole according to the dose in $\mathrm{mJ} / \mathrm{cm}^{2}$. The equation is:

$$
\begin{equation*}
y=-0,0385 \cdot x^{2}-3,8676 \cdot x+429,31 \tag{1}
\end{equation*}
$$



Figure 1: The subtle difference between photos that present astigmatism and those that don't


Figure 2: Size of holes according to dose, cleaned data
$y$ corresponds to the size of one side of the holes and $x$ corresponds to the dose in $m J / \mathrm{cm}^{2}$.

Other than the size of the holes, the other deciding factor in the determination of the ideal dose was if all of the holes were complete. Indeed, some holes were not entirely formed for low doses (see Figure 3).

It was also observed that if the dose was too strong, the structure would not hold, and the roof of the channels could come loose (See figure 4).

The ideal dose was therefore chosen to be at $24 \mathrm{~mJ} / \mathrm{cm}^{2}$, creating square holes of average side length of 369.4 nm .


Figure 3: Incomplete holes due to insufficient dosage


Figure 4: Ruptured microchannels subjected to $32 \mathrm{~mJ} / \mathrm{cm}^{2}$

### 4.2 Microchannel cleaning methods

After the determination of the optimal dose in the lithography step, the next parameter that has to be optimised is the microchannel cleaning. Indeed, native oxide will form in the channels, and if not removed, can act as a mask for the KOH etching later on. To remove this, the wafers are submerged in a HF $1 \%$ solution. Following the determination of the etch rates, one can expect that a 3 minute bath in HF $1 \%$ will remove about 18 nm of native
oxyde, more than what is expected to be present.
Following the HF bath, the wafers need to be exposed to a KOH solution to clean up the $S i$ on the insides of the microchannels.

The first cleaning test on microchannels was set up.

This cleaning is rendered complicated, as ideally, one should have access to both Acid Wet Bench and Base Wet Bench simultaneously. Moreover, the wafers need to go from acid to base, then back to acid, where they have to stay for 2 hours for neutralisation. The timing therefore has to be extremely precise, and all processes involved have to be optimised to minimize time loss and going over the reserved time at each bench.

The first cleaning test was done in this order:

- First of all, a bath in HF $1 \%$ during three minutes on the Acid Wet Bench
- Then, to remove the HF, the wafer sections were then rinsed in three consecutive DI water baths.
- Still in their last water bath, the wafer sections were then transported to the Base Wet Bench
- Once on the Base Wet Bench, the KOH mixture had to be prepared. This consisted in creating a $\mathrm{KOH}(40 \%)$ 9:1 IPA mixture, and heating it up to $50^{\circ} \mathrm{C}$ using a magnetic stirring hot plate.
- Once the wanted temperature was achieved, the wafer sections were inserted into the mixture, and left for three minutes.
- Once the three minutes over, the wafer sections were again rinsed in three separate DI water containers, and the transported back to the Acid Wet Bench,
- The wafer sections were left to sit for at least two hours in $\mathrm{HCl} 37 \%$ for neutralization.
- Finally, the wafers were again rinsed three times in DI water.

The results of this first test can be seen in Figure 5, and it can be observed that the thin walls between the microchannels have been destroyed by an exposure to the heated KOH solution that lasted too long.
One can also see the effect that the size of holes has on the cleaning process. The image in top left was exposed to $23 \mathrm{~mJ} / \mathrm{cm}^{2}$, the one on top right to $22 \mathrm{~mJ} / \mathrm{cm}^{2}$, bottom left to 18 $\mathrm{mJ} / \mathrm{cm}^{2}$ and finally bottom right to $17 \mathrm{~mJ} / \mathrm{cm}^{2}$.

The second cleaning test was done on wafer section that had been exposed to larger doses and consisted in the following steps:


Figure 5: Different side views of 3 min HF and 3 min KOH at $50^{\circ} \mathrm{C}$ cleaning

- 3 minutes in HF $1 \%$
- 1 minute in $\mathrm{KOH}(40 \%)$ 9:1 IPA at $50^{\circ} \mathrm{C}$
- Neutralization in $\mathrm{HCl} 37 \%$ for at least 2 hours

In between each step, the wafer sections were rinsed with 3 baths of DI water.
The results can be seen in Figure 6. Again, the effects of the size of the holes can be seen. Indeed, the bigger the holes, the more the chemicals can enter the microchannels and be in contact with the thin microchannel walls. Top left corresponds to the biggest holes, with a dose of $32 \mathrm{~mJ} / \mathrm{cm}^{2}$, top right $28 \mathrm{~mJ} / \mathrm{cm}^{2}$, bottom left $27 \mathrm{~mJ} / \mathrm{cm}^{2}$ and finally bottom right $25 \mathrm{~mJ} / \mathrm{cm}^{2}$.
We can observe that being exposed to the KOH mixture at $50^{\circ} \mathrm{C}$ for 1 minute is still too long, as the walls are destroyed or too thin.

To reduce the speed at which the KOH mixture attacks the Si , two options presented themselves:

- We could either reduce the time further and keep the temperature at $50^{\circ} \mathrm{C}$


Figure 6: Different side views of 3 min HF and 1 min KOH at $50^{\circ} \mathrm{C}$ cleaning

- or we could reduce the temperature to room temperature, slowing down the etch rate of the KOH solution in the Si .

To simplify the process, it was therefore decided to forego the heating of the KOH mixture and to operate at room temperature. The third cleaning test consisted in doing the same steps as for the first two, but this time the wafers were only exposed to the KOH solution for 1 minute at room temperature.
The results of this cleaning test can be seen in Figure 7.
As can be seen in Figure 7, the dose, thus the size of the holes has a great impact on the cleaning process.

Figure 7 a shows us the side view of the channels, previously exposed to $16 \mathrm{~mJ} / \mathrm{cm}^{2}$, after cleaning. We can observe that the channels are not cleaned well enough, and that there are still some left over "pillars" that were not entirely removed by the baths.

Already a dose higher, at $17 \mathrm{~mJ} / \mathrm{cm}^{2}$ (Figure 7b), the pillars are all but destroyed, and only a small amount of extra material is left. The surface inside the microchannels is still very rough, meaning that, for this dose, the length of time the wafer sections are exposed to the KOH solution is not long enough. The width of the thinnest wall between two microchannels

(c) Dose: $24 \mathrm{~mJ} / \mathrm{cm}^{2}$, width of thinnest wall

Figure 7: Different side views of 3 min HF and 1 min KOH at RT cleaning
was also measured in at $1.011 \mu \mathrm{~m}$.

At $24 \mathrm{~mJ} / \mathrm{cm}^{2}$ (Figure 7 c ), all extra residue is removed. In this case, the thinnest wall only measures 834.8 nm , almost 200 nm less than the channels exposed at $17 \mathrm{~mJ} / \mathrm{cm}^{2}$. The interior surface of the channels are smoother, meaning that the $\mathrm{SiO}_{2}$ deposition in the next steps of fabrication will be of much higher quality.

We have therefore determined a cleaning process that works for the fabrication of this specific type of microchannels:

- Start off with a 3 minutes HF $1 \%$ bath.
- Rinse three times in DI water to stop the effects of the HF.
- Transport the wafers or wafer sections, without letting them dry, to the Base Wet Bench.
- Insert the wafers or wafer sections into the KOH solution for 1 minute. This solution is a $\mathrm{KOH}(40 \%)$ 9:1 IPA mixture at room temperature.
- Rinse three times in DI water to stop the effects of the KOH solution.
- Neutralize the wafers/ wafer sections in HCl for at least 2 hours.
- Rinse three times in DI water.

It is important to note that this cleaning process is optimised for a dose of $24 \mathrm{~mJ} / \mathrm{cm}^{2}$, or for holes sized around 370 nm . If the holes are of a different size, or if the dose is different, the time lengths of the different cleaning baths has to be adapted.

## 5 Closing of the channels

Up until now, we have determined the dose needed and the size of holes to which this corresponds. Using this information, we determined the appropriate cleaning process, leaving us with clean channels in Si underneath a thin film of $\mathrm{SiO}_{2}$, as can be seen in Figure 8 ,


Figure 8: State of the fabrication after cleaning

The next step in the process flow is to create $\mathrm{SiO}_{2}$ walls inside the channels, and to close the holes on top of the channels. To do this, there are several options available to us.

### 5.1 Sputter Deposition

The first method tested to close the channels is sputter deposition. This type of physical vapor deposition consists in ejecting material from a source material, also known as "target" onto the wafer.
In our case, a 400 nm SiO 2 sputter deposition was done using the Spider 600 in Z04. A side view can be seen in Figure 9 .


Figure 9: Side view after sputter deposition

From Figure 9, we can see that the channels are not closed up, probably due to the fact that the 400 nm layer deposition was too thin. In order to see if the the holes have gotten smaller or not, a closer look can be taken in Figure 11. Indeed, the initial size of the holes corresponding to this dose is 370 nm , after the sputter deposition, they are now only 80 nm . We can therefore conclude that the holes have indeed gotten smaller, and we can assume that if the thickness of the added $\mathrm{SiO}_{2}$ were to be increased, the holes would eventually close up. One can also observe that from all these side views (Figures $9,11,12$ and 10), the channels seem to be intact for the most part. In Figure 9, we can see that the roofs of the channels seem to have broken off to some extent, but we can assume that this happened while cleaving the wafers for observational purposes after the sputter deposition.

In this case again, we can see the effects the initial dose has on the rest of the process. If we take a look at Figure 12, corresponding to a dose of $16 \mathrm{~mJ} / \mathrm{cm}^{2}$, we can see that


Figure 10: Side view of channels exposed to $24 \mathrm{~mJ} / \mathrm{cm}^{2}$ after sputter deposition


Figure 11: Size of holes after sputter deposition
the initial holes are not big enough to let through enough material to build a a full $\mathrm{SiO}_{2}$ surface in the inside of the microchannels. Indeed, it causes some small accumulations of the deposition on the bottom of the channels, but nothing on the side walls. This is therefore another confirmation of the choice of a dose of $24 \mathrm{~mJ} / \mathrm{cm}^{2}$.


Figure 12: Side view of channels exposed to $16 \mathrm{~mJ} / \mathrm{cm}^{2}$ after sputter deposition

### 5.2 LPCVD

The second option was to use a Low pressure chemical vapor deposition process. As its name indicates, this process uses chemical vapor deposition induced by a high temperature to build a thin film on the wafer. Two options existed:

- TEOS (Tetra Ethyl Ortho Silicate), process done at $710{ }^{\circ} \mathrm{C}$ and 200 mT
- or LTO (Low Thermal Oxide), process done at $425^{\circ} \mathrm{C}$ and 120 mT

After consultation with CMi staff, it was decided that the best option would be the TEOS process, as the quality of the deposition would be higher. Higher quality does however come with a drawback, as the temperature reached during this process could have some negative side effects.


Figure 13: Top view of the holes after 500 nm TEOS

After a 500 nm deposition, the first step was to look at the wafers from the top. This gave two very important results: First of all, as can be seen in Figure 13, the holes seem to be filled. However, looking at the top of the wafers also revealed cracks in the roof of the devices. These can be seen in Figures 14 and 15 .

Indeed, on most of the devices, the part where the channels are the largest shows some cracks, as can be seen in Figure 14. On one occasion, it was even observed that a crack formed on the thinnest part of the microchannel, as can be seen in Figure 15.
A side view of the cleaved microchannel can be seen in Figure 16. The image was taken at an angle in order to remove the saturation caused by the non conductive $\mathrm{SiO}_{2}$. In this image, we can also observe the buckling of the roof. This buckling is probably what causes the cracks to appear. Finally, the TEOS process is very efficient in coating the inside walls of the microchannels in $\mathrm{SiO}_{2}$. The coated thickness is measured in Figure 17.

### 5.3 Comparison between the different techniques

Comparing the two different techniques, there are several advantages and disadvantages for each technique. Indeed, the sputter deposition is a very easy process to do, we have however, not yet tested if the holes would close up all the way if the thickness were to be increased.
The LPCVD has a higher quality, but also a big disadvantage, as the cracks appear in the


Figure 14: Cracks appear after the TEOS process


Figure 15: Cracks appear after the TEOS process


Figure 16: Side view of the TEOS coated channels


Figure 17: Thickness of $\mathrm{SiO}_{2}$ coating inside the microchannels
roofs of the microchannels. The most probable cause for these cracks is the stress present in the $\mathrm{SiO}_{2}$ membrane.

This specific and last part of the mechanical aspect of this project still needs some attention to determine the best way to close up the microchannels.

## 6 Conclusion

To conclude, this project was an adaptation by trial and error of an already existing process flow to a new kind of material. After determination of the optimal dose for the dry etching process, a cleaning method was devised, taking into account the specific characteristics of the materials in use. The final process flow can be found in the annex. However, this project did not find a viable way to fabricate glass suspended microchannel resonators. The main problem is the stress in the $\mathrm{SiO}_{2}$ layer that induces cracks in the membranes. A next possible step would be to include a layer of tensile stressed silicon nitride to conteract the compressive stresses in the $\mathrm{SiO}_{2}$.
two different methods to close the channels were tested and compared. The process flow for the fabrication of glass suspended microchannel resonators.

## $7 \quad$ ANNEX

## Initial Process Flow after modification

## Optimization of Channel Design and Fabrication for suspended microchannel resonators

## Description of the fabrication project

We fabricate suspended microchannel resonators, using silicon oxide $\left(\mathrm{SiO}_{2}\right)$ as structural material. Microchannels are etched in silicon through Bosch process, and cleaned with diluted HF and KOH.
The purpose of the project is to fabricate the suspended microchannels that are made of silicon oxide $\left(\mathrm{SiO}_{2}\right)$. The shape of the microchannels will be etched directly in a silicon substrate on which $\mathrm{SiO}_{2}$ layers has been deposited previously. The sidewalls and the bottom of the microchannels will be defined by depositing of $\mathrm{SiO}_{2}$ on the etched shape. The micro-channels will be closed by the deposition as well. The microchannels will be then released from the substrate to form the suspended microchannels.

## Technologies used

DUV lithography, Dry and wet etching, RCA cleaning, LPCDV $\mathrm{SiO}_{2}$ deposition, SEM

## Photolithography masks

| Mask \# | Critical <br> Dimension | Critical <br> Alignment | Remarks |
| :---: | :---: | :---: | :---: |
| 1 | 200 nm | First layer | Stepper |
| 2 | $20 \mu \mathrm{~m}$ | 2um | Release |
| Substrate Type |  |  |  |
| Silicon <100>, Ø100mm, 525um thick, Single Side polished, Prime, p type, 0.1-0.5 Ohm.cm Thin film : 200 nm SiO 2 . |  |  |  |

## Interconnections and packaging of final device

Thinning/grinding/polishing of the samples is required at some stage of the process.
$\overline{\mathbf{X}}$ No $\quad$ Yes $\Rightarrow$ confirm involved materials with CMi staff
Dicing of the samples is required at some stage of the process.
区 No ■ Yes => confirm dicing layout with CMi staff
Wire-bonding of dies, with glob-top protection, is required at the end of the process.
X No $\quad$ Yes $=>$ confirm pads design (size, pitch) and involved materials with CMi staff

Step-by-step process outline

| Step | Process description | Cross-section after process |
| :---: | :---: | :---: |
| A0 | 6' reticle mask <br> Fabricated externally |  |
| 01 | Substrate: $\operatorname{Si}$ test $+\mathrm{SiO}_{2}$ (200 nm) |  |
| 02 | Photoresist coating <br> Material: $D U V 42 P+J S R$ <br> KrF M35G <br> Machine: ACS200 <br> Thickness: 1200 nm |  |
| 03 | DUV lithography + Development Machine: ASML PAS $5500 / 350 c+A C S 200$ |  |
| 04 | Dry etching <br> Material: $\mathrm{DUV} 42 \mathrm{P}+\mathrm{SiO}_{2}$ <br> Machine: SPTS APS <br> Depth: $60 \mathrm{~nm}+200 \mathrm{~nm}$ |  |
| 05 | Dry Etching <br> Material: Si <br> Machine: AMS 200 <br> Thickness: $6 \mu \mathrm{~m}$ |  |


| $\mathbf{0 6}$ | PR removal <br> Material: DUV42P + JSR <br> KrF M35G <br> Machine: Tepla Gigabatch |  |
| :---: | :--- | :--- |
| $\mathbf{0 7}$ | Immersing to remove residues <br> Solution: HF 1\% <br> Time: to be determined <br> Arias Acid wet bench Z14 <br> Keep in beaker containing <br> water to move it to Arias <br> solvent wet bench Z14 |  |
| $\mathbf{0 8}$ | Immersing to remove HF <br> Solution: Water followed by <br> IPA (to reduce surface <br> tension) <br> Arias solvent wet bench Z14 |  |
| $\mathbf{0 9}$ |  | Immersing to remove residues <br> Solution: KOH (40\%) + IPA <br> (9:1) <br> Time: 25 <br> Arias Base wet bench Z14 |
| $\mathbf{1 0}$ |  | SEM Inspection <br> Machine: SEM Zeiss Leo <br> Arias Acid wet bench Z14 <br> 2h neutralization HCl 37\% |
|  |  |  |


| $\mathbf{1 2}$ | RCA cleaning (without SRD) |  |  |
| :---: | :--- | :--- | :--- |
| $\mathbf{1 3}$ | LPCVD (done by the staff, <br> RCA) <br> Material: $\mathrm{SiO}_{2}$ <br> Thickness: 300 nm |  |  |

Final process flow

## Optimization of Channel Design and Fabrication for suspended microchannel resonators

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| $\mathbf{0 6}$ | PR removal <br> Material: DUV42P + JSR <br> KrF M35G <br> Machine: Tepla Gigabatch |  |
| :---: | :--- | :--- |
| $\mathbf{0 7}$ | Immersing to remove residues <br> Solution: HF 1\% <br> Time: 3 minutes <br> Arias Acid wet bench Z14 <br> Keep in beaker containing <br> water to move it to Arias <br> solvent wet bench Z14 |  |
| $\mathbf{0 8}$ | Immersing 3 times to remove <br> HF <br> Solution: DI water <br> Arias Acid wet bench Z14 |  |
| $\mathbf{0 9}$ | Immersing to remove residues <br> Solution: KOH (40\%) + IPA <br> (9:1) <br> Time: 1 minute <br> Arias Base wet bench Z14 |  |
| $\mathbf{1 0}$ |  | RCA cleaning (without HF) <br> SEM Inspection <br> Machine: SEM Zeiss Leo <br> Ahias Acid wet bench Z14 <br> 2h neutralization HCl 37\% |
|  |  |  |
|  |  |  |


| $\mathbf{1 3}$ | LPCVD (done by the staff, |  |
| :--- | :--- | :--- | :--- |
|  |  |  |
|  |  |  |
|  |  |  |
| Thickness: 500 nm |  |  |


[^0]:    ${ }^{1}$ Pauline Stevic (July 19 2018) BOE / HF - Silicon dioxide Etching Standard Operating Procedure
    ${ }^{2}$ Mitsushi Itano, Frederick W . Kern, Jr., Masayuki Miyashita, and Tadahiro Ohmi, Member, IEEE (3 August, 1993) Particle Removal from Silicon Wafer Surface in Wet Cleaning Process

