

# Numerical generation and contact analysis of rough surfaces in concrete

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## 1 Introduction

In concrete, **mixed-mode** loading leads to development of inter-facial stresses ( $\tau, \sigma$ ) between crack lips. This leads to increase in shear-carrying capacity of a concrete structure [1, 2].

Our aim is to understand the role topography (**roughness, aggregate distribution**) of cracks in concrete play in determining the inter-facial shear stress.

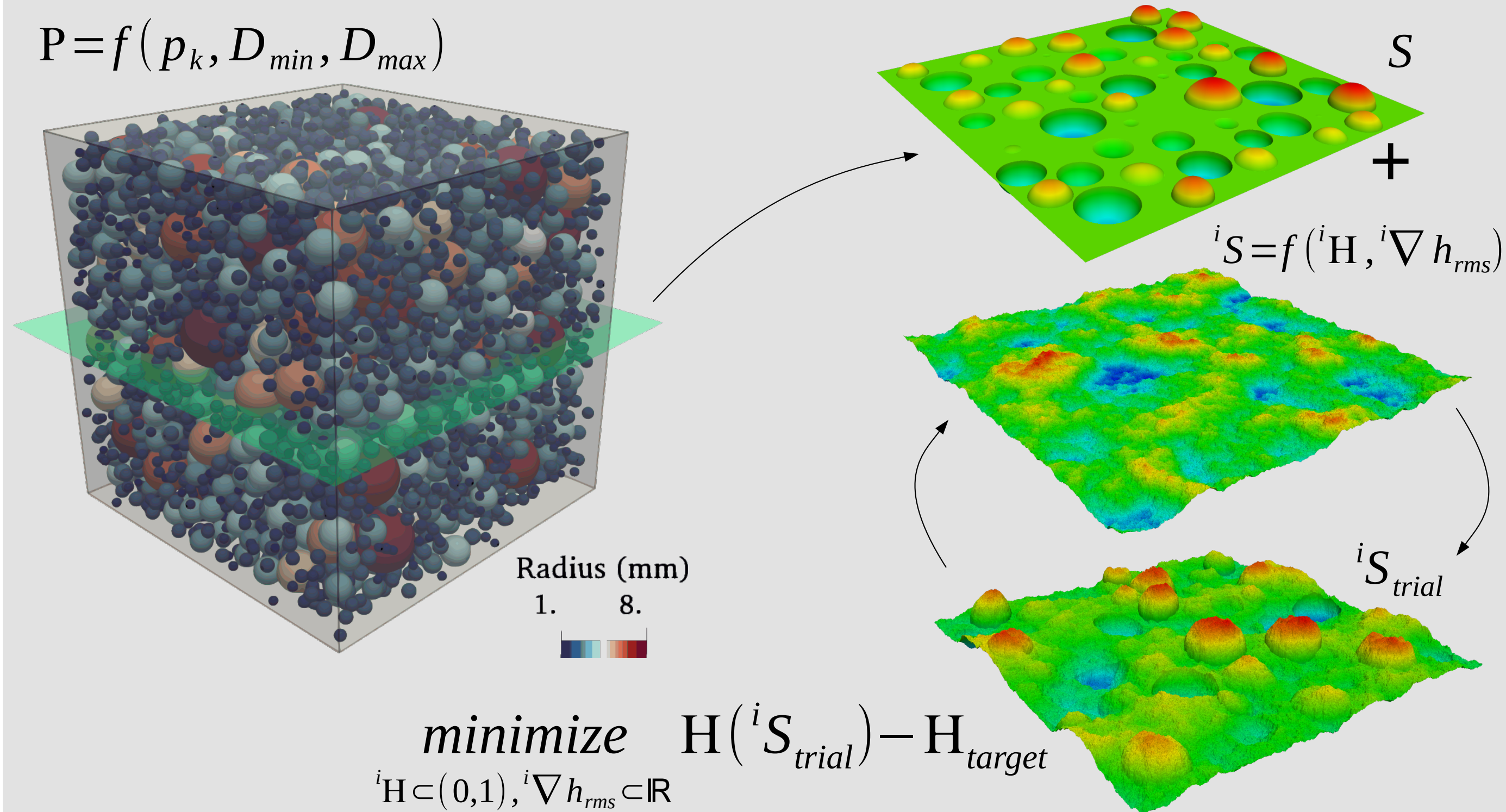
The interfacial shear stress between two contacting surfaces can be represented with a probability density integral depending on:

- Number of contact clusters,  $N$
- Contact force per cluster,  $f$
- y-component of Normal vector per cluster,  $n_y$

$$E[\tau] = \frac{1}{A_0} \iiint_{N, f, n_y} \rho(N) \cdot \rho(f|N) \cdot \rho(n_y|N) \cdot f \cdot n_y \cdot N \cdot \delta N \delta f \delta n_y$$

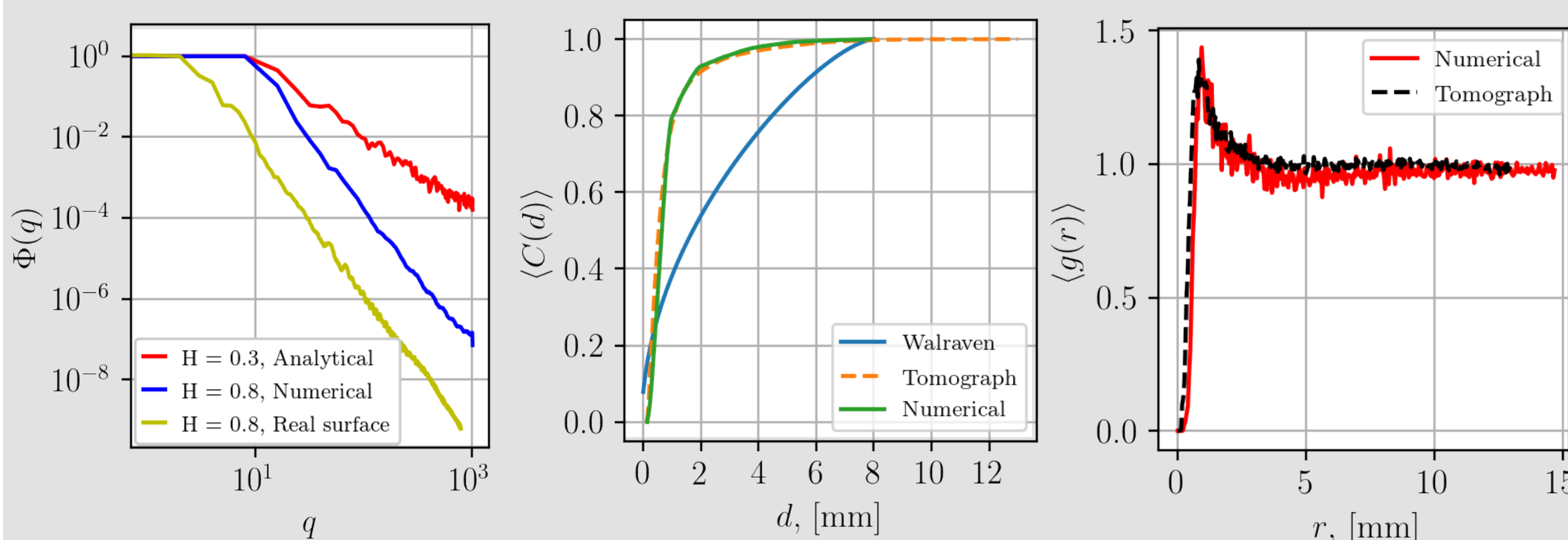
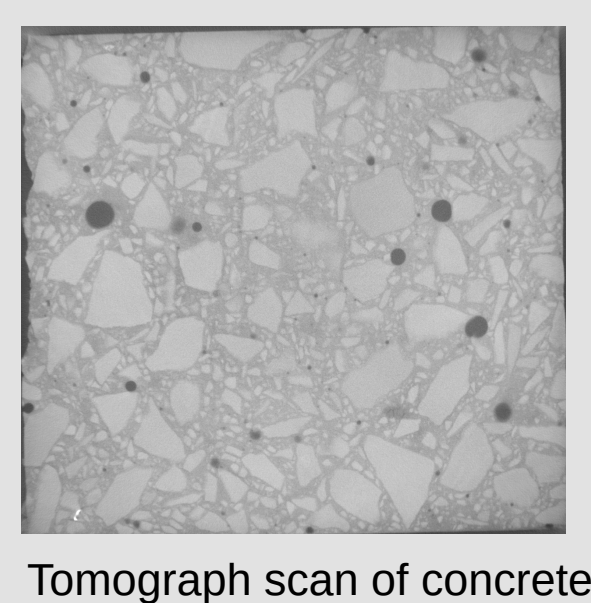
## 2 Method overview

Artificial concrete rough surfaces are fabricated to control the parameters : aggregate size distribution and roughness (**Hurst exponent, H**).



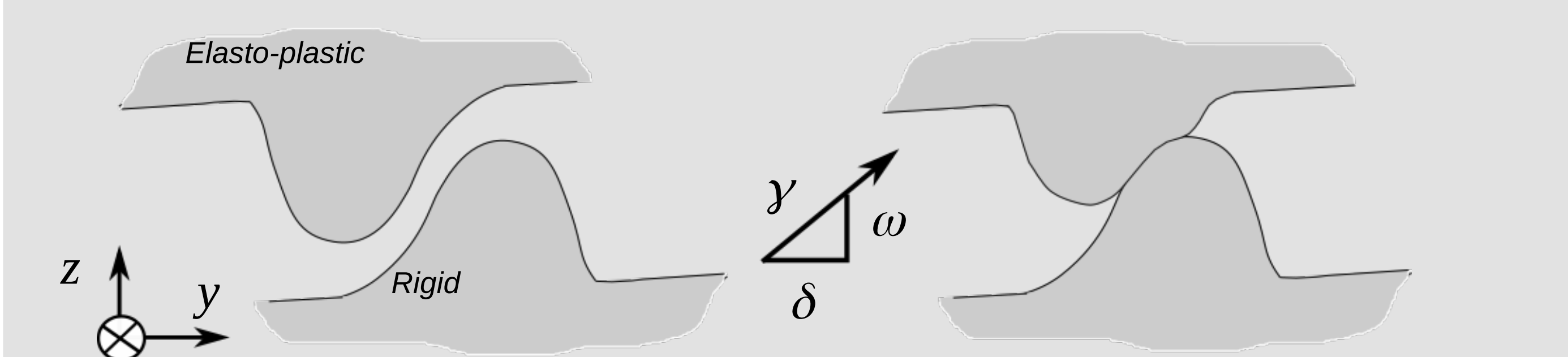
Artificially generated concrete rough surfaces are validated against surfaces from real concrete sample on 3 criteria:

- Hurst exponent,  $H(iS_{trial}) = 0.8$  matches with real surface
- Distribution of aggregate sizes  $\langle C(d) \rangle$  on surface  $S$  matches that of real concrete surface scanned using Tomograph
- Average density of aggregates in all direction,  $\langle g(r) \rangle$



We employ **Boundary-Element Method** [2] to numerically solve for contact between artificially generated surfaces considering **elasto-plastic** interactions.

The two conforming surfaces are loaded under mixed-mode loading.



## 3 Results and discussion

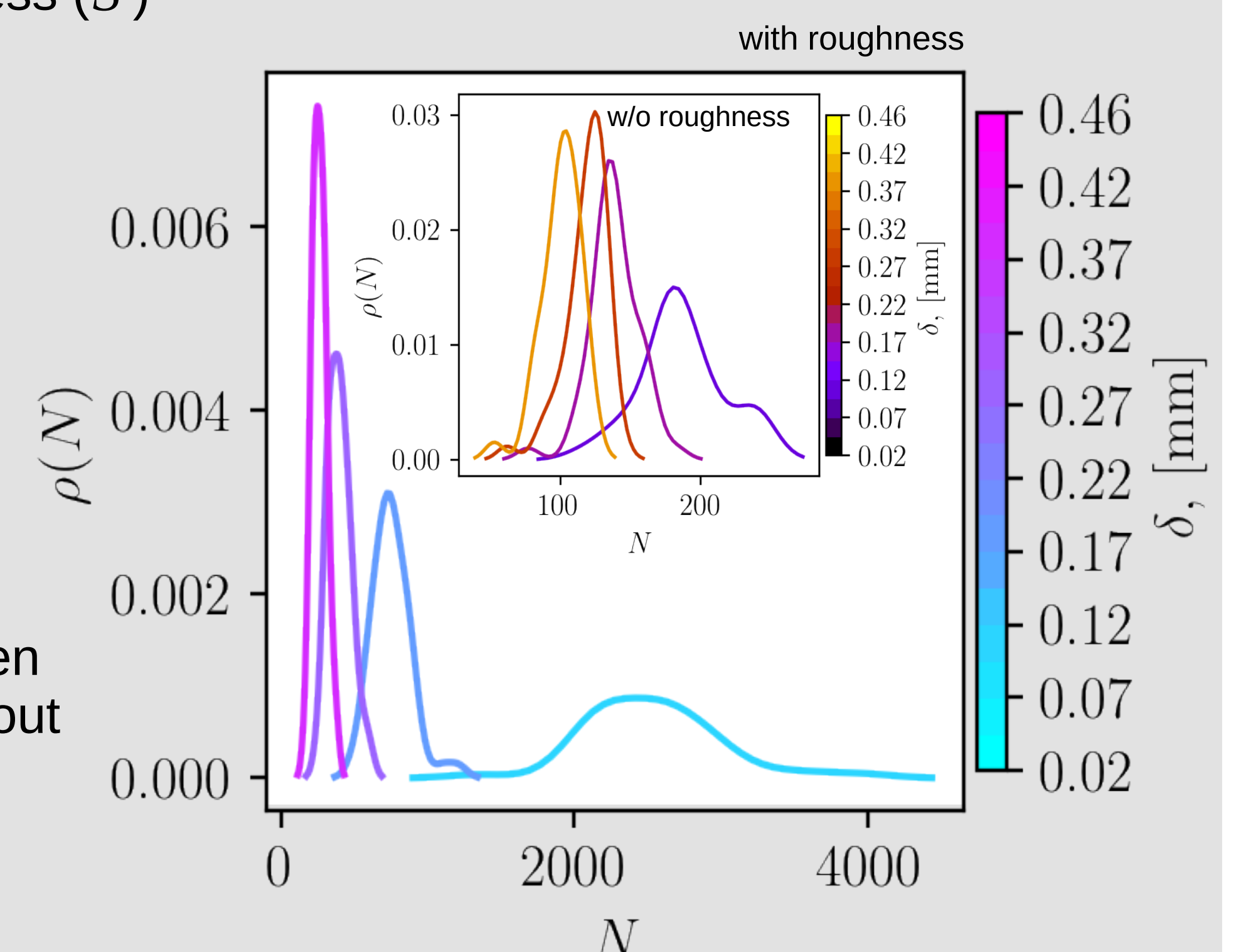
Probability densities for surface with roughness ( $iS_{trial}$ ) and surface without roughness ( $S$ )

$$\rho(N)$$

- Number of contact clusters decreases with increasing  $\delta$

- Follows Gaussian distribution

- Large number of contact clusters with roughness when compared with surface without roughness

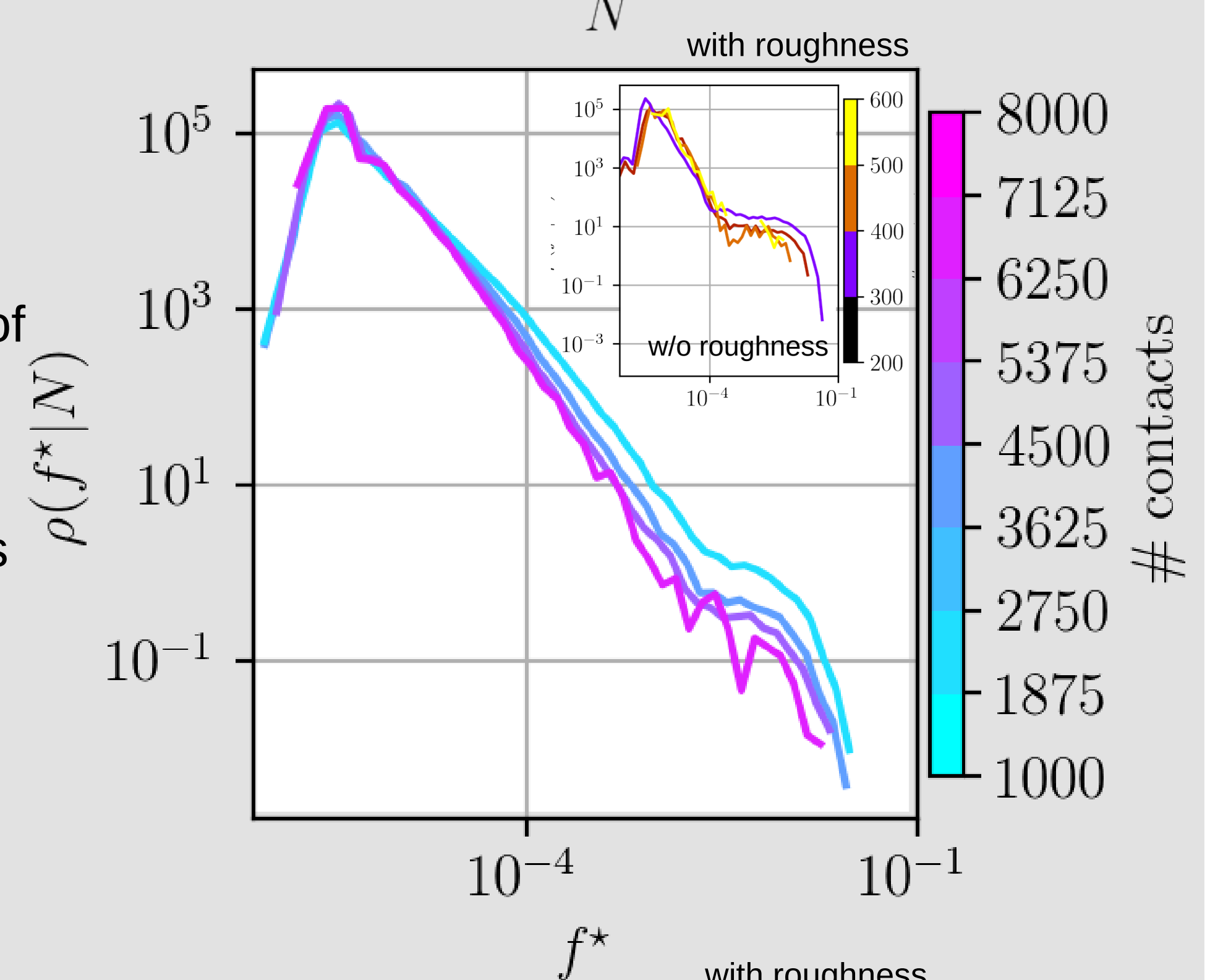


$$\rho(f|N)$$

- Follows a power-law

- Slope depends on number of contacts and therefore on  $\delta$

- Probability density saturates for higher forces (more evident for surface without roughness), effect of aggregates

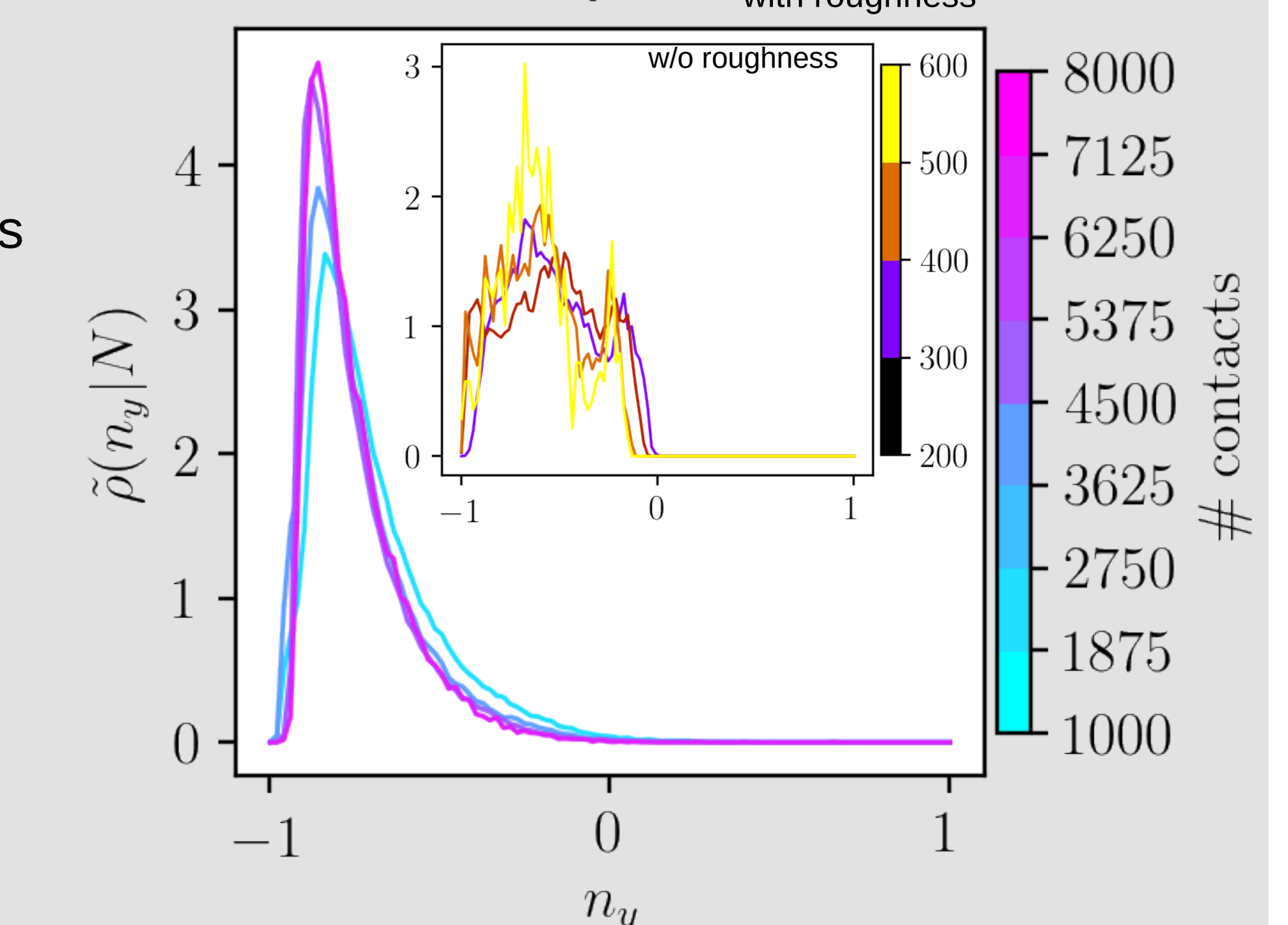


$$\rho(n_y|N)$$

- Max probability density shifts from value of -1 to 0 as increases  $\delta$

- A value of -1 indicates that  $E[\tau]$  will have large value, hence more resistance

- Thus, as  $\delta$  increases  $E[\tau]$  will decrease



## 4 Conclusion

- Artificial surfaces generated satisfy necessary characteristics and thus gives a better representation of a real rough surface in concrete

- Various probability densities follow a well-defined distributions when roughness is considered

- Thus, analytical expressions can be deduced as  $f(\delta, \gamma)$  for analytical computation of  $E[\tau]$

## 5 References

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2. J. S. Jacobsen, P. N. Poulsen, J. F. Olesen, *Characterization of mixed mode crack opening in concrete*, Mater. Struct. 45 (2012) 107–122, 2012
3. V. Rey, G. Anciaux, *Normal adhesive contact on rough surfaces : efficient algorithm for FFT-based BEM resolution*, Comput. Mech. 60 (1) (2017) 69–81, Springer Berlin Heidelberg, 2017