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# Reconfigurable Logic Gates Based on Programmable Multistable Mechanisms

*Binary logic gates are building blocks of computing machines, in particular, electronic computers. One variant is the programmable logic gate, also known as the reconfigurable logic gate, in which the logical function implemented can be modified. In this paper, we construct a mechanism to implement a reconfigurable logic gate. This mechanism is based on the concept of programmable multistable mechanisms which we introduced in previous work. The application of a programmable multistable mechanism is superior to the different bistable mechanisms previously used to implement logic gates since a single mechanism can be used to implement several logic functions. Our reconfigurable logic gates use a novel geometric construction where the geometric data depend on the stability behavior of the mechanism. There are 16 binary logic gates and our construction can theoretically produce nine of these and our physical model produces six logical gates. Input and output of the mechanism are displacement and the mechanisms can be combined serially, i.e., output of a mechanism is an input for another. We show that we can implement NOR and NAND gates, so combinations of our mechanism can express any logical function. The mechanism is therefore theoretically universal, i.e., implement any computation. We give an analytic model of the mechanism based on Euler–Bernoulli beam theory to find the geometric data, then validate it using finite element analysis and experimental demonstration. [DOI: 10.1115/1.4045970]*

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## 1 Introduction and Statement of Results

**1.1 Logic Gates.** Binary logic gates have two inputs each taking on possible values *True* or *False*, with an output taking on values *True* or *False*. For technical reasons, the usual mathematical formulation is to denote *True* by the number 1 and *False* by the number 0 [1]. Logic gates are the classical building blocks of computing machines. Electronic transistors are widely used to implement these logic functions due to the speed and miniaturized size within the nano-regime and simple integration with electronic circuits. However, under extreme conditions occurring in space applications such as high temperature and cosmic radiation, electronic gates can fail. On the other side, mechanical structure is reliable functioning under these conditions [2,3]. This has motivated research into purely mechanical structures to implement logic gates. Switches and rods are a basic example for the implementation of mechanical logic [4]. Mechanical oscillators have recently been utilized as logic devices where the logic output is encoded by oscillator frequency [5]. Bistable mechanisms have also been used to build logic gates [6,7].

There are four unary logic gates and 16 basic binary logic gates [1] and these can be combined to implement any general logical expressions. Of special interest are the NOR and NAND gates which can reproduce any other unary and binary logic gate and are therefore called *universal*. It follows that the implementation of a NOR or NAND gate and the ability to combine gates allow one to implement any computable logic function.

One construction of a binary logic gate is the *programmable logic gate*, also known as the *reconfigurable logic gate*, where the logic gate functionality can be modified post-fabrication. This paper will

focus on the construction of purely mechanical reconfigurable logic gates.

**1.2 Multistable Mechanisms.** The mechanisms considered in this paper are *compliant mechanisms* that perform their functions by the deformation of their flexible elements, e.g., slender beams [8,9].

These mechanisms store *strain energy* as they deform, and local energy minima positions correspond to stable states and energy maxima to unstable states. The qualitative behavior of such mechanisms can be described by their energy profile [9]. In particular, a mechanism is called a *multistable mechanism* if it has more than one stable state.

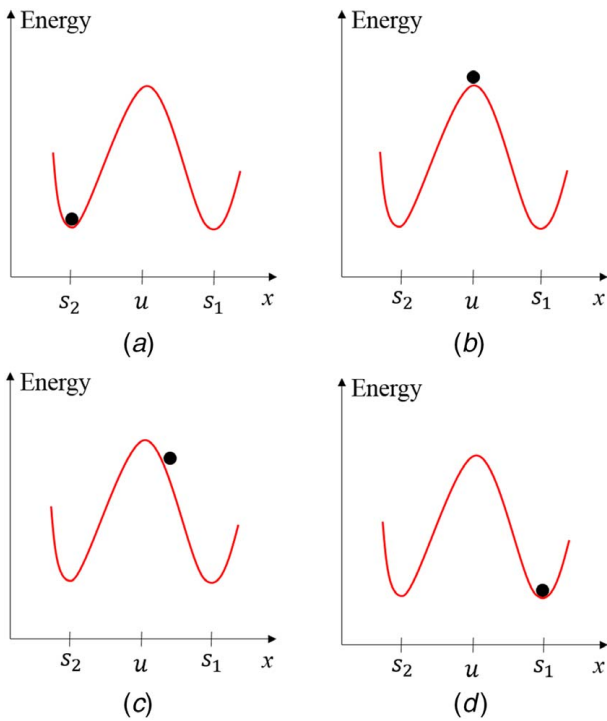
As a bistable mechanism is displaced from one stable state to another stable state, it passes through an unstable state, and before doing so, its stored energy increases. When displaced past the unstable state, the mechanism converts potential energy into kinetic energy, since the system is conservative, and the mechanism displaces to the other stable state [8], see Fig. 1, where the position of the ball indicates the state of the mechanism.

The most basic multistable mechanism is the *bistable mechanism* having two stable states. Examples of these are curved beams [10,11], the four-bar mechanism [12,13], slider crank mechanism [14], and tensural pivots [15]. Bistable mechanisms are well suited for logic computation due to their binary nature. Since they act as switches, they can be considered as mechanical analogues of transistors

**1.3 Programmable Multistable Mechanisms.** The bistable mechanisms applied to logic gates can only implement a single logic function. In order to implement reconfigurable logic gates, we use *programmable multistable mechanisms* (PMM) introduced in our previous work [16–18]. These are characterized by having a set of inputs we have named *programming inputs*  $p_2$  and  $p_1$  to modify the mechanism's stability behavior, in particular, the

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**Fig. 1** Strain energy of the displacement-driven bistable mechanism where the mechanism position is denoted by the ball at (a) stable state  $s_2$ , (b) unstable state  $u$ , (c) past unstable state  $u$ , and (d) to other stable state  $s_1$

number of stable states. Figures 2(a) and 2(b) illustrate our mechanism with programming inputs  $p_2$  and  $p_1$  and output  $x$ .

As opposed to bistable mechanisms which are displacement driven, our programmable multistable mechanisms produce displacement by modifying the energy profile. One can think of this as moving an object on a carpet by lifting the carpet, i.e., actuation is orthogonal to displacement.

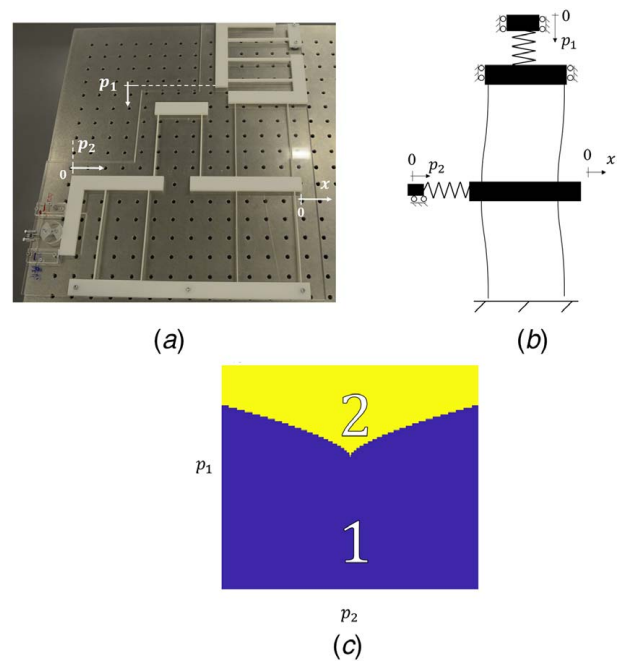
This is illustrated in Fig. 3, where the ball again represents the state of the mechanism. The mechanism is initially bistable with the ball at stable state  $s_2$  (Fig. 3(a)). Then, programming inputs  $p_1$  and  $p_2$  are applied to modify the energy profile (Fig. 3(b)). At certain values of  $p_1$  and  $p_2$ ,  $s_2$  becomes unstable as illustrated in Figs. 3(c) and 3(d) and the mechanism becomes monostable (Figs. 3(e) and 3(f)). After that, the ball moves to the other stable state  $s_1$ , which is now the only stable state (Figs. 3(e) and 3(f)). One advantage of this method is that actuation is more repeatable, as was applied to the construction of a medical device for delicate eye surgery [18].

The set programming values  $p_1$  and  $p_2$  are partitioned into regions where the mechanism is monostable and bistable. This is described by a *programming diagram*; Fig. 2(c) discussed in detail in Sec. 3. This discretization is used to construct logic gates via the geometric method of Sec. 1.4, in particular, regions of monostability will correspond to True, i.e., to output 1 and regions of bistability will correspond to False, i.e., 0.

**Remark.** In this paper, we use the term “programming” to refer to the modification of the stability behavior of the mechanism. This has no relation to stored computer programs in computability.

**1.4 Geometric Construction of Reconfigurable Logic Gates.** In this section, we present a novel geometric construction of a reconfigurable logic gate represented by block diagram in Fig. 4(a). The stability behavior of our PMM mechanism will provide the geometric data to implement this method.

Given a region  $\Omega$  in the plane and positive constants  $\alpha_2$  and  $\alpha_1$ , one can construct a reconfigurable logic gate  $f_{r_2, r_1}(i_2, i_1)$ , where  $r_2$



**Fig. 2** (a) Physically constructed demonstrator of our multi-stable mechanism implementing logic gates, (b) conceptual diagram of our mechanism, (c) programming diagram showing the number of stable states corresponding to programming inputs  $p_1$  and  $p_2$

and  $r_1$  are values that reconfigure the gate and  $i_2$  and  $i_1$  are the binary logical inputs taking values 0 or 1.

For each choice of reconfiguration values  $r_2$  and  $r_1$ , one applies the logical values  $i_2$  and  $i_1$  using  $r_2$  and  $r_1$  so that logical input  $i_j$  corresponds to coordinate  $r_j + (i_j - 1/2)\alpha_j$ . More explicitly, this says that  $i_2 = 0$  corresponds to  $r_2 - \alpha_2/2$  and  $i_2 = 1$  corresponds to  $r_2 + \alpha_2/2$ , and similarly,  $i_1 = 0$  corresponds to  $r_1 - \alpha_1/2$  and  $i_1 = 1$  corresponds to  $r_1 + \alpha_1/2$ . Geometrically, this creates a rectangle centered at  $(r_2, r_1)$  with sides of length  $\alpha_2$  and  $\alpha_1$ , and whose four corners correspond to the four possible values of  $(i_2, i_1)$  (see Fig. 4(b)).

We then define a logic gate

$$f_{r_2, r_1} = \tau[(r_2 + (i_2 - 1/2)\alpha_2, r_1 + (i_1 - 1/2)\alpha_1) \in \Omega] \quad (1)$$

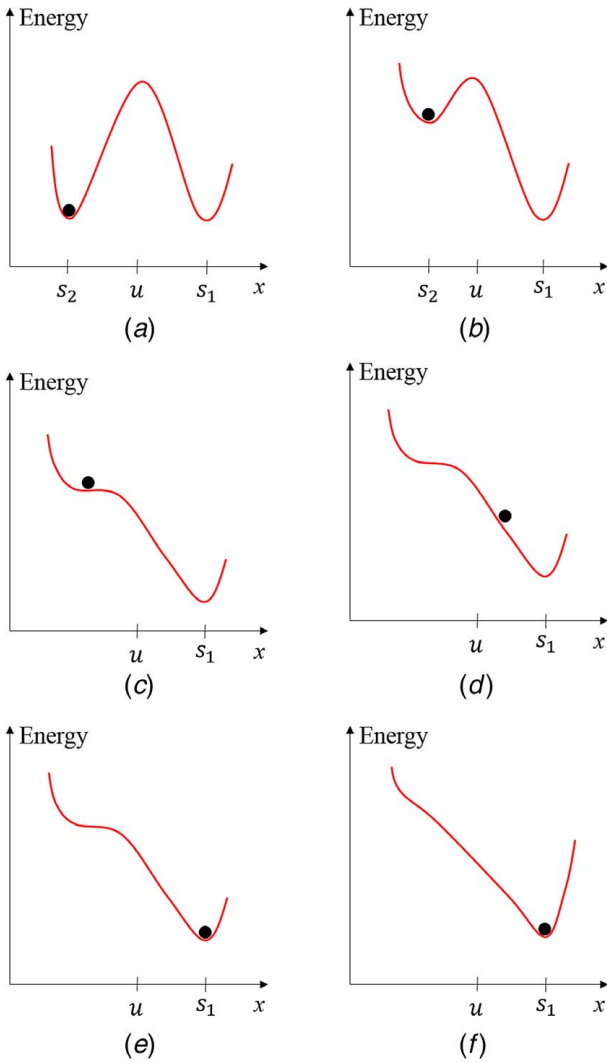
where  $\tau$  is the truth value of a logical expression  $\varepsilon$

$$\tau[\varepsilon] = \begin{cases} 1 & \text{if } \varepsilon \text{ is True} \\ 0 & \text{if } \varepsilon \text{ is False} \end{cases}$$

Geometrically, the logic gate  $f_{r_2, r_1}(i_2, i_1)$  returns 1 if and only if the corner of the rectangle corresponding to  $(i_2, i_1)$  lies inside the region  $\Omega$  (see Fig. 4(c)).

The 16 possible binary logical gates are not all necessarily implementable, as the possible gates depend on the region  $\Omega$ . For example, only 14 of these are possible when  $\Omega$  is the interior of a circular disc; the two functions corresponding to the rectangle having only opposite corners inside the disc are geometrically impossible; these are  $f_6 = 0110$  and  $f_9 = 1001$  using the notation of Table 1.

**1.5 Reconfigurable Logic Gates Generated by Programmable Multistable Mechanisms.** In this paper, reconfigurable logic gates will be generated by the geometric method of Sec. 1.4 where the region  $\Omega$  corresponds to a *programming diagram* described in more detail in Sec. 3. These charts will have the property that the region  $\Omega$  is the part of the plane lying below the single-valued function  $p_1 = \Phi(p_2)$ . This means that the truth value True



**Fig. 3** Strain energy of the one-degree-of-freedom programmable multistable mechanism for different values of  $p_1$  and  $p_2$  as the mechanism switches from bistability to monostability, where the ball denotes the position of the mechanism: (a) bistable with ball at stable state  $s_2$ , (b) the stable state  $s_2$  has a higher energy level, (c) stable state  $s_2$  vanishes and the ball starts moving to single stable state  $s_1$ , (d) ball moving toward the other stable state  $s_1$ , (e) the ball reaches the stable state,  $s_1$ , and (f) ball remains at stable state  $s_1$

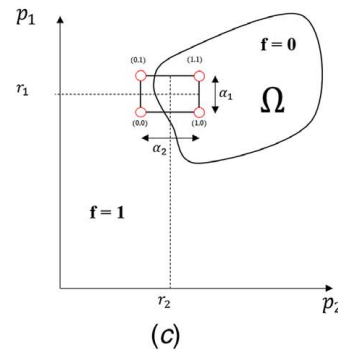
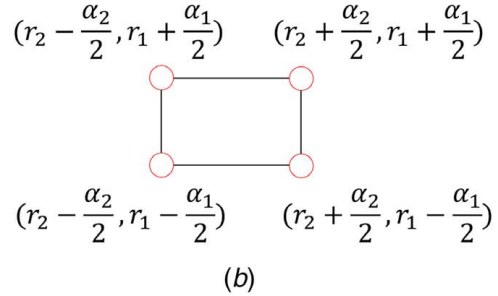
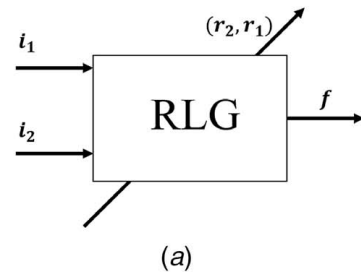
corresponds to being below the graph  $(p_2, \Phi(p_2))$  in the  $p_2$  and  $p_1$  plane (see Fig. 5).

In the case of a region defined by a single-valued function  $\Phi$ , the definition of a reconfigurable logic gate given by Eq. (1) becomes

$$f_{r_2, r_1}(i_2, i_1) = \tau[r_1 + (i_1 - 1/2)\alpha_1 < \Phi(r_2 + (i_2 - 1/2)\alpha_2)] \quad (2)$$

The definition of Eq. (2) states that  $f_{r_2, r_1}(i_2, i_1)$  has output 1 if and only if  $r_1 + (i_1 - 1/2)\alpha_1$  is less than  $\Phi(r_2 + (i_2 - 1/2)\alpha_2)$ .

The output  $f$  corresponds to a displacement  $x$ , as illustrated in Fig. 2. When the mechanism is bistable, then it has energy profile as illustrated in Fig. 3(b) and is in stable state  $s_2$ , corresponding to zero displacement  $x = 0$ . On the other hand, when the mechanism is monostable, then its energy profile corresponds to Fig. 3(d) where the mechanism is in the single stable state  $s_1$  corresponding to a displacement  $x > \beta$ , where  $\beta$  is a constant. The mechanism is designed so that  $\beta > \alpha_1$  and  $\beta > \alpha_2$ ; this property guarantees that the output of one of our mechanisms can be applied as input for another of our mechanisms, i.e., logical expressions can be constructed out of our logic gates.



**Fig. 4** (a) Block diagram representation of reconfigurable logic gate where  $i_1$  and  $i_2$  are the logic operands and  $r_1$  and  $r_2$  determine the logical operation and  $f$  is the logic output, (b) four possible logic input states, (c) region  $\Omega$  with output True when corner of the rectangle is outside  $\Omega$

**Table 1** Implementable functions

Logical expression	Binary code	$i_1$	1	0	1	0
		$i_2$	1	1	0	0
False	$f_0$		0	0	0	0
$\neg(i_1 \vee i_2)$	$f_1$		0	0	0	1
$\neg i_2$	$f_3$		0	0	1	1
$\neg(i_1 \leftarrow i_2)$	$f_4$		0	1	0	0
$\neg i_1$	$f_5$		0	1	0	1
$\neg(i_1 \wedge i_2)$	$f_7$		0	1	1	1
$i_2$	$f_{12}$		1	1	0	0
$i_1 \rightarrow i_2$	$f_{13}$		1	1	0	1
True	$f_{15}$		1	1	1	1

The number of possible logic gates generated by our PMMs using this geometric method is limited by the fact that

$$f(i_2, 1) = 1 \Rightarrow f(i_2, 0) = 1$$

which simply states that if  $r_1 + \alpha_1/2 < \Phi(r_2 + (i_2 - 1/2)\alpha_2)$ , then  $r_1 - \alpha_1/2 < \Phi(r_2 + (i_2 - 1/2)\alpha_2)$ . Geometrically, this says that if a top corner of the rectangle is below the graph, then the bottom corner just under it is also below the graph.

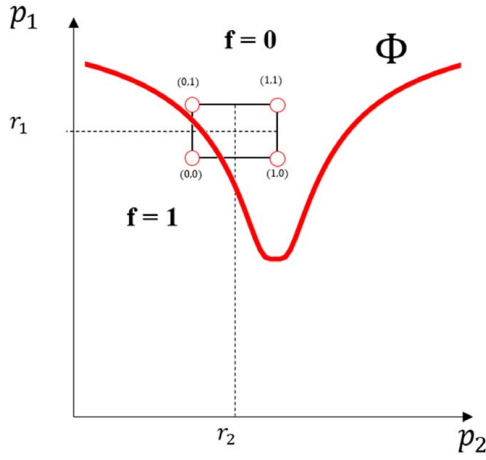


Fig. 5 Single valued function boundary  $p_1 = \Phi(p_2)$

This is the only general restriction, and using the notation of Table 1, it forbids all binary codes  $f_{xx10}$  and  $f_{10xx}$ , that is, the seven functions

$$f_2 = f_{0010}, \quad f_6 = f_{0110}, \quad f_8 = f_{1000},$$

$$f_9 = f_{1001}, \quad f_{10} = f_{1010}, \quad f_{11} = f_{1011}, \quad f_{14} = f_{1110}$$

In general, this method can generate nine logic gates at most and these functions are listed in Table 1. The number of the implemented logic functions depends on value of  $\alpha_1$  and  $\alpha_2$ .

The partition  $\Phi$  generated by the programming diagram of our PPMs can generate all nine of these logic gates. Our physical demonstrator was limited only to four of these logic gates (see Sec. 6).

We note that  $f_1 = \neg(i_1 \vee i_2)$  and  $f_7 = \neg(i_1 \wedge i_2)$  in Table 1 correspond to a NOR gate and a NAND gate, respectively, since these are universal, our mechanisms can be combined to perform any computation. In particular, our demonstrator implements  $f_1$  (see Sec. 6).

The nine possible functions divided the space of reconfiguration parameters  $r_1$  and  $r_2$  into nine regions; this generates a *reconfiguration diagram* (see Fig. 6). This discrete partition of the reconfiguration space means that the reconfiguration of our logic gates can be done by applying nine discrete inputs. The application of this technique is the subject of our current research.

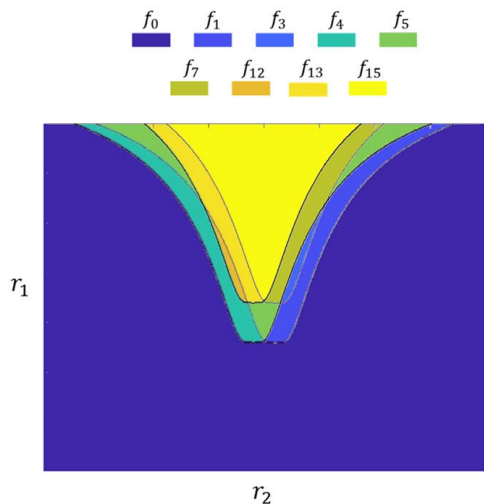


Fig. 6 The space of reconfiguration parameters  $r_1$  and  $r_2$  divided into nine regions corresponding to the nine possible logic gates

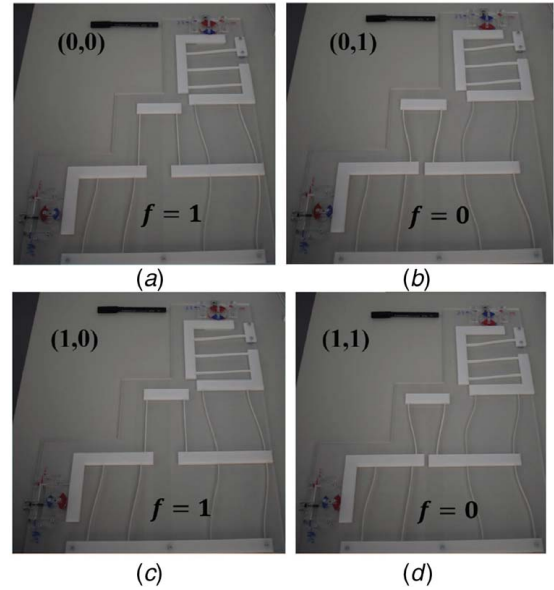


Fig. 7 Mechanism to implement  $f = \neg p_1^i$  at  $(p_2^i, p_1^i) =$  (a) (0,0), (b) (0,1), (c) (1,0), and (d) (1,1)

**1.6 Physical Implementation.** Figure 2(a) gives the physical implementation of a reconfigurable logic gate studied in this paper. The demonstrator is made of polyoxymethylene using laser cutting. Its programming diagram is given in Fig. 2(c). Two different logic functions are illustrated in Figs. 7 and 8. Further details concerning the application of the programming inputs are given in Fig. 19. We ensure that the displacement of the mechanism is within the linear regime; therefore, there is no plastic deformation.

We selected the dimensions of the mechanism such that the maximum stresses during actuation never surpass the admissible stress, which we define as the fatigue limit divided by a safety factor as discussed in Ref. [8].

**1.7 Advantages and Limitations.** Our implementation of logic gates has the following advantages compared to the state-of-the-art.

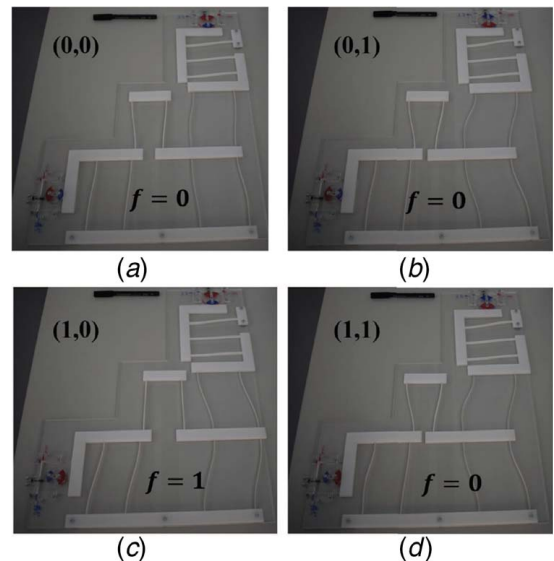


Fig. 8 Mechanism to implement  $f = p_2^i \wedge \neg p_1^i$  at  $(p_2^i, p_1^i) =$  (a) (0,0), (b) (0,1), (c) (1,0), and (d) (1,1)

- (1) Our logic gates are reconfigurable which enable the implementation of different logic functions using the same mechanical structure.
- (2) Our logic gates are based on multistable mechanisms so energy is required only during the transition between stable states, i.e., during computation. No energy is required to maintain the stable position of the mechanism.
- (3) Our mechanisms store output values, represented by the stable states.
- (4) Our mechanical logic gates can be combined without requiring auxiliary mechanisms.
- (5) Our logic gates are universal, i.e., any computable function can be implemented using the logic gates of this paper.
- (6) The number of the logic operands can be easily increased by adding a spring element for each additional input.

Complex functions can be implemented on combining logic gates. In logic design, two metrics are used to evaluate the performance of combined logic gates, fan out limit and propagation delay.

The fan out limit is the maximum number of logic gate inputs that can be driven by the output of the logic gate. As illustrated in Fig. 10, a small amount of energy is provided by the input  $E_{in}$ , represented by the energy difference between unstable state  $u$  and stable state  $s_2$ , to initiate the execution of the function. Also, the gate releases energy,  $E_{out}$ , equivalent to the energy difference between the unstable state,  $u$ , and the stable state,  $s_1$ , to represent a high output.

Therefore, the limit of the fan out is

$$M = \frac{E_{out}}{E_{in}} \quad (3)$$

assuming that the driven logic gates are identical.

The second parameter is the propagation delay. It is defined as the time taken by a signal to travel from the input of the logic gates to the output. In our case, we can consider our serial combination of programmable multistable mechanisms as a transmission line. The propagation delay within bistable transmission lines was addressed in Ref. [19] and it depends on the amount of energy released by each bistable unit and energy dissipation.

In this paper, we will focus only on the implementation of reconfigurable logic gates using programmable multistable mechanisms.

**1.8 Paper Outline.** The paper is organized as follows: Sec. 2 gives a complete description of our proposed reconfigurable logic

gate. Section 3 derives an analytical model to calculate the programming diagram by computing mechanism stiffness as a function of the programming inputs. Section 4 provides a description of the effect of modifying the programming inputs on the number of stable states, their position, and their stiffness. Section 5 gives a setup of the FEM simulation of our mechanism. Finally, Sec. 6 describes the logic gates implemented by our physical construction and deduces the reconfiguration diagram.

Whenever possible, we express our results using normalized parameters so that the expressions are independent of the actual physical dimensions of the mechanisms.

## 2 Elastically Driven Axially Loaded Double Parallelogram Mechanism

The *elastically driven axially loaded double parallelogram mechanism* (EADPM) given in Fig. 9 consists of two slender beams with thickness  $t$ , width  $w$ , and length  $\ell$ . The two beams are connected by a central block. On one extremity, the beams are fixed and the other extremity is restricted only to the movement in the axial direction of the beams and loaded by a spring of stiffness  $k_1$ . The central block is loaded by a spring  $k_2$  in the lateral direction of the beams. The spring  $k_1$  is preloaded by displacement  $p_1$  and the spring  $k_2$  is preloaded by displacement  $p_2$ . The displacement  $p_1$  and  $p_2$  are the programming inputs. The position of the central block of the mechanism is given by  $x$ .

When  $p_1 = 0$  and  $p_2 = 0$ , the mechanism is monostable as given in Fig. 9. On imposing  $x$ , the lateral displacement of the central block increases and spring  $k_2$  is loaded. As the beams deform laterally, the beams move axially loading  $k_1$ . On increasing  $p_1$  for  $p_2 = 0$ , the spring  $k_1$  imposes an axial load on the beams reducing its stiffness as illustrated in Figs. 10(a) and 10(b). As  $p_1$  increases beyond a critical value  $p_1^{cr}$ , the beams buckle and move laterally deforming the spring  $k_2$  and the mechanism is bistable. Figures 9(b) and 9(c) give the stable positions of the mechanism. These stable states correspond to the logic output.

As  $p_1$  increases beyond  $p_1^{cr}$ , the energy barrier between the stable states increases. However, if  $p_1 < 0$ , the stiffness of the mechanism increases.

The programming input  $p_2$  does not affect the stiffness of the beams. However, it modifies the mechanism overall stability behavior. To study the effect of  $p_2$  on the stability response of the mechanism, there are two qualitative distinct cases depending on  $p_1$ .

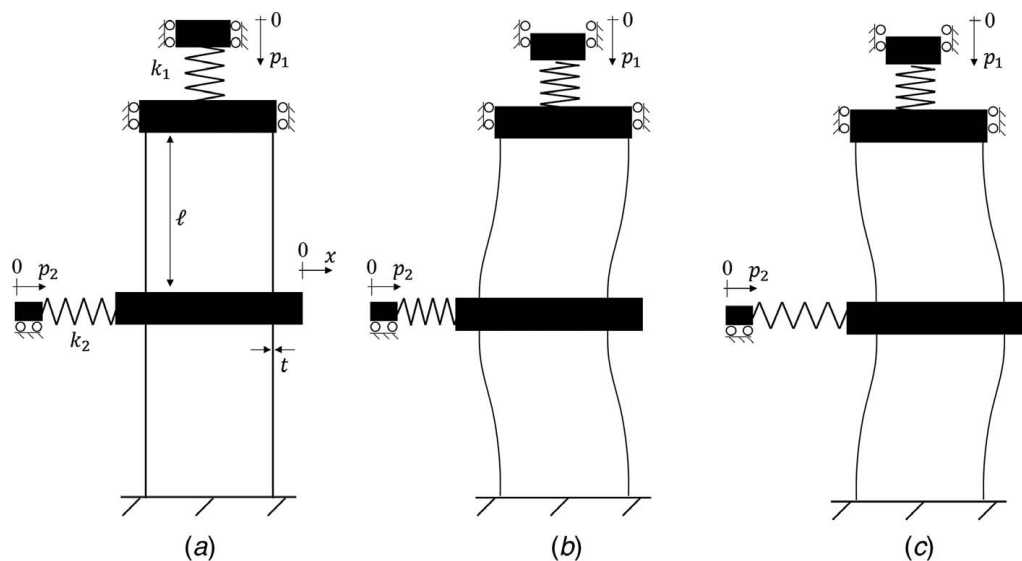
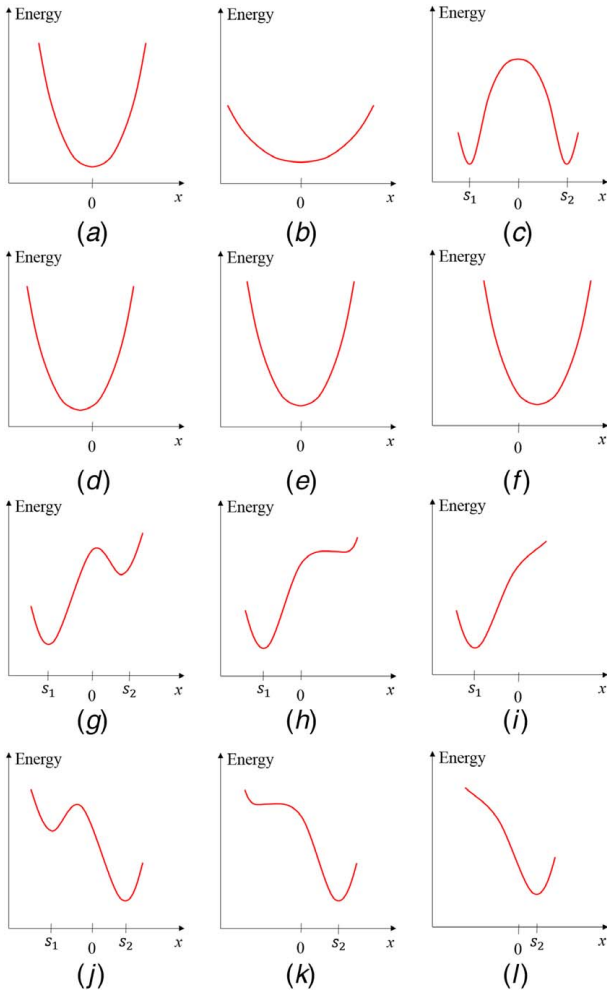


Fig. 9 An EADPM for  $p_2 = 0$  where (a) stable state at  $p_1 = 0$ , (b) and (c) stable states for  $|p_2| < p_2^{cr}$  and  $p_1 > p_1^{cr}$ , corresponding to high output and low output of a logic operation



**Fig. 10** Energy profiles of EADPM at (a)  $p_1 = 0, p_2 = 0$ ; (b)  $p_1 = p_1^{cr}, p_2 = 0$ ; (c)  $p_1 > p_1^{cr}, p_2 = 0$ ; (d)  $p_1 < p_1^{cr}, p_2 < 0$ ; (e)  $p_1 < p_1^{cr}, p_2 = 0$ ; (f)  $p_1 < p_1^{cr}, p_2 > 0$ ; (g)  $p_1 > p_1^{cr}, 0 < p_2 < -p_2^{cr}$ ; (h)  $p_1 > p_1^{cr}, p_2 = -p_2^{cr}$ ; (i)  $p_1 > p_1^{cr}, p_2 < -p_2^{cr}$ ; (j)  $p_1 > p_1^{cr}, 0 < p_2 < p_2^{cr}$ ; (k)  $p_1 > p_1^{cr}, p_2 = p_2^{cr}$ ; and (l)  $p_1 > p_1^{cr}, p_2 > p_2^{cr}$

**Case 1:**  $p_1 < p_1^{cr}$

The EADPM is monostable where the position of the stable state depends on  $p_2$ . At  $p_2 = 0$ , the mechanism has one stable position at  $x = 0$ . When  $p_2 > 0$ , the stable position will be at  $x > 0$ . Otherwise, the stable position will be at  $x < 0$  as illustrated by the energy profiles given in Figs. 10(d)–10(f).

**Case 2:**  $p_1 > p_1^{cr}$

If  $p_2 = 0$ , the mechanism is bistable. As  $p_2$  changes, the energy barrier will vary. There is a value at which  $|p_2| > p_2^{cr}$ , a stable and unstable state merge. Therefore, the energy barrier vanishes and the mechanism is monostable. The strain energy of the mechanism for different values of  $p_2$  when  $p_1 > p_1^{cr}$  are given in Figs. 10(g)–10(l).

Table 2 summarizes the different stability regions as functions of  $p_1$  and  $p_2$  where “–” indicates no impact.

**Table 2** Stability regions as functions of  $p_1$  and  $p_2$

Number of stable states	$p_1$	$p_2$
1	$p_1 < p_1^{cr}$	–
1	$p_1 > p_1^{cr}$	$ p_2  > p_2^{cr}$
2	$p_1 > p_1^{cr}$	$ p_2  < p_2^{cr}$

**Remark II:** The mechanism exhibits zero stiffness behavior at  $p_1 = p_1^{cr}$  or  $p_2 = p_2^{cr}$ . The mechanism is a zero force mechanism at  $p_1 = p_1^{cr}$  and a nonzero force mechanism when  $p_2 = p_2^{cr}$ .

**Remark III:** The value of  $p_2^{cr}$  is a function of  $p_1$ . The higher  $p_1$  is, the higher  $p_2^{cr}$  will be. When  $p_1 < p_1^{cr}$ ,  $p_2^{cr}$  does not exist.

### 3 Analytical Model

The goal of the model is to find the stability boundaries at which the mechanism switches between monostability and bistability, which are essential for finding the relation between the logic operation and the programming inputs. This requires a qualitative description of the stability behavior of the EADPM. Our model is based on the following assumptions:

- (1) The beams are slender, i.e., the beam thickness is 100 times lower than the length. Therefore, there is no shear within the beam.
- (2) The beam displacement is within its intermediate range.
- (3) The material used is a linear elastic material with Young’s modulus  $E$ .
- (4) The elastic axial extension of the beams is neglected.

Figure 9(a) gives the main variables representing the dimensions of the mechanism used in the model and Table 3 gives the value of these dimensions. The stiffness of the double parallelogram mechanism can be written as [20]

$$k_p = \frac{48EI}{\ell^3} \left( 1 - \frac{N}{N_0} \right) \quad (4)$$

where

$$N_0 = \frac{2\pi^2 EI}{\ell^2}, \quad I = \frac{wt^3}{12}$$

The axial load exerted on the beams is

$$N = k_1(p_1 - \lambda)$$

where  $\lambda$  is the axial displacement of the beam

$$\lambda = \frac{6x^2}{5\ell}$$

Substituting back into the equation

$$k_p = \frac{48EI}{\ell^3} \left( 1 - \frac{k_1(p_1 - \frac{6x^2}{5\ell})}{N_0} \right)$$

The effective stiffness of the mechanism is equivalent to two springs, the beams denoted by  $k_p$  and  $k_2$ , connected in parallel. Therefore, the total required force is

$$f = k_p x - k_2(p_2 - x) \quad (5)$$

We normalize the force  $f$  by the factor  $EI/\ell^2$ . This leads to the following equation:

$$\hat{f} = \frac{f\ell^2}{EI} = \frac{288}{5} \gamma \hat{x}^3 + (48 - 48\gamma \hat{p}_1 + \hat{k}_2) \hat{x} - \hat{k}_2 \hat{p}_2 \quad (6)$$

**Table 3** Dimensions used for FEM simulation

Parameter	Value	Parameter	Value
$\ell$	120 (mm)	$t$	0.2 (mm)
$w$	10 (mm)	$E$	210 (GPa)
$k_1$	5 (kN/m)	$k_2$	30 (N/m)

where

$$\hat{x} = \frac{x}{\ell}, \quad \hat{p}_1 = \frac{p_1}{\ell}, \quad \hat{p}_2 = \frac{p_2}{\ell}, \quad \gamma = \frac{k_1 \ell}{N_0}, \quad \hat{k}_2 = \frac{k_2 \ell^3}{EI}$$

The roots of equation determine the number of stable states of the mechanism. On normalizing the equation by the first coefficient, it can be rewritten as

$$\hat{x}^3 + \left( \frac{5}{6\gamma} - \frac{5}{6} \hat{p}_1 + \frac{5\hat{k}_2}{288\gamma} \right) \hat{x} - \frac{5\hat{k}_2 \hat{p}_2}{288\gamma} = 0 \quad (7)$$

The number of the real roots is determined by the discriminant which can be written as

$$\Delta = -4 \left( \frac{5}{6\gamma} - \frac{5}{6} \hat{p}_1 + \frac{5\hat{k}_2}{288\gamma} \right)^3 - 27 \left( \frac{5\hat{k}_2 \hat{p}_2}{288\gamma} \right)^2 \quad (8)$$

In order to have more than one root, i.e., multistability, the discriminant  $\Delta$  needs to be positive. This condition can be written as

$$\hat{p}_2 < \left| \frac{576\gamma}{15\sqrt{3}\hat{k}_2} \left( \frac{5}{6} \hat{p}_1 - \frac{5}{6\gamma} - \frac{5\hat{k}_2}{288\gamma} \right)^{3/2} \right| \quad (9)$$

This equation represents the stability boundary between monostable and bistable configurations. This is equivalent to the function  $\Phi$  discussed in Sec. 1. In order to have real value, the following condition has to be satisfied:

$$\hat{p}_1 > \left( \frac{1}{\gamma} + \frac{\hat{k}_2}{48} \right) \quad (10)$$

Therefore, once both conditions in Eqs. (10) and (9) are satisfied, the mechanism exhibits bistability behavior.

The positions of the stable states,  $s_1$  and  $s_2$ , and unstable state,  $u$ , are the roots of the cubic polynomial given in Eq. (6), where the mechanism position at the roots  $x_{s1}$  and  $x_{s2}$  corresponding to  $s_1$  and  $s_2$ , respectively, and the mechanism position of the root  $x_u$  corresponds to  $u$ .

The stiffness of the mechanism is the first derivative of the force, given in Eq. (6), with respect to  $\hat{x}$  such that

$$\hat{k} = \frac{864}{5} \gamma \hat{x}^2 + 48 - 48\gamma \hat{p}_1 + \hat{k}_2 \quad (11)$$

The stiffness of the mechanism at stable and unstable states can be evaluated at the position of the roots  $s_1$ ,  $s_2$ , and  $u$ .

**Remark IV:** The stiffness of the mechanism is independent of displacement  $p_2$ .

## 4 Mechanism Behavior With Respect to Programming Input

The stability behavior of a PMM can be determined by calculating its strain energy, which depends on the value of  $p_1$  and  $p_2$ . Figure 11 illustrates the normalized force for different values of  $p_1$  and  $p_2$ . As discussed in our previous work [16], the qualitative behavior of PMM can be described in terms of the programming diagram, bifurcation diagrams, and stiffness maps. These diagrams are essential to illustrate the operation of mechanism as reconfigurable logic gate as it will be given in Sec. 6.

**4.1 Programming Diagram.** The programming diagram gives the relation between the number of stable states and  $p_1$  and  $p_2$ , as illustrated in Fig. 12(a). The values of  $p_1^{cr}$  and  $p_2^{cr}$  representing the curve  $\Phi$  are highlighted in Fig. 12(b). At  $p_2 = 0$ , the mechanism is bistable when  $p_1 > p_1^{cr}$ . Otherwise, it is a monostable mechanism.

If  $|p_2| < p_2^{cr}$ , the mechanism is bistable for  $p_1 > p_1^{cr}$ . The values of  $p_1^{cr}$  and  $p_2^{cr}$  representing the stability boundaries are given by Eqs. (10) and (9).

To describe the impact of  $p_1$  and  $p_2$  on the mechanism stability behavior qualitatively, we use both bifurcation and stiffness diagrams.

**4.2 Bifurcation Diagram.** A bifurcation diagram gives the relation between the position of stable and unstable states with the programming inputs. Since we have two programming inputs, we fix one of the programming inputs and vary the other to simplify the analysis of the mechanism behavior.

Figure 13 illustrates the impact of  $p_1$  on the position of the stable and unstable states for given  $p_2$ . At  $p_2 = 0$ , the mechanism acts as buckled beams. One stable state exists,  $s_1$ . At  $p_1 = p_1^{cr}$ , pitchfork bifurcation occurs. The stable state becomes unstable  $u$  and bifurcates into two stable states  $s_1$  and  $s_2$ .

For non-zero  $|p_2| < p_2^{cr}$ , a saddle-node bifurcation occurs instead of a pitchfork bifurcation, at which a stable state and an unstable state emerge. For  $p_2 < 0$ , the bifurcation occurs at  $x > 0$  as shown in Fig. 13(b). Otherwise, the bifurcation node occurs for  $p_2 > 0$  at  $x < 0$  as given in Fig. 13(c). The value of  $x$  at which bifurcation occurs depends on  $p_2$ . The higher  $|p_2|$ , the higher  $|x|$ .

In Fig. 14, the bifurcation diagram of stable and unstable states with  $p_2$  for different values of  $p_1$  is shown. If  $p_1 < p_1^{cr}$ , the mechanism has one stable state  $s_1$ . As  $p_2$  increases, the position of the stable state varies linearly. As  $p_1$  increases, the relation between the position of stable states becomes nonlinear due to the softening effects of the beam under compression.

At  $p_1 = p_1^{cr}$ , bifurcation occurs; two stable states and one unstable state emerge at  $p_2 = 0$  as given in Fig. 14(b). As  $p_1$  increases, the position of the bifurcation nodes varies. It should be noted that the bifurcation node is the value of  $p_2^{cr}$ , where the mechanism switches from bistability to monostability.

If we assume that the mechanism is positioned at  $s_2$  in Figs. 13(b) and 13(c), on decreasing  $p_1$ , the mechanism position will slightly change until  $p_1$  reaches the bifurcation node. Then, the stable state  $s_2$  vanishes and the mechanism will switch to  $s_1$  releasing energy. The energy released and distance traveled by the mechanism on switching depend on  $p_2$ .

Similarly,  $p_2$  can be used to switch the mechanism between its stable states. We assume that the mechanism is placed at  $s_2$  position given in Fig. 14(c). As  $p_2$  increases, the mechanism slightly moves. Once  $p_2 > p_2^{cr}$ ,  $s_2$  vanishes and the mechanism snaps from  $s_2$  to  $s_1$ .

**4.3 Stiffness Map.** The stiffness map gives the relation between the stiffness of stable states,  $s_1$  and  $s_2$ , and unstable state  $u$  versus the programming inputs  $p_1$  and  $p_2$  as illustrated in Fig. 15.

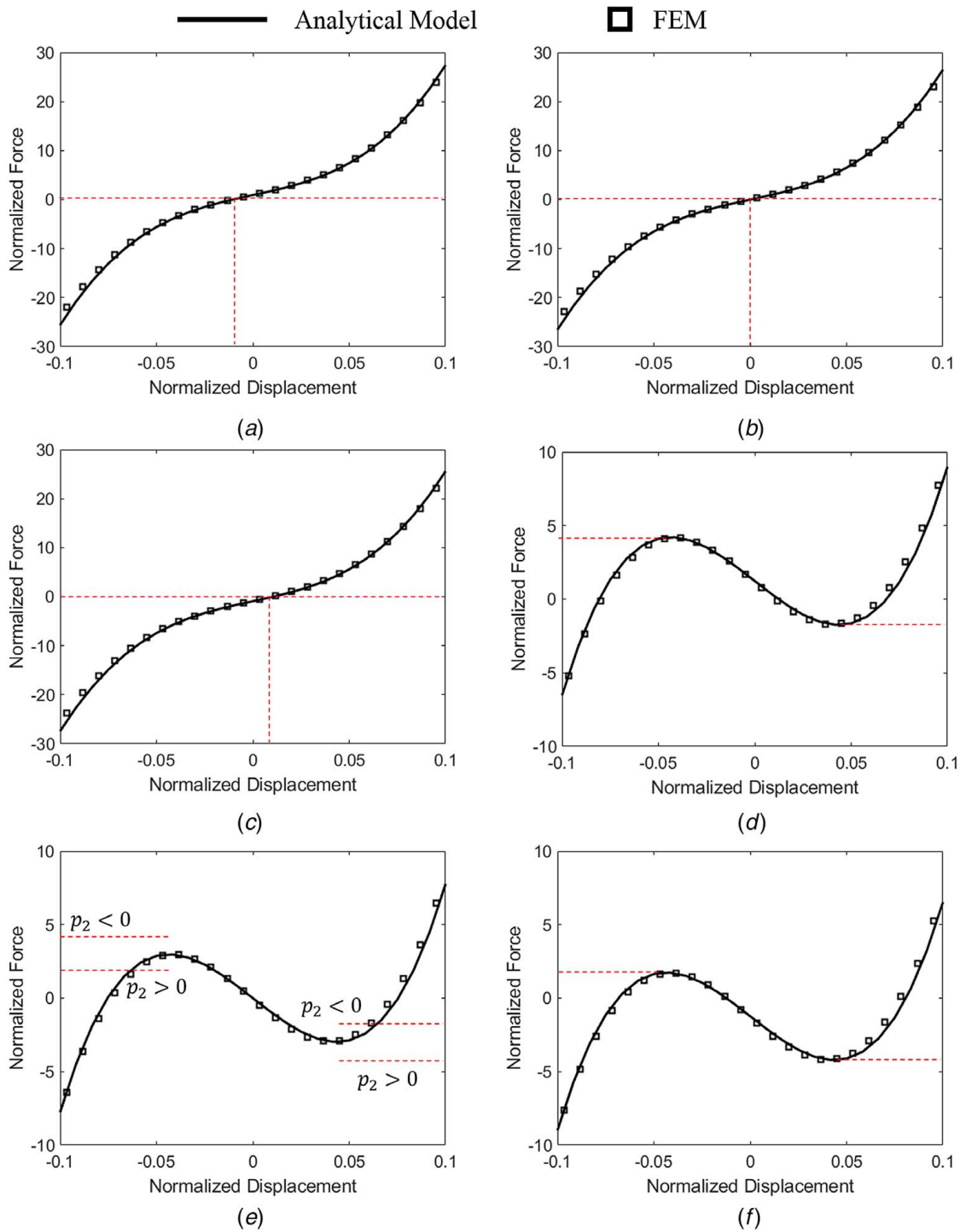
In the case of the stable state,  $s_1$ , it does exist for all values of  $p_1$  and  $p_2$ . The stiffness is always positive, implying that the position is stable.  $p_1$  has a higher impact on the stiffness. For large negative values  $p_1$ , the stiffness of EADPM is high and it decreases with increasing  $p_1$ . It reaches zero at  $p_1 = p_1^{cr}$  when  $p_2 = 0$ . After that, increasing  $p_1$  increases stiffness. The stiffness of  $s_1$  is slightly affected by  $p_2$ .

In the case of the unstable state,  $u$ , it exists only when the mechanism is bistable and its stiffness is always negative. Similar to  $s_1$ , the stiffness magnitude increases on increasing  $p_1$  and it is slightly impacted by  $p_2$  variations.

For the stable state,  $s_2$ , it does exist only when the mechanism is bistable. The stiffness varies significantly with  $p_1$  and slightly with  $p_2$ . As  $p_1$  increases, the stiffness increases.

## 5 Numerical Verification

COMSOL was used to verify our analytical computations. Table 3 gives the dimensions of the mechanism used in the simulation. The solid mechanics module is used with the linear elastic material model.



**Fig. 11 Numerical verification of the model at (a)  $p_1 = 0$  (mm),  $p_2 = -3$  (mm); (b)  $p_1 = 0$  (mm),  $p_2 = 0$  (mm); (c)  $p_1 = 0$  (mm),  $p_2 = 3$  (mm); (d)  $p_1 = 1.0$  (mm),  $p_2 = -4$  (mm); (e)  $p_1 = 1.0$  (mm),  $p_2 = 0$  (mm); and (f)  $p_1 = 1.0$  (mm),  $p_2 = 4$  (mm)**

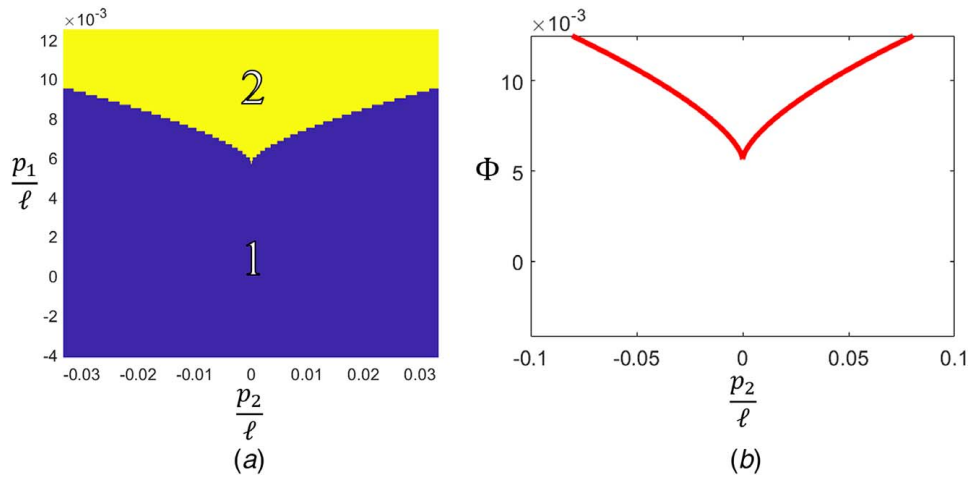
The programming inputs were applied as prescribed displacement. A parametric sweep was performed. For each step, the strain energy was calculated where geometric non-linearity was considered. A mesh convergence test was performed to verify the validity of the solution.

The number of energy minima represents the number of stable states. The mechanism reaction force and stiffness were calculated as the first and second derivatives of the strain energy with respect to the displacement. Figure 19 gives the deformation of our logic gate based on the finite element analysis.

## 6 Logic Computation

The EADPM can be used as a reconfigurable logic device as illustrated in Fig. 16. The boundary condition of the mechanism is modified by imposing displacement,  $p_1$  and  $p_2$ , representing the programming input. As discussed in Sec. 1, the programming inputs have two components, the reconfiguration component,  $r_1$  and  $r_2$ , and the logic operand  $i_1$  and  $i_2$ . The number of the stable states of the mechanism can be either “1” or “2” depending on the values of  $r_1$  and  $r_2$  with respect to the critical function,  $\Phi$ , represented by  $p_1^{cr}$  and  $p_2^{cr}$ .



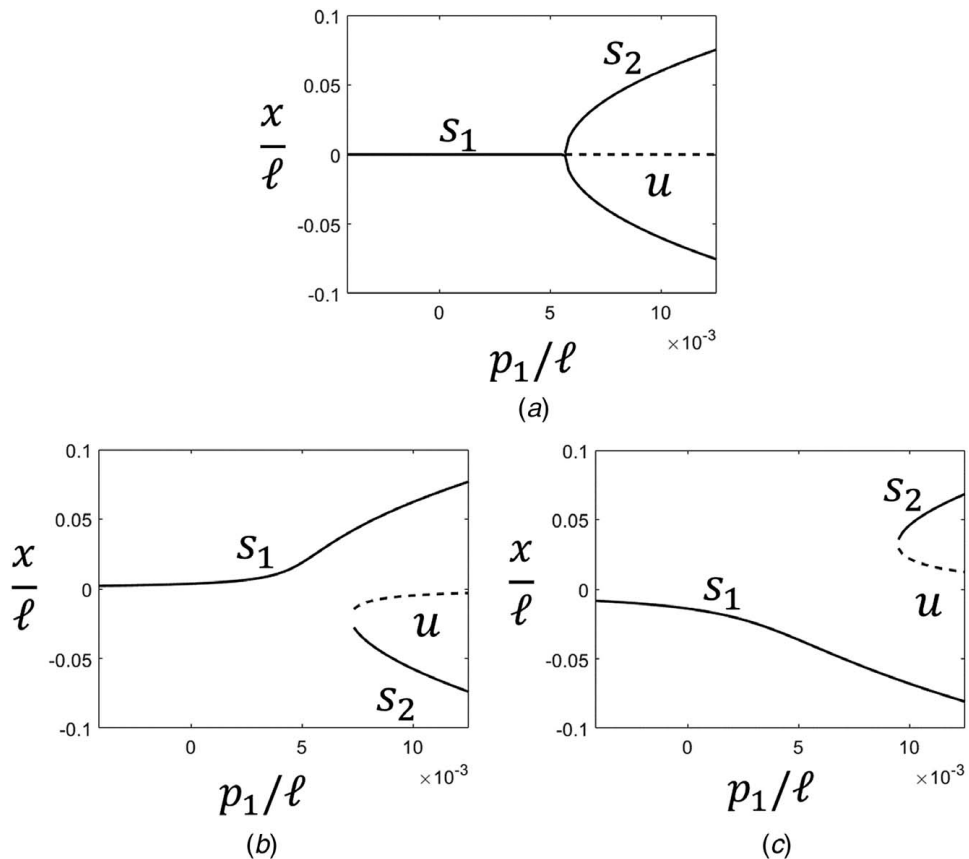


**Fig. 12 (a) Programming diagram and (b) stability boundaries, representing the function  $\Phi$  used for logic computation**

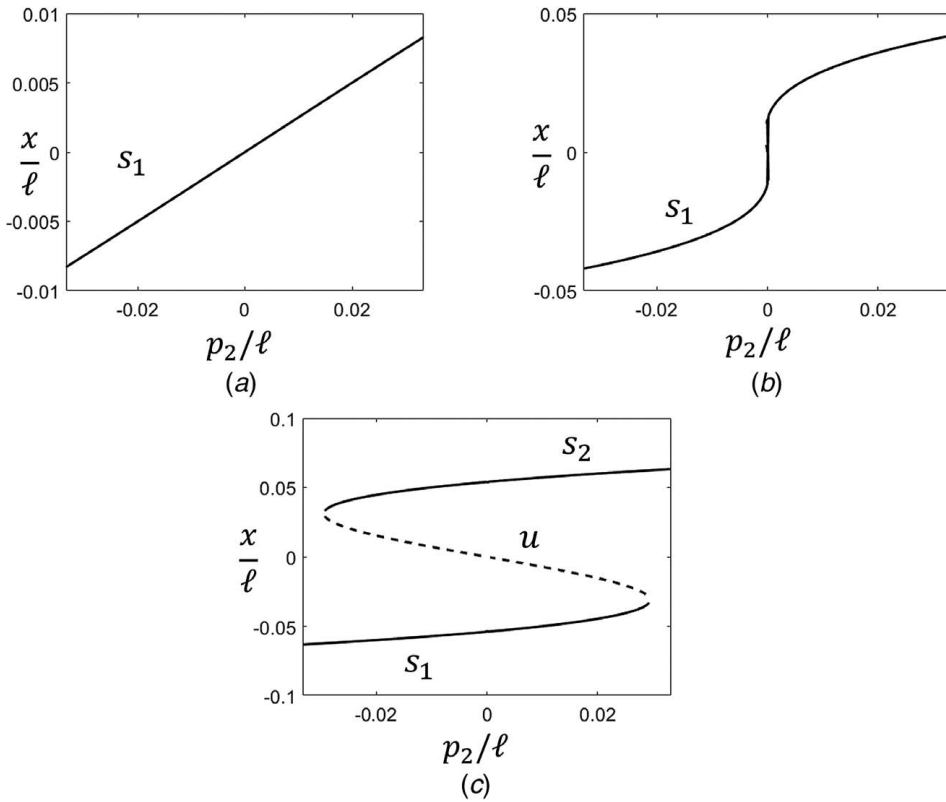
The displacement  $r_1$  and  $r_2$  set the mechanism as bistable close to the stability boundary, as given in Fig. 16(b) and the mechanism is placed at  $s_2$ . On applying  $i_1$  and/or  $i_2$ , the mechanism switches from bistability to monostability as given in Fig. 16(c). We denote the output “0,” if the mechanism maintains its state  $s_2$ , i.e., bistable. The output is “1” if the mechanism is monostable and its stable state  $s_2$  vanishes. As we change the values of  $r_1$  and  $r_2$ , the mechanism snaps and energy release will occur for different combinations of  $i_1$  and  $i_2$ . Therefore, the implemented logic function is changed.

As shown in Fig. 17, the number of implementable logic functions depends on the value of  $\alpha_1$  and  $\alpha_2$ . Therefore, we sweep  $r_1$  and  $r_2$  for given values of  $i_1$  and  $i_2$  and possible logic functions are found using our analytical model. This is done as follows:

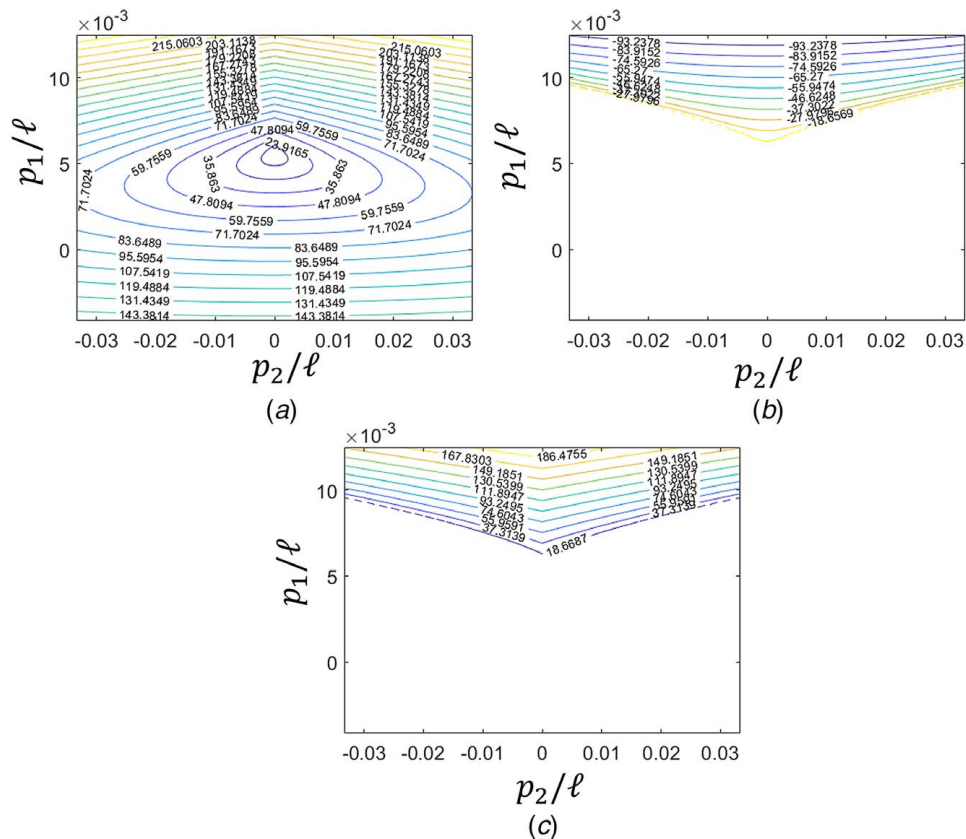
- (1) Check that the mechanism is bistable at  $r_1$  and  $r_2$ .
- (2) If the mechanism is bistable, we calculate the discriminant from Eq. (8) for the four possible values of the input.
- (3) If the discriminant for any of the four values is not positive, it indicates monostability and the output is “1” for this value.



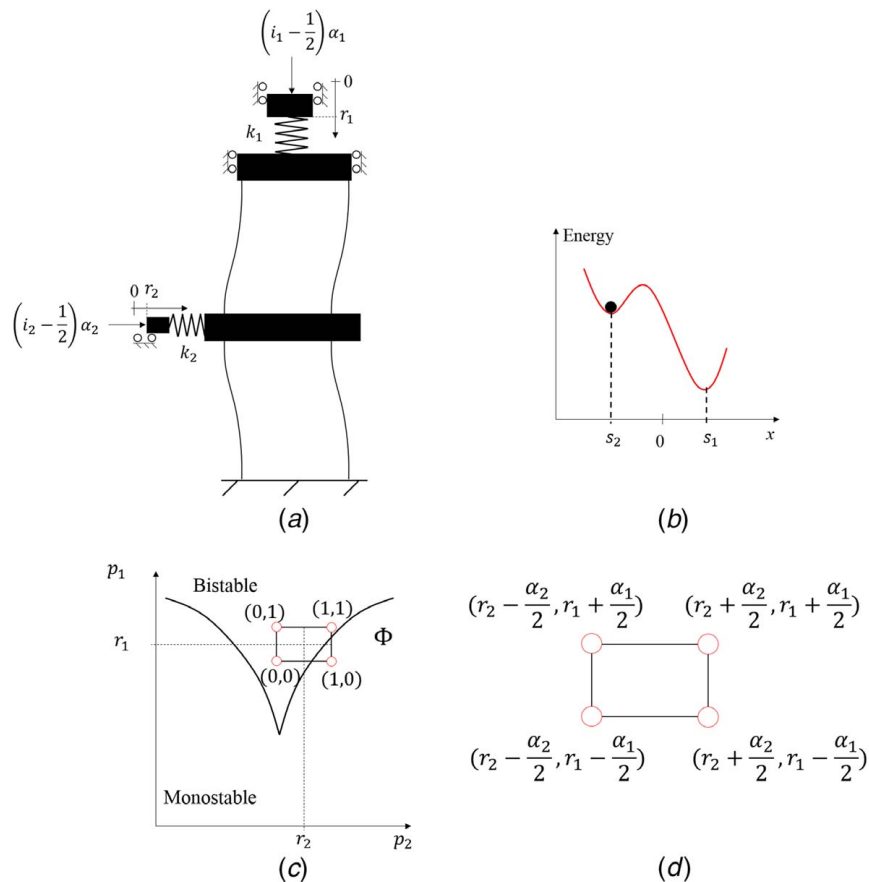
**Fig. 13 Bifurcation diagram for stable and unstable states as a function of  $p_1$  at (a)  $p_2 = 0$  (mm), (b)  $p_2 = 1$  (mm), and (c)  $p_2 = -1$  (mm)**



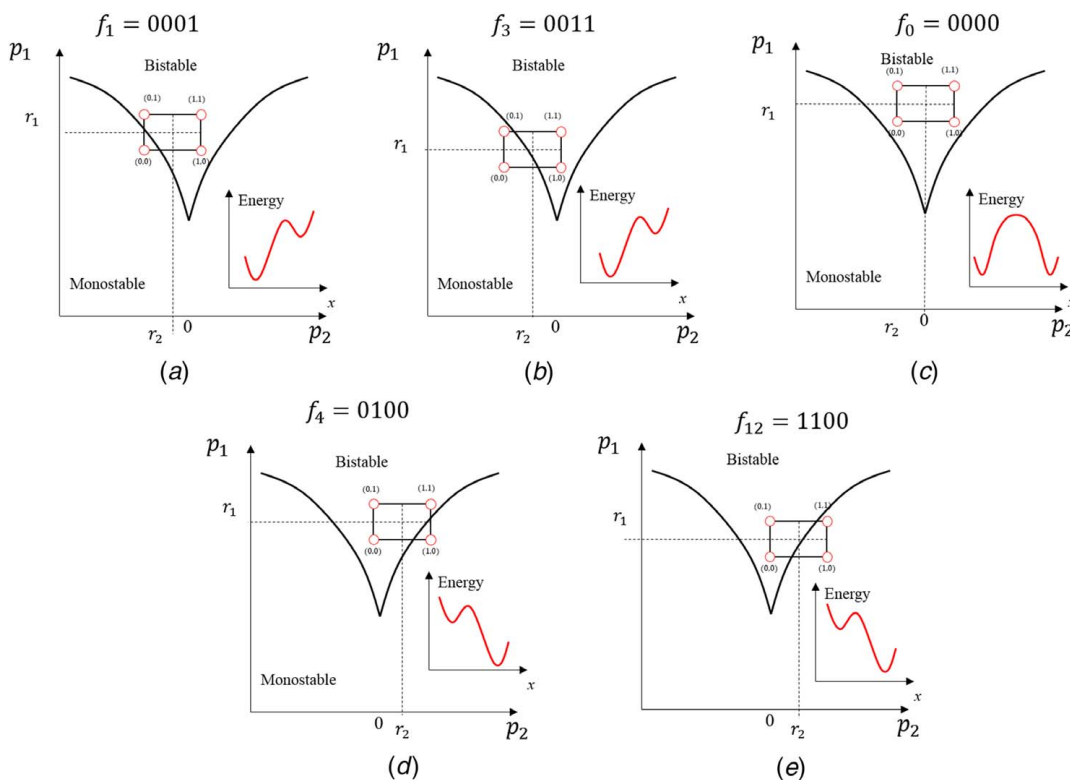
**Fig. 14** Bifurcation diagram for stable and unstable states as a function of  $p_2$  at (a)  $p_1 = 0.2$  (mm), (b)  $p_1 = 0.7$  (mm), and (c)  $p_1 = 1$  (mm)



**Fig. 15** Stiffness maps as a function of the programming inputs for (a)  $s_1$ , (b)  $u$ , and (c)  $s_2$



**Fig. 16 Configuration of the EADPM for implementing logic operations: (a) mechanism, (b) energy profile corresponding to the mechanism deformation, (c) input values on the programming diagram, and (d) rectangle representing the four discrete values of the operands**



**Fig. 17 Possible logic functions implemented by the EADPM for different values of  $r_1$  and  $r_2$ : (a) NOT ( $i_2$  OR  $i_1$ ), (b) NOT  $i_2$ , (c) False, (d)  $i_2$  OR (NOT  $i_1$ ), and (e) NOT  $i_2$**

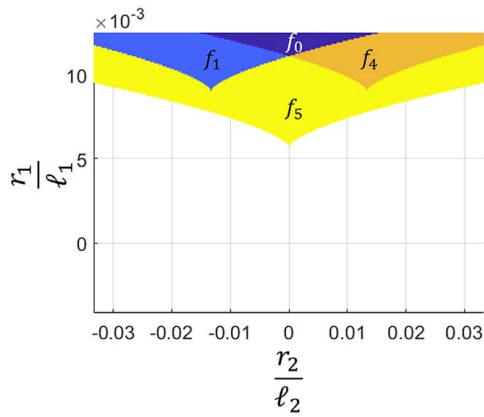


Fig. 18 Reconfiguration diagram for  $\alpha_1 = 1.6$  (mm) and  $\alpha_2 = 6$  (mm) based on the analytical model

- (4) A reconfiguration diagram relating the implementable function with the set component of programming input,  $r_1$  and  $r_2$ , is calculated.

Figure 18 shows the reconfiguration diagram for certain values  $i_1$  and  $i_2$  where the functions  $f_i$  are given in Table 1.

We built a demonstrator of the EADPM out of plastic to illustrate the different logic functions. Figure 19 shows the mechanism

deformation based on numerical and experimental demonstration. The programming inputs are applied via a slider and a cam, where the position of the sliders gives the set component,  $r_1$  and  $r_2$ , and the position of the cams represents the logic operands,  $i_1$  and  $i_2$ . We verified that  $f_0$ ,  $f_4$ , and  $f_5$  are implementable when  $r_1$  is positive. This is illustrated by the timing diagram in Fig. 20.

## 7 Future Work

We plan to use the discretization afforded by the reconfiguration diagram to construct a PMM with purely discrete reconfiguration input. We also plan to design new PMMs having different programming maps such that more of the possible 16 logical gates can be realized by the same mechanism. We will then combine mechanisms in order to implement more complex computations.

## 8 Conclusion

This paper provides new concepts to implement mechanical computation. We present a novel geometric method to construct a reconfigurable logic gate. We further construct a new programmable multistable mechanism (PMM), the EADPM, to generate the geometric data for a reconfigurable logic gate. Based on our analytical calculations, 9 of 16 possible implementable logic operations can be constructed using this mechanism. We gave a complete qualitative analysis of the mechanism's stability behavior. The analytical

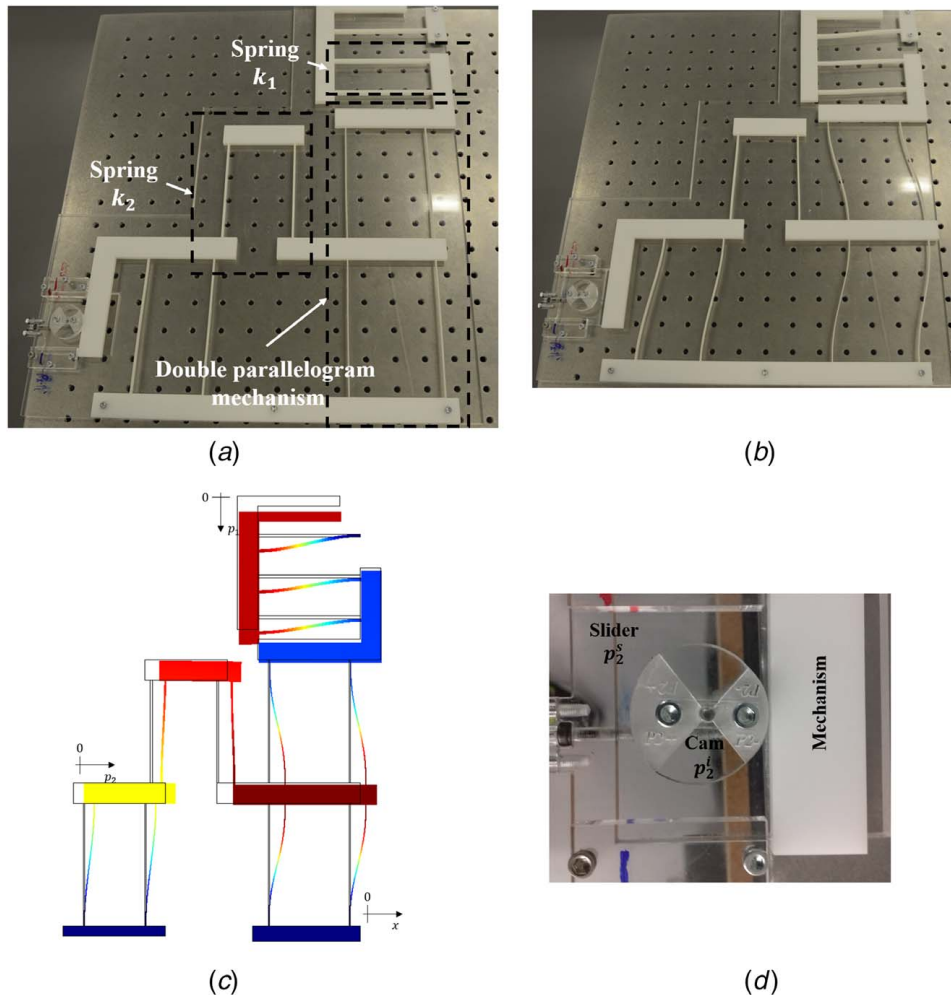
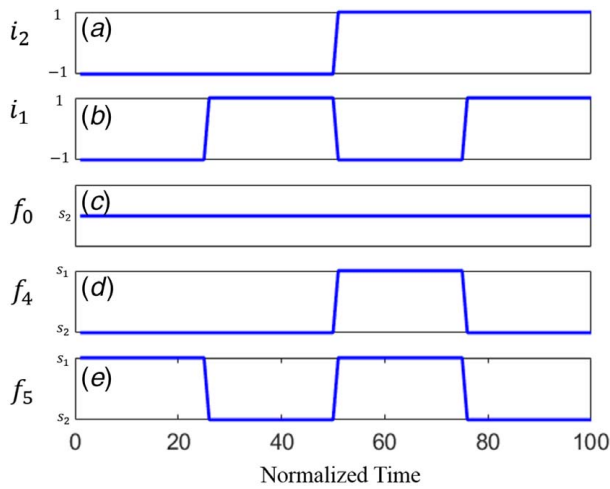


Fig. 19 (a) Physical demonstrator, (b) deformed in a stable state, (c) FEM simulation of the mechanism deformation, and (d) cam and slider for imposing  $i_2$  and  $r_2$ , respectively



**Fig. 20** Timing diagram based on experimental demonstration for (a)  $i_1$ , (b)  $i_2$ , (c)  $f_0$  at  $r_1 = 12$  (mm),  $r_2 = 5$  (mm); (d)  $f_4$  at  $r_1 = 8$  (mm),  $r_2 = 5$  (mm), and (e)  $f_5$  at  $r_1 = 7$  (mm),  $r_2 = 5$  (mm)

computations were verified using numerical simulations and experimental demonstration.

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