Analytic study on low-n external ideal infernal modes in tokamaks with large edge pressure gradients

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The problem of pressure driven infernal type perturbations near the plasma edge is addressed for a circular limited tokamak configuration which presents an edge flattened safety factor. The plasma is assumed to be separated by a vacuum region from a metallic wall, either ideally conducting or resistive. The dispersion relation for such type of instabilities is derived and discussed for two classes of equilibrium profiles for pressure and mass density.

1. Introduction

Attaining high performance tokamak operation regimes is of primary interest for a future fusion reactor. Such a condition is usually achieved in the so called tokamak H-mode (high confinement) regime. Besides the high confinement time, the H-mode is characterised by large pressure gradients located near the plasma boundary. These gradients favour the development of a particular kind of instability called the Edge Localised Mode (ELM). Such type of perturbations are rapid and violent bursts of energy and particles which can severely damage the plasma facing components with intolerable heat loads. An increasing interest has been therefore devoted to the study of the so called quiescent high confinement mode (QH-mode). The QH-mode regime (Burrell et al. 2002; Suttrop et al. 2003, 2005) shares with the H-mode a large edge pressure pedestal (edge transport barrier) and high energy confinement time but without the presence of ELMs. These are replaced by a less dangerous continuous magnetohydrodynamic (MHD) activity called Edge Harmonic Oscillation (EHO). The energy loads deposited by EHOs are much lower compared to the ones associated with ELMs. EHOs have low-n toroidal number (e.g. n = 1, 2, 3 while ELMs are instead characterised by large n values) and are always experimentally observed during the QH-mode operation (Burrell et al. 2002; Solano et al. 2010; Burrell et al. 2001, 2005; Suttrop et al. 2004).

These low-n oscillations have been linked with kink/peeling modes (Connor et al. 1998) which are proposed as a possible candidate for the explanation of the appearance of these perturbations. Linear and nonlinear simulations of QH-mode DIII-D plasma discharges showed that kink/peeling modes are the main unstable modes in the nonlinear phase whose saturation leads to a three dimensional stationary state with toroidal periodicity characterised by a low-n number (generally n=1,2) (Liu et al. 2015). These low-n modes

are not the linearly most unstable modes in the linear phase, but they are driven by the nonlinear coupling with medium- $n (\sim 3, 4, 5)$ harmonics (Liu et al. 2015).

Steep edge pressure gradients are associated in the low collisionality regime with a large edge bootstrap current contribution which produces an edge flattening of the safety factor q profile. Numerical studies of low-n MHD modes in QH regime with a plateau in q near the edge, corresponding to the peak of the bootstrap current, have been found to have infernal-like features (Zheng et al. 2013a,b). Indeed under these conditions, i.e. large pressure gradients and q flat over and extended region, it is likely that infernal type instabilities develop. These instabilities are characterised by a toroidicity induced coupling between neighbouring Fourier harmonics. Three dimensional free boundary MHD equilibria simulations of JET and TCV-like plasmas, in which a large edge bootstrap current flattens the safety factor, recovered saturated ideal kink/peeling structures (Cooper et al. 2016b,a, 2015). The computed equilibrium state is characterised by a distorted boundary with a dominant n=1 Fourier component where the corrugation is driven mainly by non axisymmetric components of the parallel current density.

Thus the main aim of this work is to study analytically the stability properties against infernal modes of MHD equilibria which present a local flattening of the safety factor close to the plasma boundary associated with large pressure gradients. We assume a vacuum region separating the plasma and the metallic wall. The analysis of the perturbation is split into various regions, each treated separately. The eigensolutions for the Fourier modes in each region are matched with the appropriate choice of the plasma-vacuum and vacuum-wall jump interface conditions. This eventually yields the dispersion relation.

The paper is organised as follows: Section 2 describes the geometry and the physical model employed for the plasma modelling. The infernal modes equations are introduced and a discussion on their validity on the applicability to our problem is given. In Sec. 3 the eigensolutions for coupled Fourier harmonics are solved for particular choice of the safety factor profile and their logarithmic jumps across the transition point between high and low shear regions are evaluated. In section 4 we solve for the vacuum perturbation and apply the appropriate boundary conditions at the plasma edge and metallic wall interfaces. The solution of the equation for the main eigenmode m_0 and the matching procedure with the high shear region eigensolutions is presented in section 5 where two classes of equilibrium profiles for temperature and mass density are considered. The dispersion relation is eventually derived and discussed in section 6 with two different wall boundary conditions. Finally the findings of this work and future outlook are summarised in section 7. The appendices include a description of inertial corrections ad residual coupling effects at the resonant surface of the $m_0 - 1$ harmonic.

2. Physical Model

We consider a large aspect ratio tokamak of major and minor radii R_0 and a respectively ($\varepsilon = a/R_0 \ll 1$) with shifted circular toroidal surfaces. The vacuum region extends for a < r < b and for r > b + d and a metallic wall of thickness d is located at b < r < b + d. The equilibrium assumes a strong toroidal field (B_T) and a smaller poloidal field (B_T), i.e. $B_T/B_T \sim O(\varepsilon)$ with $\beta \sim O(\varepsilon^2)$ (here $\beta = p_0/B_T^2$ where p_0 is the equilibrium pressure). We use a right handed straight field line coordinate system (r, ϑ, φ) where r is a flux label with the dimensions of length, ϑ and φ are the poloidal-like (counter-clockwise) and toroidal angles respectively. The contravariant and covariant basis vectors are denoted hereafter by ∇C^i and e_{C^i} respectively, with $C^i = (r, \vartheta, \varphi)$.

The magnetic field in the plasma is represented in terms of flux functions (D'haeseleer

et al. 1991):

$$\boldsymbol{B} = \boldsymbol{\nabla} f \times \boldsymbol{\nabla} \vartheta - \boldsymbol{\nabla} \psi \times \boldsymbol{\nabla} \varphi.$$

The equilibrium fluxes ψ_0 and f_0 depend only on r, and $q = f_0'/\psi_0'$ with $f_0' \approx B_0 r$ which follows from $B_T \approx R_0 B_0 / R$ (Wesson 2011) (B_0 is the magnetic field strength on the axis and the prime denotes the derivative with respect to the radial variable). Normalizing $\mu_0 = 1$, from the Ampére's law $J = \nabla \times B$, where J is the current density, we have $J_0 = J_0^{\varphi}/B_0^{\varphi} = 1/R_0[(r\mu)' + \mu]$ and $J_0' = 1/(mR_0)[(r^2k_{||,m})'/r]'$ (Hazeltine & Meiss 1992), where $\mu = 1/q$ and $k_{||,m} = m\mu - n$.

Our stability analysis is based on the following ideal MHD equations (Hazeltine & Meiss 1992):

$$\rho \left[\partial_t \boldsymbol{v} + \boldsymbol{v} \cdot \nabla \boldsymbol{v} \right] = -\nabla p + \boldsymbol{J} \times \boldsymbol{B}, \tag{2.1}$$

$$\boldsymbol{E} + \boldsymbol{v} \times \boldsymbol{B} = 0, \tag{2.2}$$

$$\partial_t p + \boldsymbol{v} \cdot \boldsymbol{\nabla} p + \Gamma p \boldsymbol{\nabla} \cdot \boldsymbol{v} = 0, \tag{2.3}$$

$$\partial_t \rho + \boldsymbol{\nabla} \cdot (\rho \boldsymbol{v}) = 0, \tag{2.4}$$

where Γ is the adiabatic index, \boldsymbol{E} is the electric field, $\boldsymbol{v} = \boldsymbol{v}_E + \boldsymbol{v}_{||}$ is the plasma MHD velocity, $\boldsymbol{v}_E = \boldsymbol{E} \times \boldsymbol{B}/B^2$ and $\boldsymbol{v}_{||} = \boldsymbol{v}_{||}\boldsymbol{b}$ with $\boldsymbol{b} = \boldsymbol{B}/B$. It is convenient to write $\boldsymbol{v} = \partial \boldsymbol{\xi}/\partial t$ where $\boldsymbol{\xi}$ is the Lagrangian perturbed fluid displacement. ρ is the mass density assumed constant, p the plasma pressure. We stress the point that we consider an ideal plasma so that the development of tearing type instabilities is prevented. By means of (2.2) we have:

$$\tilde{\boldsymbol{B}} = \boldsymbol{\nabla} \times (\boldsymbol{\xi} \times \boldsymbol{B}_0), \tag{2.5}$$

where $\tilde{\boldsymbol{B}}$ is the perturbed magnetic field and \boldsymbol{B}_0 the equilibrium magnetic field. From now on equilibrium quantities will be denoted with the subscript 0 and perturbed quantities have a dependence of the type $\exp[i(m\vartheta - n\varphi) + \gamma t]$.

For our analysis we choose a safety factor which has a local edge flattening as shown in Fig. 1. The gap between safety factor and the resonance m_0/n is denoted by δq , i.e. $\delta q = q - m_0/n$ (note that δq can be either positive or negative). It is implicitly assumed that $m_0 > 1$. In a more realistic geometry with separatrix the safety factor grows up to large values, though in a narrow region much smaller compared to the expected radial extension of the mode. This particular case is out of the scope of the present work. Nevertheless, motivated by (Zheng et al. 2013a,b; Medvedev et al. 2006), we expect that the main physical ingredients for the development of an edge infernal type MHD instability are captured. According to Turnbull & Troyon (1989) we assume that the ratio q_a/q_0 is sufficiently large (q_0 and q_a are the values of the safety factor on the magnetic axis and at the edge respectively) in order to be stable against low-n external kink modes.

Hence pressure gradients and field line bending weakening in the region of flat q allow for mode coupling between neighbouring poloidal Fourier harmonics (Hastie & Hender 1988; Waelbroeck & Hazeltine 1988; Gimblett et al. 1996; Brunetti et al. 2014). In the infernal mode analysis the presence of three Fourier modes with mode numbers $(m_0, n), (m_0 \pm 1, n)$ is usually assumed whose relative amplitude is $X_{m_0 \pm 1, n} \sim O(\varepsilon) X_{m_0, n}$, where $X = \xi \cdot \nabla r$. For sake of simplicity hereafter we will drop the subscript n and we introduce the notation $X_{\pm} = X_{m_0 \pm 1, n}$.

Thus according to figure 1, we refer to the region which extends from the magnetic axis to $r = r_* < a$ the magnetic shear is large $(q' \sim O(1))$ and the pressure gradient sufficiently small as the **sheared region**. Here mode coupling is prevented and the different Fourier

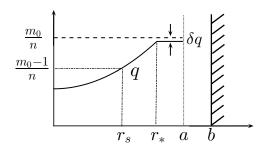


FIGURE 1. Model safety factor with the vacuum interface extending from a to b. In the edge low-shear region $(r_* < r < a)$ the q profile is close to m_0/n . The position of the $(m_0 - 1)/n$ resonant surface is highlighted.

harmonics behave independently according to (Mikhailovskii 1998; Brunetti et al. 2014):

$$\frac{d}{dr} \left[r^3 k_{||,m}^2 \frac{dX_m}{dr} \right] - r(m^2 - 1) k_{||,m}^2 X_m = 0.$$
(2.6)

It will be shown in Sec. 4 that also the vacuum magnetic perturbation is described by (2.6). Indeed in the vacuum the safety factor is expected to grow as r^2 so that we can regard also this region as a sheared region.

In low-shear region extends from r_* to the plasma edge r=a and here the safety factor is almost flat and close to m_0/n . Thus coupling between neighbouring Fourier modes can occur and the equations describing the perturbation are (Hastie & Hender 1988; Waelbroeck & Hazeltine 1988; Gimblett *et al.* 1996; Brunetti *et al.* 2014; Wahlberg *et al.* 2013):

$$\frac{d}{dr} \left[r^{3} Q \frac{dX_{m_{0}}}{dr} \right] + r \left[(1 - m_{0}^{2})Q + r \left(\frac{A_{2}}{n^{2}} \right)' - \frac{\alpha^{2}}{2} + \frac{\alpha r}{R_{0}} \left(\frac{1}{q^{2}} - 1 \right) \right] X_{m_{0}}
+ \frac{\alpha}{2} \left[\frac{r^{-m_{0}}}{1 + m_{0}} \left(r^{2 + m_{0}} X_{+} \right)' + \frac{r^{m_{0}}}{1 - m_{0}} \left(r^{2 - m_{0}} X_{-} \right)' \right] = 0,$$

$$\left[r^{-1 \mp 2m_{0}} \left(r^{2 \pm m_{0}} X_{\pm} \right)' \right]' = \frac{1 \pm m_{0}}{2} \left[\alpha r^{\mp m_{0}} X_{m_{0}} \right]',$$
(2.8)

with $Q=(\delta q/q)^2+A_1/n^2$, with $\omega_A=B_0/(R_0\sqrt{\rho})$ and $\alpha=-(2R_0p_0'q^2)/B_0^2$. Equilibrium mass density gradients are allowed since they play an important role in the determination of the pressure gradients in the narrow edge region where the perturbation we are interested in is localised. In the limit $\gamma/[\Gamma p_0/(\rho_0R_0^2)]\ll 1$ we approximate (Wahlberg et al. 2013) $A_1\simeq (\rho_0\gamma^2)/(\bar{\rho}\omega_A^2)[1+2q^2]$ and $A_2\approx A_1$ ($\bar{\rho}$ is the value of the mass density on the magnetic axis).

Equations (2.7) and (2.8) have been derived for $\beta \sim \varepsilon^2$. Then the following question arises: are they applicable when the pressure gradient increases, i.e. when $\alpha \sim 1$? We point out that from (2.7), the requirement that the inertial term is of the same order of the coupling term gives $Q \sim (\alpha \Delta r/a)^2$ where Δ is the width of the low-shear region. In the following analysis analysis we assume that $Q \sim \varepsilon^2$. If $\alpha \sim 1$ and the pressure gradient is localised within a narrow region, the assumption of concentric circular magnetic surfaces still holds (Greene & Chance 1981; Connor *et al.* 2016) and from the equation for the Shafranov shift Δ_s (assumed of order ε):

$$\Delta_s'' + 3\Delta_s'/r = 1/R_0 + \alpha/r, \tag{2.9}$$

we approximate $r\Delta_s'' \approx \alpha$ and $T_0' = -p_0'R_0/B_0 \sim \alpha$ ($T_0 = B_{0,\varphi}$ being the toroidal covariant component of the equilibrium magnetic field (Connor *et al.* 2016; Greene & Weimer 1971)).

Neglecting effects linear wrt the magnetic shear (i.e. flat q) the elements of the metric tensor in our straight field line coordinate system are evaluated up to order ε giving:

$$\begin{split} g_{rr} &= 1 + \alpha^2 \sin^2 \vartheta - 2\Delta_s' \cos \vartheta + 4(\frac{r}{R_0} - \Delta_s') \alpha \sin^2 \vartheta, \\ g_{r\vartheta} &= (r\alpha + 2\frac{r^2}{R_0} - 2r\Delta_s') \sin \vartheta + (\frac{r}{R_0} + \Delta_s') r\alpha \sin \vartheta \cos \vartheta, \\ g_{\vartheta\vartheta} &= r^2 + \frac{2r^3}{R_0} \cos \vartheta + 2r^2 \Delta_s' \cos \vartheta, \\ g_{\varphi\varphi} &= R_0^2 (1 + \frac{2r}{R_0} \cos \vartheta), \quad ^1/\sqrt{g} = \frac{1}{rR_0} (1 - \frac{2r}{R_0} \cos \vartheta), \end{split}$$

where the ratio $g_{\varphi\varphi}/\sqrt{g}$ depends only on the flux label r having used (2.9) and $\langle R^2 \rangle' \approx -R_0 \alpha$, where $\langle \cdot \rangle := ^1/_{2\pi} \int_0^{2\pi} (\cdot) d\vartheta$. Shaping effects such as ellipticity and triangularity have not been included in the flux surfaces parametrisation since their angular dependencies are of the type $\cos 2\vartheta$ and $\sin 2\vartheta$ (Connor *et al.* 2016). These corrections do not play a role in the coupling mechanism between ± 1 neighbouring Fourier sidebands. We see that g_{rr} and $g_{r\vartheta}$ are modified compared to their standard low β expressions (Brunetti *et al.* 2014; Lazzaro & Zanca 2003). The latter are recovered by allowing α to become small.

For $\alpha \lesssim 1$ we approximate $g_{rr} \simeq 1$ and at leading order the set of the equations describing the perturbation is still given by (2.7) and (2.8). Conversely assuming that $\alpha \gtrsim 1$ in a narrow region of width Δ , we introduce the following orderings:

$$r\frac{d}{dr} \sim \frac{r}{\Delta} \sim \frac{1}{\varepsilon}, \ Q \sim \varepsilon^2, \ m_0 \sim \alpha \sim 1, \ \frac{X_{\pm}}{X_{m_0}} \sim \varepsilon.$$
 (2.10)

By means of (2.10) and employing the large α metric tensor, at leading order we can derive the following coupled equations (we approximate $r_* \sim a$):

$$a^{2}[QX'_{m_{0}}]' - \frac{\alpha^{2}}{2}X_{m_{0}} + \frac{\alpha}{2}\left[\frac{aX'_{+}}{1+m_{0}} + \frac{aX'_{-}}{1-m_{0}}\right] = 0,$$
(2.11)

$$aX_{\pm}'' = \frac{1 \pm m_0}{2} [\alpha X_{m_0}]'. \tag{2.12}$$

The two simpler equations above can be used as an alternative to (2.7) and (2.8) in order to make analytically treatable more complex/realistic profiles. This will be discussed in Sec. 5.2. We arrive to the same set of equations also when we have we have $1/m \sim \Delta r/r \sim \varepsilon^{1/2}$ (in this case $X_{\pm}/X_{m_0} \sim \varepsilon^{1/2}$). Pushing further the ordering of m, i.e. $1/m \sim \varepsilon$, we enter in a purely ballooning-like configuration, where all the harmonics have the same amplitude. This problem is not addressed and is beyond the scope of these paper.

Therefore equations (2.6), (2.7) and (2.8) (or alternatively (2.11) and (2.12)) form the basis for the analysis developed in the next sections. The solutions to this set of equations must fulfil the boundary conditions imposed at the plasma-"outer world" interface at r = a. Hence the solution to the problem, which is presented in the next sections, proceeds as follows: first the equations for the perturbations are solved in the sheared and vacuum regions (with the appropriate boundary conditions). Then Eqs. (2.7) and (2.8) are solved in the low-shear region, and plasma-"outer world" boundary conditions are applied. Smooth matching of the eigensolutions across the transition points yields eventually the dispersion relation.

3. Sheared Region Eigenfunctions

The aim of this section is to derive the logarithmic derivative of the fluid displacement X_{\pm} for the neighbouring harmonics of the mode m_0 . These quantities are required in the derivation of the dispersion relation when smooth matching of the eigenfunctions at r_* is required.

We assume a precise analytic form of the safety factor so that the eigenproblem is analytically solvable in terms of the hypergeometric equation. The profile of the rotational transform in $0 < r < r_*$ is taken of the form (Mikhailovskii 1998):

$$(m_0 - 1)\mu - n = S[1 - (r/r_s)^{\lambda}], \tag{3.1}$$

where r_s is the position of the resonant surface of the mode $(m_0 - 1, n)$ (cf. Fig. 1). By requiring that $\mu(r_*) \approx n/m_0$ we obtain $S = \frac{n/m_0}{[(r_*/r_s)^{\lambda} - 1]}$. Note that in this approximation δq corrections appearing in the logarithmic derivatives of the eigenfunctions are neglected. We shall analyse in this region each harmonic separately. An alternative model for the safety factor which provides simpler expressions for \mathbb{C}_{\pm} and \mathbb{B}_{\pm} has been used in Brunetti et al. (2017).

3.1. Main harmonic m_0

We multiply (2.6) by X_{m_0} and integrate between 0 and r_* (Hazeltine & Meiss 1992; Mikhailovskii 1998) yielding:

$$r^{3}k_{||,m_{0}}^{2}X_{m_{0}}\frac{dX_{m_{0}}}{dr}\Big|_{0}^{r_{*}} - \int_{0}^{r_{*}}dr\left[r^{3}k_{||,m_{0}}^{2}\left|\frac{dX_{m_{0}}}{dr}\right|^{2} + r(m_{0}^{2} - 1)k_{m_{0},m_{0}}^{2}|X_{m_{0}}|^{2}\right] = 0, (3.2)$$

where the boundary condition $X_{m_0}(0) = 0$ is assumed. Since $[r^3 k_{||,m_0}^2 X_m \frac{dX_m}{dr}]_{r_*} \sim k_{||,m_0}(r_*)^2 \ll 1$ (with the reasonable assumption that the derivatives are not diverging), we are left with an integral of positive terms which must be zero. The only possibility is that the function under the sign of integration is vanishing, this is:

$$X_{m_0} = 0. (3.3)$$

We point out that this analysis is valid for a generic safety factor. This is in accordance with numerical calculations presented e.g. in Zheng et al. (2013a,b). Note that the equation above still holds if the $q = m_0/n$ surface is crossed, viz. $\delta q > 0$, if the resonant point of the main m_0 mode (to whom we refer with r_m) is not far from r_* (i.e. $r_m \approx r_*$) (Gimblett et al. 1996).

3.2. Lower sideband $(m_{-} = m_0 - 1)$

With the choice of the rotational transform given by (3.1), the expressions for the sidebands are readily obtained (with the constraint $X_{\pm}(0) < \infty$). Introducing the variable $z = (r/r_s)^{\lambda}$, when z < 1, the solution of (2.6) for the lower sideband fulfilling the boundary condition on the magnetic axis is (Mikhailovskii 1998; Kuvshinov & Mikhailovskii 1991; Brunetti *et al.* 2014):

$$X_{-} = A_1 z^{(m_{-}-1)/\lambda} (1-z)^{-1} F(\eta, \zeta; \eta + \zeta + 1; z)$$
(3.4)

where F is the hypergeometric function (see Abramowitz & Stegun 1968, p. 555) and we defined $\eta = (m_- - \bar{m}_-)/\lambda$, $\zeta = (m_- + \bar{m}_-)/\lambda$, $\bar{m}_- = \sqrt{m_-^2 + 2\lambda + \lambda^2}$. Conversely, when z > 1, the solution of (3.3) reads (Mikhailovskii 1998; Kuvshinov & Mikhailovskii

1991; Brunetti et al. 2014):

$$X_{-} = \frac{z^{-(1+\bar{m}_{-})/\lambda}}{z-1} \left(A_{2}^{*}F\left(\zeta, -\eta; 1+\zeta-\eta; 1/z\right) + B_{2}^{*}z^{\zeta-\eta}F\left(-\zeta, \eta; 1+\eta-\zeta; 1/z\right) \right)$$
(3.5)

where
$$A_2^* = -A_2 \frac{\eta \zeta \Gamma(-\eta) \Gamma(\zeta)}{\Gamma(1-\eta+\zeta)}$$
 and $B_2^* = -B_2 \frac{\eta \zeta \Gamma(\eta) \Gamma(-\zeta)}{\Gamma(1+\eta-\zeta)}$.

The asymptotic behaviour of these functions close to r_* , depends on the ratio B_2/A_2 . Neglecting for sake of simplicity inertial correction in this layer, B_2/A_2 is found by imposing that for an ideal mode the displacement is finite at its own rational surface (modifications of the ratio B_2/A_2 due to inertial corrections or residual coupling effects are discussed in Appendix A). Thus we immediately obtain $B_2/A_2 \rightarrow -1$ and $A_1 = 0$.

In the limit $(r_s/r_*)^{\lambda} \ll 1$, far from the resonant surface $(z \gg 1)$, we have:

$$X_{-} \sim \left(\frac{r}{r_{*}}\right)^{-(\bar{m}_{-}+\ell)} + C_{0}\left(\frac{r}{r_{*}}\right)^{\bar{m}_{-}-\ell},$$
 (3.6)

with $C_0 = -\frac{\Gamma(\eta)\Gamma(-\zeta)\Gamma(1-\eta+\zeta)}{\Gamma(-\eta)\Gamma(\zeta)\Gamma(1+\eta-\zeta)} \left(r_*/r_s\right)^{2\bar{m}_-}$ and $\ell = \lambda + 1$. Thus by means of (3.6) it is straightforward to obtain:

$$\mathbb{C}_{-} = \frac{r_* X'_{-}(r_*)}{X_{-}(r_*)} = (\bar{m}_{-}) \frac{C_0 - 1}{C_0 + 1} - \ell. \tag{3.7}$$

When $(r_s/r_*)^{\lambda} \sim 1$ it is possible to show that $\mathbb{C}_{-} \sim O(z-1)$. Since generally speaking the ratio $(r_s/r_*)^{\lambda}$ is of order of unity, in the numerical computation of the dispersion relation we shall use the complete expression (3.5).

3.3. Upper sideband $(m_{+} = m_0 + 1)$

It is easy to show that with the safety factor given by (3.1) the resonant surface of the mode $(m_0 + 1, n)$ occurs at $r_+ = r_s \left[1 + \frac{2m_0[(r_*/r_s)^{\lambda} - 1]}{(m_0 + 1)}\right]^{1/\lambda}$. The expression for the upper sideband reads:

$$X_{+} \sim \tilde{z}^{(m_{+}-1)/\lambda} (1-\tilde{z})^{-1} F(\tilde{\eta}, \tilde{\zeta}; \tilde{\eta} + \tilde{\zeta} + 1; \tilde{z}),$$
 (3.8)

where $\tilde{z} = (r/r_+)^{\lambda}$, $\tilde{\eta} = (m_+ - \bar{m}_+)/\lambda$, $\tilde{\zeta} = (m_+ + \bar{m}_+)/\lambda$, $\bar{m}_+ = \sqrt{m_+^2 + 2\lambda + \lambda^2}$. Hence if $(r_*/r_s)^{\lambda} \gg 1$ and $m_0 \gg 1$ then $r_+/r_* \sim 2^{1/\lambda}$ so that from (3.8) we obtain:

$$\mathbb{C}_{+} = \frac{r_{*}X'_{+}(r_{*})}{X_{+}(r_{*})} \approx (m_{+} - 1) + \lambda + \frac{\lambda \tilde{\eta}\tilde{\zeta}}{1 + \tilde{\eta} + \tilde{\zeta}} \frac{F(\tilde{\eta} + 1, \tilde{\zeta} + 1; \tilde{\eta} + \tilde{\zeta} + 2; \frac{1}{2})}{2F(\tilde{\eta}, \tilde{\zeta}; \tilde{\eta} + \tilde{\zeta} + 1; \frac{1}{2})}.$$
 (3.9)

Conversely in the limit $(r_*/r_s)^{\lambda} \sim 1 + \delta$ with $\delta \ll 1$ we have $(r_+/r_*)^{\lambda} \sim 1 + \delta_*$ with $\delta_* = \frac{m_0 - 1}{m_0 + 1} \delta$, which yields:

$$\mathbb{C}_{+} \approx \frac{\lambda}{\delta_{+}} + m_{+} - 1 - \lambda - \lambda \tilde{\eta} \tilde{\zeta} [2\gamma_{E} + \Psi(\tilde{\eta} + 1) + \Psi(\tilde{\zeta} + 1) + \ln \delta_{*}]. \tag{3.10}$$

In order to avoid approximations which could introduce unphysical behaviours, as in the case for the lower sideband, the full expression for X_+ (cf. Eq. (3.5)) is preferred when the growth rate is computed numerically.

In the next sections the quantities \mathbb{C}_{\pm} will be matched to the low-shear region solutions and then used for the evaluation of the dispersion relation.

4. Vacuum region

In the vacuum region the magnetic field must fulfil the conditions $\nabla \times \mathbf{B} = \nabla \cdot \mathbf{B} = 0$. Hence we write $\mathbf{B} = \nabla \chi$ with the constraint $\nabla^2 \chi = 0$ (Wesson 1978). In large aspect ratio and under the assumption m > n for each Fourier harmonic, the equation determining the mth component of the vacuum perturbation reads:

$$r(r\chi_m')' - m^2 \chi_m = 0.$$

Recalling that $\tilde{B}^r = \chi'$, this gives $\tilde{B}^r \sim (r/b)^{-m-1} - D(r/b)^{m-1}$ for a < r < b where D is a constant determined by the boundary conditions at the plasma-metallic wall interface. In the region r > b + d the solution of the vacuum perturbation is written in terms of modified Bessel functions (N.Lashmore-Davies 2001). However for $r \gtrsim b + d$ the behaviour of the radial perturbed magnetic field is well approximated by $\tilde{B}^r \sim (r/b)^{-m-1}$ (Mikhailovskii 1998; N.Lashmore-Davies 2001).

By means of the Faraday's law $E = \eta J$, and assuming that the radial derivatives of the perturbation are dominant, the equation for the perturbation within the wall is:

$$\frac{d^2\tilde{B}^r}{dr^2} = \sigma\gamma\tilde{B}^r. \tag{4.1}$$

In the thin wall approximation $(d/b \ll 1)$ (Gimblett 1986) we integrate (4.1) across the wall, so that $[r(\tilde{B}^r)'/\tilde{B}^r]_b^{b+d} = \frac{\gamma}{\omega_A} S_w(d/b)$ with $S_w = \sigma b^2 \omega_A$. Here ω_A is computed in the plasma core. Matching the solution in the regions r < b and r > b+d and employing the wall jump condition yield D = F/(F+2m) where $F = \frac{\gamma}{\omega_A} S_w(d/b)$. Note that if we consider the case of a perfectly conducting wall (i.e. $\eta \to 0$, $S_w \to \infty$) we must have D = 1, hence $\tilde{B}^r = 0$ for any m which corresponds to the condition $\hat{n} \cdot \mathbf{B} = 0$ where \hat{n} is the normal vector pointing outward the r = a surface (we identify $\hat{n} \equiv \nabla r$) (Bernstein et al. 1958; Freidberg 1987; Wesson 1978).

The jump condition at the plasma-vacuum interface is (Bernstein *et al.* 1958; Freidberg 1987):

$$[\hat{\boldsymbol{n}} \cdot \boldsymbol{B}]_a = 0, \tag{4.2}$$

where $\llbracket \cdot \rrbracket_a = (\cdot)_{a+\delta} - (\cdot)_{a-\delta}$ with $\delta \to 0$. By means of (2.5) we can extend the definition of perturbed displacement X outside the plasma, i.e. we write \tilde{B}^r in terms of X. This yields $\tilde{B}^r \sim k_{||,m}X$ so that since \tilde{B}^r must be continuous (cf. Eq. (4.2)), X also is continuous since $k_{||}$ is continuous by hypothesis. It follows that the vacuum perturbation fulfils equation (2.6). Thus it is easy to see that in the vacuum for a generic Fourier mode m we have (Mikhailovskii 1998; Wesson 1978):

$$\frac{rX'_m}{X_m}\Big|_{a+\delta} = \frac{2\mu_*}{\mu_* - n/m} - \frac{m+1 + \frac{F}{F+2m}(m-1)(a/b)^{2m}}{1 - \frac{F}{F+2m}(a/b)^{2m}},$$
(4.3)

where in the vacuum $\mu = \mu_* a^2/r^2$ (i.e. vanishing toroidal current) (Mikhailovskii 1998). Let us introduce the notation $\mathbb{B}_{\pm} = \frac{r X'_{m_0 \pm 1}}{X_{m_0 \pm 1}}\Big|_{a+\delta}$. We point out that, as calculated in section 3, the δq corrections \mathbb{B}_{\pm} are not taken into account.

For the Fourier mode m_0 , since $\mu_* - n/m_0 \sim \delta q \ll 1$ we set $X_m(a) \approx 0$. This can be deduced by the fact that close to the plasma edge we must have $X_{m_0}(r) \sim \frac{X_{m_0}(a)}{\delta q}[1 - (a/b)^{2m_0}D]$ where obviously D is computed for the mode m_0 . Since $\delta q \ll 1$ in general we must set $X_{m_0}(a) = 0$ in order to have a finite displacement at the plasma boundary following Eq. (4.2). In the case of an ideal or nearly ideal wall we note that in the vacuum region having introduced the quantity X_m , the equation describing the perturbation is

(2.6). Thus if we multiply (2.6) by X_{m_0} and integrate by parts from a to b we obtain (3.2) with the replacements $r_* \to a$ and $a \to b$. Since $k_{||,m_0}^2(a) \ll 1$ and $X_{m_0}(b) = 0$ eventually we obtain $X_{m_0} = 0$. We shall still approximate $X_{m_0}(a) \approx 0$ when the resonance $q = m_0/n$ is in the vacuum gap if the resonant point is sufficiently close to a.

As in the treatment of the sheared region, the logarithmic derivatives of the sideband harmonics are matched with the solutions in the low-shear region when the dispersion relation is derived. This will be shown in the next section.

5. Low-shear region matching and dispersion relation

In this section we solve for the main mode and the sideband harmonics deriving eventually the dispersion relation. In this region of width $a-r_*=\Delta\sim\varepsilon\ll 1$, large pressure gradients drive large edge bootstrap current contributions which in turn flatten the safety factor. There are several choices for the equilibrium profiles for p_0 and ρ_0 (e.g. linear, piecewise continuous polynomials etc.) which allow for an exact treatment of the perturbation. Our analysis concentrates first on a case in which the profiles are step-like and then on a more realistic tanh type profiles. The step-like case has been already treated in Brunetti et al. (2017) and it turns out to be useful when toroidal rotation is considered (this is not discussed here). In the next subsection we limit to summarise the findings and to show the mathematical procedure for the derivation of the dispersion relation. Part of these techniques are employed when the tanh model is considered, though a slightly different approach must be used.

5.1. Step-like functions

In order to mimic the abrupt decrease of the pressure and mass density in the flat-q region (Burrell *et al.* 2001, 2005), following Ref. Wahlberg *et al.* (2013) we introduce step-like profiles:

$$p_0/p_* \sim \rho/\rho_0 = \Theta(r_p - r) \tag{5.1}$$

where $\Theta(x)$ is the Heaviside step function of argument x, $r_p = (a + r_*)/2$ while p_* is the value of plasma pressure at r_* . The mass density is assumed constant in $0 < r < r_*$.

By integrating once (2.8) we obtain:

$$(r^{2\pm m} X_{m\pm 1})' = r^{1\pm 2m} L_{\pm} + \frac{1\pm m}{2} \alpha r^{1\pm m} X_m,$$
 (5.2)

Integration of Eq. (2.8) across r_p gives $[(r^{2\pm m}X_{\pm})']_{r_p} = 0$ implying that in (5.2) we must have $L_{\pm}(r < r_p) = L_{\pm}(r > r_p)$, i.e. the constant L_+ (or L_-) on the left and on the right of r_p must be the same. Thus plugging (5.2) into (2.7), under the assumption $(1/q^2 - 1) \approx -1$, yields:

$$\left[r^3 Q X'_{m_0} \right]' + r \left[(1 - m_0^2) Q + \hat{\gamma}^2 \frac{r \rho'_0}{\bar{\rho}} - \frac{\alpha r}{R_0} \right] X_{m_0} + \frac{\alpha}{2} \left[\frac{r^{1+m_0} L_+}{1+m_0} + \frac{r^{1-m_0} L_-}{1-m_0} \right] = 0, \quad (5.3)$$

where $\hat{\gamma}^2 = \gamma^2 (1 + 2q^2) / (n\omega_A)^2$.

The three harmonic must be supplied with appropriate boundary conditions. The solution of the main harmonic m_0 in the sheared and vacuum regions (cf. sections 3.1 and 4) provides the constraint:

$$X_{m_0}(r_*) = X_{m_0}(a) = 0. (5.4)$$

The boundary conditions for the sideband harmonics are obtained by integrating (2.8) across r_* and a. Since the pressure and its gradient at these points is vanishingly small,

this yields:

$$\frac{rX'_{\pm}(r)}{X_{\pm}(r)}\Big|_{r\to r_{*}^{+}} = \mathbb{C}_{\pm}, \quad \frac{rX'_{\pm}(r)}{X_{\pm}(r)}\Big|_{r\to a^{-}} = \mathbb{B}_{\pm}, \tag{5.5}$$

where the quantities \mathbb{C}_{\pm} and \mathbb{B}_{\pm} have been evaluated in sections 3 and 4 respectively.

Before solving for the main harmonic we first determine the constants L_{\pm} . These are obtained by evaluating (5.2) at r_* and a and using the constraint (5.4). Since the pressure gradient is vanishing at the plasma boundary, we obtain $X_{\pm}(r_*) = r_*^{\pm m_0} L_{\pm}/(2 \pm m_0 + \mathbb{C}_{\pm})$ and $X_{\pm}(a) = a^{\pm m_0} L_{\pm}/(2 \pm m_0 + \mathbb{B}_{\pm})$. By means of (5.1), integration of Eq. (5.2) from r_* to a finally gives $\frac{r_p^{\pm m_0} L_{\pm}}{1 \pm m_0} = X_0 \frac{\hat{\beta}}{\varepsilon_p} \Lambda^{(\pm)}$ where $\hat{\beta} = 2p_* q^2/B_0^2$, $\varepsilon_p = r_p/R_0$ and (Gimblett et al. 1996):

$$\Lambda^{(\pm)} = \frac{(r_p/r_*)^{2\pm 2m_0} (1\pm m_0)[2\pm m_0 + \mathbb{C}_{\pm}][2\pm m_0 + \mathbb{B}_{\pm}]}{(\mathbb{C}_{\pm} \mp m_0)[2\pm m_0 + \mathbb{B}_{\pm}] - (\mathbb{B}_{\pm} \mp m_0)[2\pm m_0 + \mathbb{C}_{\pm}](\frac{a}{r_*})^{2\pm 2m_0}}.$$
 (5.6)

Using (5.2) and (5.3) with the profiles given in (5.1), integrating across r_p shows that the singularities arising from p_0' and ρ_0' produce discontinuities at this point of X_{\pm} , X_{\pm}' and X_{m_0}' while X_{m_0} remains continuous. By means of (5.1), the equation for X_m is greatly simplified:

$$\left[r^3 X_{m_0}''\right]' + r(1 - m_0^2) X_{m_0} = 0$$

The equation above is solved separately for $r < r_p$ and $r > r_p$ imposing continuity at r_p and the constraints (5.4), giving:

$$X_{m_0} = X_0 \times \begin{cases} \frac{\left(\frac{r}{r_*}\right)^{m_0 - 1} - \left(\frac{r}{r_*}\right)^{-m_0 - 1}}{\left(\frac{r_p}{r_*}\right)^{m_0 - 1} - \left(\frac{r_p}{r_*}\right)^{-m_0 - 1}}, & r < r_p, \\ \frac{\left(\frac{r}{a}\right)^{m_0 - 1} - \left(\frac{r}{a}\right)^{-m_0 - 1}}{\left(\frac{r_p}{a}\right)^{m_0 - 1} - \left(\frac{r_p}{a}\right)^{-m_0 - 1}}, & r > r_p, \end{cases}$$

$$(5.7)$$

Following Ref. Wahlberg *et al.* (2013), the dispersion relation is obtained by integrating (5.3) across r_p . This gives:

$$r_p [\![QX'_{m_0}]\!]_{r_p} - \left[\hat{\gamma}^2 + \hat{\beta}\right] X_0 + \left(\frac{\hat{\beta}}{\varepsilon_p}\right)^2 [\Lambda^{(+)} + \Lambda^{(-)}] X_0 / 2 = 0.$$
 (5.8)

Let us define introduce $g_{\pm} = \frac{rX'_m}{X_m}\Big|_{r_p^{\pm}}$. By means of (5.7), it is easy to show that if $r_p \approx a$ and $m_0 \sim 1$ then $g_- \approx -g_+ \approx 2a/\Delta$. Hence Eq. (5.8) becomes:

$$\frac{\hat{\gamma}^2}{2} + \left(\frac{\delta q}{q}\right)^2 = \frac{\Delta}{4a} \left[\frac{\hat{\beta}^2}{2\varepsilon_p^2} (\Lambda^{(+)} + \Lambda^{(-)}) - \hat{\beta} \right]. \tag{5.9}$$

The last term on the rhs of (5.9) corresponds to the Mercier term in (2.7) and has a weak stabilising influence. It is clear that the instability drive are the pressure gradient and the field line bending weakening. This dispersion relation has been discussed in detail in Brunetti et al. (2017). We shall now use this result as a reference for the more realistic tanh case presented in the next section.

5.2. Tanh model

In this section we decide to model p_0 and ρ_0 with more realistic smooth profiles. It is important to note that since the step at r_p is lost, in order to derive the dispersion

relation, we must adopt a different procedure compared to the one employed in the previous case.

The total pressure is written as $p_0 = n_0(T_i + T_e)$ where T_s is the temperature of the s species and n_0 the numerical density where quasineutrality has been imposed. Assuming that the electron temperature profile is proportional to the density profile, i.e. $T_e \approx T_{e0} n_0 / \bar{n}$ (\bar{n} is the value of the numerical density in the core) and $T_i \gg T_{e0}$ with $T_i' \ll 1$ we eventually obtain $p_0 \sim n_0 T_i$ and $p_0' \sim n_0' T_i$. Hence pressure and mass density have approximately the same shape (Zheng et al. 2013a,b) in qualitative accordance with experimental data (Burrell et al. 2001, 2005). Thus a more realistic choice for the profiles of p_0 and ρ_0 is the following:

$$p_0/p_* \sim \rho_0/\bar{\rho} = \frac{1}{2} \left[1 - \tanh[(r - r_p)/\delta] \right],$$
 (5.10)

where $\delta/\Delta \lesssim 1$ and r_p has been already defined in the previous section. Note that for $\delta \to 0$ we shall recover the step-like case (this will be indeed shown later).

In this region we adopt the ordering presented in (2.10), and therefore we employ Eqs. (2.11) and (2.12). As in the previous section, we Integrate once (2.12) and we plug the result into (2.11) obtaining:

$$a^{2}[QX_{m_{0}}]' + \frac{\alpha}{2} \left[\frac{\hat{L}_{+}}{1+m_{0}} + \frac{\hat{L}_{-}}{1-m_{0}} \right] = 0,$$
 (5.11)

$$aX'_{\pm} = \hat{L}_{\pm} + \frac{1\pm m}{2}\alpha X_m,$$
 (5.12)

where explicitly $Q = Z[1 - c \tanh x/\delta]$ with $Z = (\delta q/q)^2 + \hat{\gamma}^2/2$ and $c = \frac{\hat{\gamma}^2}{2Z}$. The solution of (5.11) is easily obtained and it reads:

$$X_{m_0} = c_1 + \left(c_2 + \frac{H\delta}{c}\right)\frac{x}{\delta} + c_2\left\{c\ln\left[\cosh\left(\frac{x}{\delta}\right) - c\sinh\left(\frac{x}{\delta}\right)\right]\right\},\tag{5.13}$$

where
$$x = r - r_p$$
 and $H = \frac{q^2 p_*/2}{B_0^2 Z \varepsilon} \left[\frac{\hat{L}_+/a}{1+m_0} + \frac{\hat{L}_-/a}{1-m_0} \right]$.

By integrating (2.12) across a and r_* , under the assumption that the pressure gradient is not too large at these points and employing (5.4) we find that the sidebands fulfil Eqs. (5.5). The constants $c_{1,2}$ of the main harmonic are determined by imposing the boundary conditions (5.4) yielding $(h = \Delta/2)$:

$$c_1 = \frac{hH \ln[1 + (1 - c^2)\sinh^2(h/\delta)]/2}{h/\delta - c\tanh^{-1}[c\tanh(h/\delta)]}, \quad c_2 = -\frac{hH/c}{h/\delta - \tanh^{-1}[c\tanh(h/\delta)]}.$$
(5.14)

As shown in the previous section, to compute the constants \hat{L}_{\pm} equation (5.12) is first evaluated both at r_* and a and then integrated from r_* to a yielding:

$$\hat{L}_{\pm} = \frac{\mathbb{B}_{\pm} \mathbb{C}_{\pm} (1 \pm m_0)/(2a)}{\left[\mathbb{C}_{\pm} - \mathbb{B}_{\pm} - \mathbb{B}_{\pm} \mathbb{C}_{\pm} \Delta/a\right]} \int_{r_*}^{a} \alpha X_{m_0} dr.$$

$$(5.15)$$

We immediately note that $\hat{L}_{\pm}(X_{m_0})$ are linear in X_{m_0} , i.e. for k constant $k\hat{L}_{\pm}(X_{m_0}) = \hat{L}_{\pm}(kX_{m_0})$. The expressions for \hat{L}_{\pm} are inserted into the equation for the main harmonic (5.11) and the resulting expression is divided by the real number $\int_{r_{\star}}^{a} \alpha X_{m_0} dr$. The solution to this equation is still given by (5.13) with an appropriate rescaling of the constants $c_{1,2}$ (i.e. the term H). Hence this is equivalent to solve (5.11) imposing the integral condition (Wahlberg & Graves 2007):

$$\int_{r_{*}}^{a} \alpha X_{m_0} dr = 1. \tag{5.16}$$

Equation (5.16) provides the dispersion relation with $\hat{L}_{\pm} = \frac{\mathbb{B}_{\pm}\mathbb{C}_{\pm}(1\pm m_0)/(2a)}{[\mathbb{C}_{\pm}-\mathbb{B}_{\pm}-\mathbb{B}_{\pm}\mathbb{C}_{\pm}\Delta/a]}$. Plugging

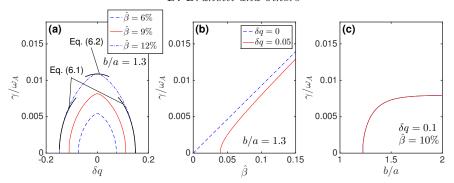


FIGURE 2. Ideal wall boundary condition growth rates for the main mode $m_0/n = 4/1$ with $\varepsilon = 1/3$, $r_s = 0.8$, $\lambda = 2$, $r_*/a = 0.95$ and $h/\delta = 3$ wrt δq (a), $\hat{\beta}$ (b) and wall position (c). Note that $\hat{\beta}$ can be rather large due to the factor q^2 . The asymptotic behaviour obtained from formulae (6.1) and (6.2) is shown in the left panel (a).

(5.13) and (5.14) into (5.16), some straightforward algebra produces the following result:

$$\frac{\hat{\gamma}^2}{2} + \left(\frac{\delta q}{q}\right)^2 = \left(\frac{\hat{\beta}}{2\varepsilon}\right)^2 \left[\frac{\hat{L}_+}{1 + m_0} + \frac{\hat{L}_-}{1 - m_0}\right] A_{\gamma},\tag{5.17}$$

where $\hat{\beta}$ has been introduced in the previous section and $A_{\gamma} = \frac{h}{c} \left[\frac{ch/\delta - \tanh^{-1}(c\tanh(h/\delta))}{h/\delta - c\tanh^{-1}(c\tanh(h/\delta))} \right]$. We shall now analyse more in detail the dispersion relation Eq. (5.17) and the associated shape of the eigenfunctions,

6. Analysis of the dispersion relation of the tanh model

The main difficulty arising in the solution of (5.17), is the dependence upon the growth rate embedded in the function A_{γ} , i.e. inside the coefficient c. Generally speaking the solution of such a dispersion relation must be tackled numerically. Nonetheless an explicit dependence of γ on the plasma parameters can be obtained for some special cases.

Let us consider first the case of a perfectly conducting wall $(\sigma \to \infty)$. If the metallic wall is directly interfaced with the plasma then $\mathbb{B}_{\pm} \to \infty$ and because $\mathbb{C}_{\pm} > 0$ we immediately have $\hat{L}_{\pm} \leq 0$. Therefore, since $A_{\gamma} > 0$, the rhs of (5.17) is negative indicating stability. Thus with ideal wall boundary conditions, a vacuum region is necessary for the instability to develop. This also suggests a threshold in the wall position for the growth rate in accordance with the results presented in Zheng et al. (2013a,b).

Let us now examine the behaviour of A_{γ} near marginal stability ($c \ll 1$) and in the strong instability region ($c \sim 1$). By taking the corresponding limits we obtain at leading order:

$$A_{\gamma} \sim h\left(1 - \frac{\tanh(h/\delta)}{h/\delta}\right), \quad c \ll 1 \left(2\delta q^2/(q\hat{\gamma})^2 \gg 1\right),$$
 (6.1)

$$A_{\gamma} \to h \left(1 - \frac{4h/\delta}{2h/\delta + \sinh(2h/\delta)} \right), \quad c \sim 1 \left(2\delta q^2 / (q\hat{\gamma})^2 \ll 1 \right).$$
 (6.2)

Thus the γ dependence in A_{γ} is removed and an explicit expression for the growth rate can be obtained. The resulting growth rates wrt the plasma parameters are shown in Fig. 2.

It is worth noticing that particular attention has to be devoted when A_{γ} is expanded near c = 1. Indeed a series expansion A_{γ} in (c - 1) cannot be performed if h/δ becomes

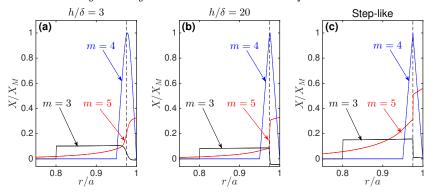


FIGURE 3. Plot of the eigenfunctions normalised wrt the maximum of the main mode (X_M) for the tanh (a)-(b) and the step-like model (c) in ideal wall boundary condition with $\varepsilon=1/3$, $\hat{\beta}=3\%$, $r_s=0.8$, $\lambda=2$, $r_*/a=0.95$ and $q_*=4$. The main mode has $m_0=4$, n=1. In panels (a) and (b) the eigenfunctions are computed for $\delta q=0.03$ corresponding to $\gamma/\omega_A\approx 1.4\times 10^{-3}$. The dashed vertical line indicates the position of the low-shear region middle point r_p . We set in the panel (a) $h/\delta=3$ while in (b) $h/\delta=20$. Qualitatively the behaviour of the step model is recovered for large h/δ . Note that the maximum of the main harmonic $(m_0=4)$ in the tanh model is slightly shifted to the right wrt r_p .

sufficiently large. Therefore we decided to retain only the first term which provides the correct asymptotic behaviour for $h/\delta \to \infty$. In such a case $(\delta \to 0)$ it is easy to see that in both cases $(c \ll 1 \text{ and } c \sim 1)$ the step-like dispersion relation Eq. (5.9) is formally recovered with the appropriate substitutions for $\Lambda^{(\pm)} \to \hat{L}_{\pm}$ and without the Mercier contribution which has been dropped due to the ordering (2.10). The shape of the eigenfunctions also qualitatively reduces to the step-like case as shown in figure 3. Differences remain due to the fact that in the system of equations (5.11) and (5.12) we dropped we terms which conversely are retained in (5.2) and (5.3). In addition the shape of the eigenfunctions depends on the value of δq (and to the corresponding growth rate), contrarily to the step case. We note that the radial structure of the main and sidebands harmonics closely resembles what has been found numerically in 3D equilibria simulations (Cooper et al. 2015, 2016b,a) and in MHD stability calculations (Medvedev et al. 2006; Zheng et al. 2013a,b).

We shall now consider the case with a resistive wall. For sake of simplicity in the following analysis we set $\omega_A = 1$. We assume that the conductivity is sufficiently large so that we can expand \mathbb{B}_{\pm} in $1/\sigma$, yielding $\mathbb{B}_{\pm} = \mathbb{B}_{\pm}|_{\sigma=\infty} + \frac{\mathbb{B}_{\pm}^w}{S_w\gamma(d/b)}$ with:

$$\mathbb{B}_{\pm}^{w} = \frac{4(m_0 \pm 1)^2 (a/b)^{2m_0 \pm 2}}{1 - (a/b)^{2m_0 \pm 2}} > 0. \tag{6.3}$$

Inserting this result into the expressions for \hat{L}_{\pm} , at leading order in $1/\sigma$ we obtain:

$$\frac{\hat{L}_{\pm}}{1 \pm m_0} \approx \frac{\mathbb{B}_{\pm}^0 \mathbb{C}_{\pm} / (2a)}{[\mathbb{C}_{\pm} - \mathbb{B}_{+}^0 - \mathbb{B}_{+}^0 \mathbb{C}_{\pm}^{\Delta/a}]} + \frac{1}{S_w \gamma} \left(\frac{(b/d) \mathbb{B}_{\pm}^w \mathbb{C}_{\pm}^2 / (2a)}{[\mathbb{C}_{\pm} - \mathbb{B}_{+}^0 - \mathbb{B}_{+}^0 \mathbb{C}_{\pm}^{\Delta/a}]^2} \right), \tag{6.4}$$

where $\mathbb{B}^0_{\pm} = \mathbb{B}_{\pm}|_{\sigma=\infty}$. The expression above is written as $\frac{\hat{L}_{\pm}}{1\pm m_0} \approx \mathscr{D}_{\pm} + \mathscr{R}_{\pm}/(S_w\gamma)$. Hence the Eq. (5.17) can be cast in the following manner:

$$\hat{\gamma} \left[\hat{\gamma}^2 - \hat{\gamma}_I^2 \right] = \gamma_w^3, \tag{6.5}$$

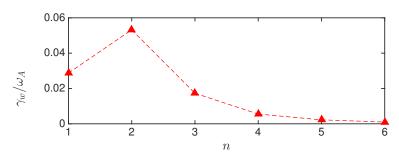


FIGURE 4. Plot of γ_w/ω_A wrt the toroidal mode number n with $\varepsilon = 1/3$, b/a = 1.3, $d/a = 10^{-2}$ $\hat{\beta} = 5\%$, $r_s = 0.8$, $\lambda = 2$, $r_*/a = 0.95$, $S_w = 10^5$ and $q_* = 4$ (here we dropped the normalisation $\omega_A = 1$). Note that γ_w/ω_A peaks for small values of n.

where $\hat{\gamma}_I^2 = 2(\hat{\beta}/2\varepsilon)^2 h[\mathcal{D}_+ + \mathcal{D}_-]$ is the growth rate with the ideal wall and:

$$\gamma_w^3 = 2\frac{\sqrt{1+2q^2}}{nS_w} \left(\frac{\hat{\beta}}{2\varepsilon}\right)^2 h[\mathcal{R}_+ + \mathcal{R}_-] > 0,$$

having assumed for sake of simplicity that $h/\delta \gg 1$, i.e. $A_{\gamma} \to h$.

Let us assume that $\hat{\gamma}_I^2 > 0$. Therefore if $\gamma_w/\hat{\gamma}_I \ll 1$, the growth rate can be written as $\hat{\gamma} = \hat{\gamma}_I + \frac{\gamma_w^3}{2\hat{\gamma}_I^2}$. Conversely if $\gamma_w/\hat{\gamma}_I \gg 1$, the growth rate is $\hat{\gamma} = \gamma_w + \frac{\hat{\gamma}_I^2}{3\gamma_w}$. In both cases the destabilising effect of the resistive wall is evident. In the contrary case, when $\hat{\gamma}_I^2 < 0$ and γ_w sufficiently small (i.e. we are in the stability region with the ideal wall) instability is still possible with growth rate $\hat{\gamma} = \gamma_w^3/|\hat{\gamma}_I^2|$. The behaviour of γ_w wrt n is shown in Fig. 4.

Although toroidal rotation effects are not considered in the present work, based on the results shown in Brunetti et al. (2017) we expect that the Doppler shift due to the toroidal flow should be included in the low-shear inertial contribution with a modification of the dispersion relation:

$$\hat{\gamma} \left[\frac{(\gamma - in\Omega)^2 (1 + 2q^2)}{n^2} - \hat{\gamma}_I^2 \right] = \gamma_w^3,$$

where Ω is the rotation frequency evaluated at r_* . It is easy to see that for sufficiently large toroidal rotation, the resistive wall effects become negligible.

7. Conclusions

In this work we addressed the linear stability properties of infernal type perturbations with a safety factor flat and close to a rational $(q \approx m_0/n)$ near the edge. Such a configuration presents a main (m_0, n) Fourier harmonic, resonant in the flat q region, which is coupled with its neighbouring sidebands $(m_0 \pm 1, n)$.

An exact analytic treatment of the magnetic perturbation in the inner region of large magnetic shear has been possible with a careful choice, though rather general, of the safety factor. In the region of the local edge flattening of the safety factor, the equilibrium profiles for pressure and mass density have been modelled with two simple classes of analytic functions. In one case (already discussed in Brunetti et al. (2017)) the step-like model has been employed. In the second case we introduced a layer ordering in the the low shear region resulting in a simplification of the coupled equations for the three harmonics. This allowed us to use a more realistic tanh model. A vacuum region with

a parabolic safety factor $(q \sim r^2)$ has been included with either ideally conducting or resistive wall boundary conditions. Each region has been analysed separately and the solutions eventually matched across the transitions points. The advantage of this choice for the equilibrium profiles, i.e. safety factor and either step or tanh-like pressure and mass density, consists in a exact mathematical description of both the eigenfunctions and the associated dispersion relation. We point out that additional corrections such as inertia and residual coupling associated with the behaviour of the sidebands inside the large shear region have been neglected, though a brief description of their effects on the shape of the eigenfunction has been given in the appendices. This dispersion relation which has been derived is sufficiently simple to show the explicit dependence of growth rate upon the engineering plasma parameters, i.e. plasma current profile and β .

In the ideally conducting wall case, the presence of a vacuum region separating plasma and wall is necessary for the instability to develop. The drive of the instability are the pressure gradients and the field line bending weakening. The shape of the eigenfunctions calculated analytically exhibit similarities with both numerical results (Zheng et al. 2013a,b; Medvedev et al. 2006) and with experimental findings (Chen et al. 2016). The finite wall conductivity has a destabilising effect, and near the ideal wall marginal stability boundary the resistive wall growth rate peaks for small values of the toroidal (also poloidal) mode numbers.

Although in the present work effects of plasma rotation have been neglected, from the results obtained in Brunetti et al. (2017) for step-like profiles, in the ideal wall case a subsonic toroidal rotation should Doppler shift the eigenfrequency without altering the stability properties. Therefore we may argue that the calculations with the more realistic tanh model presented in this work should apply also with cases in which toroidal rotation is accounted. We shall also expect that resistive wall effects become negligible for sufficiently large toroidal flows.

Sheared poloidal flow and the associated electric field effects will require further analytic investigations. Finally the effects of the separatrix may alter the jump conditions of the magnetic perturbation, resulting in a modification of the dispersion relation. Shaping effects also (mainly elongation), in particular close to the edge where they have the strongest effect, can alter the mode dynamics. It is envisaged that a numerical approach is required to address such a difficult problem.

Appendix A. Resonant layer modifications to the lower sideband Effects of inertial corrections

The quantity B_2/A_2 which appears in (3.5), depends on the growth rate γ as inertial corrections may become important when the resonant surface of the lower sideband is approached. We expand (3.4) and (3.5) about r_s giving (we use the same notation as in Ref. Mikhailovskii (1998)):

$$X_{-}(z<1) \sim \frac{1}{1-z} + \eta \zeta \ln(1-z) + \Delta_c, \quad X_{-}(z>1) \sim \frac{1}{z-1} - \eta \zeta \ln(z-1) + \Delta_p, \quad (A1)$$

where $\Delta_c = \left[\eta \zeta(2\gamma_E - 1 + \Psi(\zeta + 1) + \Psi(\eta + 1)) - \frac{m_- - 1}{\lambda}\right]$ (γ_E is the Euler-Mascheroni constant and Ψ the Digamma function (see Abramowitz & Stegun 1968, p. 253)), $\Delta_p = d_+ + \frac{B_2/A_2}{1+B_2/A_2}(d_- - d_+)$ and:

$$d_{\pm} = \eta \zeta [1 - 2\gamma_E - \Psi(\pm \zeta + 1) - \Psi(\mp \eta + 1)] \mp \frac{\bar{m}_- \pm 1}{\lambda}.$$

Equations (A1) contain a logarithmic term which is generally neglected when the inertial layer is studied in slab geometry. Following the analysis presented in Ref.

(Mikhailovskii 1998), we allow for inertial effects in (2.6) close to r_s so that $(' \equiv \frac{d}{dx})$:

$$[(1+x)^{2/\lambda+1}(x^2+\bar{\gamma}^2)X']'-(1+x)^{2/\lambda-1}\frac{m_-^2-1}{\lambda^2}[x^2+\bar{\gamma}^2]X=0,$$

where z=1+x and $\bar{\gamma}^2=\gamma^2/(S\omega_A)^2(1+2q^2)$. Let us introduce the following ordering: $x\sim\bar{\gamma}\sim\delta, \frac{d}{dx}\sim\frac{1}{\delta}$ with $\delta\ll 1$ and $\frac{m_-^2-1}{\lambda^2}\sim S\sim 1$. We write the solution as $X=X_0+\delta X_1+O(\delta^2)$ and then expand the equation above in a series of δ . Eventually we have:

$$X = c_0 - c_1/\bar{\gamma}\arctan(x/\bar{\gamma}) \pm c_3\ln(x^2 + \bar{\gamma}^2),\tag{A 2}$$

where \pm is for $x \leq 0$. As $x/\bar{\gamma} \to \infty$ the logarithmic terms in (A2) are immediately matched with (A1) by choosing $c_3 = \eta \zeta/2$, while the non logarithmic part of (A2) behaves as:

$$X \sim c_0 \pm \frac{c_1}{|x|} \left(1 - \frac{\pi}{2} |x| / \bar{\gamma} \right),$$
 (A3)

where \pm is for $x \leq 0$ as before. Matching (A 3) with (A 1) gives $\frac{\pi}{\hat{\gamma}} + \Delta_c + \Delta_p = 0$ and eventually we obtain:

$$B_2/A_2 = -\frac{1 - [\eta \zeta \cot(\pi \eta)]\bar{\gamma}}{1 - [\eta \zeta \cot(\pi \zeta)]\bar{\gamma}} \approx -1 + \hat{\gamma}\eta \zeta [\cot(\pi \eta) - \cot(\pi \zeta)],$$

where the last approximation holds if $\hat{\gamma} \ll 1$.

Allowance for residual coupling effects

We assume that a small coupling contribution remains near the resonant point r_s of the lower harmonic X_- . This corresponds to the fact that the main harmonic m_0 and pressure gradients can be non vanishing exactly for $r < r_*$. For sake of simplicity we write $m = m_0 - 1$. Thus we modify the (2.6) by adding the constant U which represents the coupling corrections similar to the ones appearing in (2.7) and (2.8):

$$\frac{d}{dr} \left[r^3 Q \frac{dX_-}{dr} \right] - r(m^2 - 1)QX_- + U = 0, \tag{A4}$$

where here $Q = k_{\parallel}^2 + \gamma^2 (1 + 2q^2) \omega_A^2$. We assume that the coupling constant U is small far from r_s , but sufficiently large close to this point.

To simplify the analysis we employ a safety factor which is constant $1/q = \mu_0$ for $0 < r < r_0$ and $1/q = \mu_* \sim n/m_0 < \mu_0$ for $r_* < r < a$, while in the region $r_0 < r < r_*$ behaves as Brunetti *et al.* (2017):

$$\mu \approx n/m_0(r_*/r)^2. \tag{A 5}$$

This corresponds to a current profile of the form (the profiles for q and J_0 are shown in figure 5):

$$R_0 J_0 = \begin{cases} 2\mu_0, & 0 < r < r_0 \\ 0, & r_0 < r < r_*, \\ 2\mu_*, & r_* < r < a, \end{cases}$$
 (A 6)

In the region $r_0 < r < r_*$, sufficiently far from r_s we neglect the terms proportional to γ , hence the solution of the equation above reads:

$$X_{-} = T_{\lessgtr} \frac{(r/r_s)^{m-1}}{k_{||}} + K_{\lessgtr} \frac{(r/r_s)^{-m-1}}{k_{||}} - \frac{U}{2m} \left[\frac{r^{m-1}}{k_{||}} \int \frac{r^{-m-1}}{k_{||}} dr - \frac{r^{-m-1}}{k_{||}} \int \frac{r^{m-1}}{k_{||}} dr \right],$$

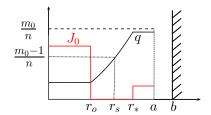


FIGURE 5. Step current model: the q profile is assumed parabolic (i.e. vanishing current) for $r_0 < r < r_*$.

where K_{\leq} and T_{\leq} are constants and the integrals in the expression above can be easily represented in terms of the Gauss hypergeometric function although a more careful treatment is needed when m is even.

When the resonant surface is approached we have:

$$X_{-}(r \leq r_{s}) = \pm \frac{(K_{\leq} + T_{\leq})}{2n|\hat{x}|} - \frac{K_{\leq}(1/2 - m) + T_{\leq}(1/2 + m)}{2n} - \frac{U}{4n^{2}r_{s}} \ln|\hat{x}|$$

$$\mp \frac{U}{4m^{2}n^{2}r_{s}|\hat{x}|} - \frac{U}{4n^{2}r_{s}} \left(\gamma_{E} - 1 + \ln 2 + \Psi(\frac{m}{2}) + \frac{1}{m} - \frac{1}{2m^{2}}\right), \quad (A7)$$

where $\hat{x} = (r-r_s)/r_s$. Far from r_s , neglecting the term proportional to U, $K_<$ is expressed in terms of $T_<$ by imposing smoothness at r_0 (if $r_0 \ll r_*$ and m_0 sufficiently large we can approximate $K_< \approx 0$). If the inertial layer is thin, we may assume that the poloidal flux $\psi_- \sim \hat{x}X_-$ is continuous across r_s . This implies that $(K_< + T_<) = (K_> + T_>)$. The part of (A 7) which does not contain the logarithm can be written as:

$$X_{-}(r \leq r_s) \sim \frac{1}{|\hat{x}|} [1 + \Delta_{\mp} |\hat{x}|],$$
 (A8)

where we defined:

$$\varDelta_{\pm} = \pm \frac{\frac{1}{2} + m + \left(\frac{1/2 - m}{1/2 + m}\right) \frac{K_{\lessgtr}}{T_{\lessgtr}} + \frac{U/T_{\lessgtr}}{2m^2 n r_s} \mathcal{H}}{1 + \frac{K_{\lessgtr}}{T_{\lessgtr}} - \frac{U/T_{\lessgtr}}{2m^2 n r_s}},$$

with $\mathcal{H} = m^2 [\gamma_E - 1 + \ln 2 + \Psi(\frac{m}{2})] + m - \frac{1}{2}$. In the inertial layer we approximate Eq. (A 4) as:

$$\frac{d}{d\hat{x}}\left[(\hat{x}^2 + \bar{\gamma})^2 \frac{dX_-}{d\hat{x}}\right] + U_1 = 0, \tag{A 9}$$

where $\bar{\gamma}^2 = \gamma^2 (1 + 2q^2)/(\omega_A m r_s \mu_s')^2$ and $U_1 = \frac{1}{r_s} U/(m r_s \mu_s')^2$. The solution of Eq. (A 9) is $X_- = c_0 + c_1 \arctan(\hat{x}/\bar{\gamma}) - \frac{U_1}{2} \ln(\hat{x}^2 + \bar{\gamma}^2)$, where $d_{0,1}$ are constants of integration. The logarithmic terms are automatically matched. If $\hat{x}/\bar{\gamma} \to \infty$, the asymptotic behaviour of the non logarithmic part of the layer solution behaves as (A 3). Matching gives $\frac{\pi}{\bar{\gamma}} + \Delta_+ + \Delta_- = 0$ (see previous section).

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