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## **Effects of episodic rainfall on a subterranean estuary**

Xiayang Yu<sup>1</sup>, Pei Xin<sup>1</sup>, Chunhui Lu<sup>1</sup>, Clare Robinson<sup>2</sup>, Ling Li<sup>3</sup>, D. A. Barry<sup>4</sup>

<sup>1</sup> State Key Laboratory of Hydrology-Water Resources and Hydraulic Engineering, Hohai University, Nanjing, China

<sup>2</sup> Department of Civil and Environmental Engineering, Western University, London, Ontario, Canada

<sup>3</sup> School of Civil Engineering, The University of Queensland, Queensland, Australia

<sup>4</sup> Laboratoire de technologie écologique (ECOL), Institut d'ingénierie de l'environnement (IIE), Faculté de l'environnement naturel, architectural et construit (ENAC), Ecole Polytechnique Fédérale de Lausanne (EPFL), Station 2, 1015, Lausanne, Switzerland

Corresponding author: Pei Xin, State Key Laboratory of Hydrology-Water Resources and Hydraulic Engineering, Hohai University, Nanjing, China. ([pei.xin@outlook.com](mailto:pei.xin@outlook.com))

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## 22 **Abstract**

23 Numerical simulations were conducted to examine the effect of episodic rainfall on  
24 nearshore groundwater dynamics in a tidally-influenced unconfined coastal aquifer, with a  
25 focus on both long- (yearly) and short-term (daily) behavior of submarine groundwater  
26 discharge (SGD) and seawater intrusion (SWI). The results showed non-linear interactions  
27 among the processes driven by rainfall, tides and density-gradients. Rainfall-induced infiltration  
28 increased the yearly averaged fresh groundwater discharge to the ocean but reduced the extents  
29 of the saltwater wedge and upper saline plume as well as the total rate of seawater circulation  
30 through both zones. Overall, the net effect of the interactions led to an increase of the SGD. The  
31 nearshore groundwater responded to individual rainfall events in a delayed and cumulative  
32 fashion, as evident in the variations of daily averaged SGD and salt stored in the saltwater  
33 wedge (quantifying the extent of SWI). A generalized linear model (GLM) along with a  
34 Gamma distribution function was developed to describe the delayed and prolonged effect of  
35 rainfall events on short-term groundwater behavior. This model, validated with results of daily  
36 averaged SGD and SWI from the simulations of groundwater and solute transport using  
37 independent rainfall datasets, performed well in predicting the behavior of the nearshore  
38 groundwater system under the combined influence of episodic rainfall, tides and density-  
39 gradients. The findings and developed GLM form a basis for evaluating and predicting SGD,  
40 SWI and associated mass fluxes from unconfined coastal aquifers under natural conditions,  
41 including episodic rainfall.

42

### 43 **Keywords**

44 Submarine groundwater discharge; Seawater intrusion; Coastal aquifer; Recharge; Numerical  
45 modeling; Density-dependent flow

46

### 47 **Key Points:**

- 48 • SGD and SWI responded to rainfall events in a delayed and prolonged fashion
- 49 • Effect of episodic rainfall on SGD and SWI was quantified using the Gamma distribution  
50 function
- 51 • Rainfall-induced SGD and SWI were predictable

52

## 53 **1. Introduction**

54 The freshwater-saltwater mixing zone in a coastal aquifer, called subterranean estuary, plays  
55 an important role in controlling chemical fluxes from the aquifer to ocean [*Burnett et al.*, 2006;  
56 *Moore*, 1999; 2010; *Robinson et al.*, 2009; *Santos et al.*, 2012]. In this zone, submarine  
57 groundwater discharge (SGD) and seawater intrusion (SWI) are two complementary processes  
58 [*Moore*, 2010; *Werner et al.*, 2013], with the former covering all the water effluxes across the  
59 land-ocean interface and the latter linked to the extent of intruded saltwater in a coastal aquifer.  
60 Recent studies suggested that chemical fluxes associated with SGD can be comparable to riverine  
61 chemical inputs into the sea [*Kwon et al.*, 2014; *Moore*, 1996; *Rodellas et al.*, 2015; *Wang et al.*,  
62 2015]. SGD and SWI have been studied intensively in recent decades due to their significant

63 impacts on coastal environments and water quality in coastal aquifers [*Bakhtyar et al.*, 2012;  
64 *Bakhtyar et al.*, 2013; *Brovelli et al.*, 2007; *Lu et al.*, 2015; *Michael et al.*, 2013; *Moore*, 2010;  
65 *Santos et al.*, 2012; *Wang et al.*, 2015; *Werner et al.*, 2013].

66 Terrestrial groundwater discharge, density-driven flow, tides and waves are major driving  
67 forces affecting SGD and SWI in coastal aquifers (Fig. 1) [*Burnett et al.*, 2006; *Heiss and*  
68 *Michael*, 2014; *Li et al.*, 1999; *Michael et al.*, 2016; *Moore et al.*, 2008; *Taniguchi et al.*, 2002;  
69 *Xin et al.*, 2010]. In early work, it was assumed that SGD could be estimated based on a  
70 summation of fluxes driven by these forces independently [*Burnett et al.*, 2006; *Li et al.*, 1999;  
71 *Taniguchi et al.*, 2002], i.e.,

$$72 \quad \text{SGD} = Q_f + Q_c = Q_f + Q_d + Q_t + Q_w \quad (1)$$

73 where  $Q_f$  and  $Q_c$  are the inland freshwater input and total circulating seawater flux,  
74 respectively; and  $Q_c$  is given by a linear combination of the density-driven flow ( $Q_d$ ), tidally  
75 driven flow ( $Q_t$ ) and wave-induced flow ( $Q_w$ ).

76 In the presence of a seaward hydraulic gradient, fresh terrestrial groundwater flows towards  
77 and discharges into the coastal sea. In the absence of tides and waves on the seaward side, fresh  
78 groundwater flows above the denser seawater associated with the saltwater wedge (SW).

79 Convective circulation of seawater through the SW is caused by the density-gradient and affected  
80 by hydrodynamic dispersion along the freshwater-saltwater transition zone of the SW [*Cooper*,  
81 1959] (Fig. 1). The extent of the intruding saltwater wedge generally increases with decreasing  
82 fresh groundwater discharge ( $Q_f$ ) [*Glover*, 1959; *Smith*, 2004; *Werner et al.*, 2013].

83 Most coastlines worldwide are exposed to tides. The effect of tides on subterranean estuaries  
84 has been studied intensively over the last ten years [*Anschutz et al.*, 2009; *Heiss and Michael*,  
85 2014; *Kuan et al.*, 2012; *Li et al.*, 2008; *Mao et al.*, 2006; *Robinson et al.*, 2006; *Robinson et al.*,  
86 2007a; *Robinson et al.*, 2007b; *Robinson et al.*, 2009; *Wilson et al.*, 2015; *Zhang et al.*, 2016].  
87 Tidal fluctuations drive seawater circulations in shallow intertidal aquifers, alter the salt  
88 distribution and, under certain conditions, lead to the formation of an upper saline plume (USP)  
89 (Fig. 1) [*Evans and Wilson*, 2016; *Heiss and Michael*, 2014; *Robinson et al.*, 2006; *Robinson et*  
90 *al.*, 2007a]. Fresh groundwater discharges through a “tube” bounded by the USP and lower SW  
91 [*Boufadel*, 2000; *Robinson et al.*, 2007a]. The tide-induced seawater circulations can contribute  
92 significantly to the total SGD [*Burnett et al.*, 2006; *Li et al.*, 1999; *Robinson et al.*, 2007a] and  
93 limit the extent of SWI [*Kuan et al.*, 2012].

94 Waves are another important forcing factor for a nearshore subterranean estuary. The effects  
95 of waves are mainly manifested in wave setup, an onshore upward tilt in the mean sea level that  
96 drives a seawater circulation similar to that induced by tides [*Bakhtyar et al.*, 2013; *Geng et al.*,  
97 2014; *Li and Barry*, 2000; *Longuet-Higgins*, 1983; *Robinson et al.*, 2014; *Xin et al.*, 2010]. This  
98 circulation also increases the total SGD and inhibits the SWI. In contrast to tides, which have  
99 well-defined principal frequencies (e.g., spring-neap tides with semi-diurnal solar and lunar  
100 frequencies), waves are highly random with the height and period varying irregularly [*Heiss et al.*,  
101 2015; *Xin et al.*, 2014]. This leads to dynamic and irregular variations of SGD, SWI and USP at  
102 various temporal scales [*Robinson et al.*, 2014; *Xin et al.*, 2014].

103 Evaporation and rainfall lead to net water loss and gain for the aquifer, which affect  
104 groundwater discharge to the ocean. The effect of evaporation on nearshore groundwater slightly  
105 reduces the total SGD but increases considerably the pore-water salinity in the intertidal zone  
106 [*Geng and Boufadel, 2015; Geng et al., 2016*]. The rainfall effect however has not been  
107 investigated directly. Rainfall induces water infiltration that increases the aquifer recharge and  
108 raises the watertable [*Evans and Wilson, 2017; Heiss and Michael, 2014; Jun et al., 2013; Li et*  
109 *al., 2009*]. This would affect the SGD and SWI processes in the nearshore zone. A particular  
110 question is how rainfall interacts with other forcing factors, including tides and density-gradients.  
111 Interactions among different forces on the nearshore groundwater are non-linear and requires  
112 careful consideration in applying Eq. 1 for estimating the total SGD [*King, 2012; Sawyer et al.,*  
113 *2013; Xin et al., 2010; Xin et al., 2014; Xin et al., 2015*]. Each term in the equation cannot be  
114 treated as being solely dependent on a particular forcing factor but instead are functions of all the  
115 interacting forces.

116 The effect of rainfall on nearshore groundwater is likely to be long-lasting and cumulative,  
117 and is expected to result in hysteretic groundwater response, i.e., dependence of the present  
118 groundwater behavior on past rainfall events. *Xin et al. [2014]* examined the hysteresis of SGD  
119 driven by irregular waves and developed a hysteretic model based on functional data analysis  
120 [*Ramsay and Silverman, 2005*]. In the model, the effects of past wave conditions on SGD were  
121 assumed to vary over a continuum and were described by a continuous and smooth function  
122 (Gamma distribution function). Given its episodic nature, it is unclear whether the effect of

123 rainfall on SGD and SWI processes in the nearshore aquifer can be described similarly by a  
124 hysteretic model.

125 This study aims to examine the impact of rainfall based on numerical simulations with  
126 year-long data of episodic rainfall generated randomly to drive the nearshore groundwater flow  
127 and (salt) solute processes that are also affected by tides and density gradients. The analysis of  
128 the simulation results focuses on both long- and short-term nearshore groundwater responses  
129 with respect to yearly and daily averaged SGD and SWI. The yearly averaged SGD and SWI  
130 are analyzed to reveal the interactions of rainfall, tide and density-gradients. The variations of  
131 daily averaged quantities are linked to rainfall events through functional data analysis with the  
132 intention to develop a predictive, hysteretic model of SGD and SWI under episodic rainfall  
133 conditions.

134

## 135 **2. Numerical model and simulations**

136 The 2D model simulates a vertical cross-shore section of a nearshore unconfined aquifer  
137 with a setup similar to those adopted in previous studies (Fig. 1) [*Geng and Boufadel, 2015;*  
138 *Kuan et al., 2012; Liu et al., 2016; Robinson et al., 2007a; Xin et al., 2010; Xin et al., 2014*].

139 The model domain and parameter values were based on the conditions of a field site on the west  
140 coast of Moreton Island, Australia [*Robinson et al., 2006*]. At the site, oceanic oscillations are  
141 dominated by semi-diurnal tides. The aquifer was assumed to be homogeneous and isotropic  
142 [*Robinson et al., 2006*].

143 Variably saturated and density-dependent pore-water flow coupled with salt transport in the  
144 aquifer was simulated using SUTRA [Voss and Provost, 2008] under various forcing conditions  
145 including rainfall, tides and density-gradients.

146 In SUTRA, pore-water flow is described by the Richards equation [Richards, 1931] with  
147 the relative hydraulic conductivity and soil saturation calculated using the *van-Genuchten* [1980]  
148 formulas (details in *Xin et al.* [2010]). The model parameter values used in the simulations were  
149 representative of a permeable sandy coastal aquifer [Robinson *et al.*, 2006] with hydraulic  
150 conductivity  $K_s = 10$  m/d, porosity  $\phi = 0.45$ , longitudinal dispersivity  $\alpha_L = 0.5$  m and transverse  
151 dispersivity  $\alpha_T = 0.05$  m. The residual soil water saturation  $S_{wres}$  was set to 0.1 while the shape  
152 parameters  $\alpha$  and  $n$  were set to  $14.5 \text{ m}^{-1}$  and 2.68, respectively, for the *van-Genuchten* [1980]  
153 formulas [Carsel and Parrish, 1988]. This model setup was also used previously by *Xin et al.*  
154 [2010].

155 The occurrence, duration and intensity of rainfall over a year,  $R$  [ $\text{LT}^{-1}$ ], were determined by  
156 a Markov-chain Monte-Carlo simulator [Morris, 1995] (Fig. 2), in which the probability of dry  
157 weather following an hour of rain was set to 10% and the probability of rain following an hour  
158 of dry weather to 1%. The rainfall intensity followed a normal distribution with a mean  
159 intensity of 2 mm/h and standard variation of 0.5 mm/h. The annual rainfall of the generated  
160 random rainfall series was around 1.6 m occurring over approximately 80 events. The rainfall  
161 pattern was assumed to repeat on an annual basis and hence the generated year-long rainfall  
162 data were applied to all simulation years.



163        Rainfall-induced vertical infiltration was simulated as water influx across the aquifer  
164 surface including the exposed beach section. Based on the pore-water pressure ( $P$ ) at the node  
165 immediately below the aquifer surface, the local maximum infiltration rate under the surface  
166 ponding condition of zero water depth was calculated as  $I_{\max} = -K_s \left[ 1 - P / (\rho g \Delta z) \right]$ , where  
167  $\Delta z$  is the vertical grid size,  $\rho$  is the fluid density and  $g$  the gravitational acceleration. The  
168 rainfall infiltration rate ( $RI$ ) was then determined according to  $RI = \min(R, I_{\max})$ . It should be  
169 noted that a sandy coastal unconfined aquifer was considered in the simulations. The soil under  
170 the aquifer platform (AF in Fig. 1) was largely unsaturated, with an infiltration capacity larger  
171 than the maximum rainfall rate. Thus, infiltration-excess runoff did not occur. On the sloping  
172 beach (EF in Fig. 1), tides induced a moving boundary condition, which led to increase and  
173 decrease of the recharge area (in width) on falling and rising tides, respectively (more details in  
174 Section 3.1).

175        The details of the model setup and boundary conditions for all the simulations are given in  
176 Table 1. To explore how rainfall combines with tides and density-gradients to influence the  
177 nearshore groundwater dynamics, simulations were conducted with and without rainfall, and  
178 under both non-tidal (static sea level, Cases 1-3) and tidal (sea level oscillating with the semi-  
179 diurnal tide, Cases 4-6) conditions. The inland freshwater influx was set to  $2.1 \text{ m}^3/\text{m}/\text{d}$  (per unit  
180 width aquifer) for most simulation cases. In two reference cases without rainfall (Cases 3 and 6),  
181 fluxes matching the total rainfall-induced daily averaged infiltration rates were added uniformly  
182 to the landward boundary to evaluate the effect of vertical recharge versus increased inland  
183 groundwater influx. Additional two simulations (Cases 7 and 8) were conducted to examine the

184 effect of increased model domain sizes in both vertical and cross-shore directions, i.e., the  
185 upper boundary (AF) was extended upwards by 2 m in Case 7 (note that the beach, EF, was also  
186 extended to fix the beach slope) and the left boundary (AB) was extended landwards by 50 m in  
187 Case 8 (see *Xin et al.* [2010] for the detailed setup of the tide-induced moving boundary).

188

### 189 **3. Results and analysis**

#### 190 **3.1. Long-term rainfall effect based on yearly averaged results**

191 The simulations were run with no rainfall included for 5 years to reach a steady (for Case 1)  
192 or quasi-steady (periodic) state (for Case 4) with respect to both hydraulic heads and salinity  
193 distribution. These simulations produced similar results (Figs. 3a,c) to those of *Robinson et al.*  
194 [2007a] and *Xin et al.* [2010], in particular, changes of the salinity distribution due to the  
195 influence of tides (Fig. 3c for Case 4 versus Fig. 3a for Case 1). These results served as a model  
196 verification. Tide-induced recirculation led to the formation of a USP in the intertidal zone. The  
197 freshwater-saltwater mixing zone expanded, while the extent of the SWI decreased (i.e., the toe  
198 of the SW retreated from  $x = -40$  to  $-10$  m,  $z = -30$  m).

199 The simulations were subsequently run for another 5 years with the year-long rainfall data  
200 applied repeatedly for each year. The groundwater system reached a new quasi-steady state with  
201 invariant yearly averaged flux (SGD) and salt distributions. In the non-tidal case (Case 2),  
202 rainfall produced an additional freshwater influx of  $0.62 \text{ m}^3/\text{m}/\text{d}$  (per unit width aquifer) to the  
203 aquifer (through the upper boundary). This was the same as the total rainfall rate on the exposed  
204 aquifer surface ( $0.62 \text{ m}^3/\text{m}/\text{d}$ , 150 m in the cross-shore direction), indicating strong infiltration

205 capacity during the rainfall events. As expected, the rainfall-induced infiltration increased the  
206 freshwater discharge to the ocean, which in turn reduced the extent of SWI in the aquifer – the  
207 toe of the SW retreated from  $x = -40$  m in Case 1 to  $-30$  m in Case 2 (Fig. 3b versus 3a,  $z = -30$   
208 m).

209 In the tidal case (Case 5), rainfall produced a freshwater influx to the aquifer at the annual  
210 average rate of  $0.61 \text{ m}^3/\text{m}/\text{d}$ , slightly less than that for the non-tidal case (Case 2) due to the  
211 reduced infiltration capacity in the intertidal zone. This again increased the freshwater discharge  
212 to the ocean. As a result, the USP contracted and the SW retreated as evident in the comparison  
213 with Case 4 with no rainfall (Fig. 3d versus 3c). We calculated the salt mass stored in,  
214 respectively, the USP ( $SM_{\text{USP}}$ ) and SW ( $SM_{\text{SW}}$ , note that only the area of  $x \leq 20$  m was  
215 considered as seawater occupied the area for  $x > 20$  m) (Table 1). The yearly averaged  $SM_{\text{USP}}$   
216 decreased from  $3,498 \text{ kg}/\text{m}$  in Case 4 to  $2,485 \text{ kg}/\text{m}$  in Case 5, due to contraction of the USP.  
217 This is consistent with the results of *Robinson et al.* [2007a], which demonstrated that the size  
218 of the USP is controlled by the magnitude of tidal forcing relative to the fresh groundwater  
219 discharge rate. The retreat of the SW led to a reduction of  $SM_{\text{SW}}$  from  $16,801$  (Case 4) to  
220  $15,255$  (Case 5)  $\text{kg}/\text{m}$ . This reduction,  $1,546 \text{ kg}/\text{m}$ , was significantly less than that under the  
221 non-tidal condition, i.e., the difference between Case 1 and Case 2 ( $5,916 \text{ kg}/\text{m}$ ).

222 As expected, rainfall infiltration modified the water fluxes across the aquifer-ocean  
223 interface (Fig. 4). In the non-tidal case, rainfall infiltration increased the total SGD from  $2.26$   
224 (Case 1) to  $2.89$  (Case 2)  $\text{m}^3/\text{m}/\text{d}$  across a slightly expanded water efflux zone (Table 1 and Fig.  
225 4a). The increase of SGD was largely due to the additional freshwater influx/discharge induced

226 by rainfall and also a slightly larger flux of circulating seawater through the SW driven by  
227 density gradients ( $0.17 \text{ m}^3/\text{m/d}$  in Case 2 compared with  $0.16 \text{ m}^3/\text{m/d}$  in Case 1). The increase  
228 of the seawater circulation rate was caused by intensified freshwater-seawater mixing in the  
229 mixing zone of the SW due to increased freshwater discharge [Smith, 2004].

230 Tides induced significant seawater circulation at a rate of  $2.56 \text{ m}^3/\text{m/d}$  ( $Q_t$ ) in the intertidal  
231 zone with influx occurring between the high tide level and the mean sea level ( $-10 \leq x \leq 0 \text{ m}$ ,  
232 Fig. 4b), as shown by Case 4 in comparison with Case 1. The tidal effect also produced an  
233 increased rate of seawater circulation through the SW ( $0.56 \text{ m}^3/\text{m/d}$  compared with  $0.16 \text{ m}^3/\text{m/d}$   
234 in Case 1). As discussed above, rainfall generated an additional freshwater influx of  $0.61$   
235  $\text{m}^3/\text{m/d}$  to the aquifer, which increased the total freshwater discharge but reduced the extents of  
236 the USP and SW. The rainfall effect also resulted in a reduction in the tidal seawater circulation  
237 ( $Q_t$ ), similar to that of Case 4. However, the seawater circulation through SW driven by density  
238 gradients ( $Q_d$ ) was enhanced slightly (increased from  $0.56 \text{ m}^3/\text{m/d}$  in Case 4 to  $0.58 \text{ m}^3/\text{m/d}$  in  
239 Case 5), similar to the non-tidal case (Case 2). The net effect of rainfall led to an increase of  
240 SGD from  $5.22 \text{ m}^3/\text{m/d}$  in Case 4 to  $5.50 \text{ m}^3/\text{m/d}$  in Case 5. Despite an additional freshwater  
241 influx of  $0.61 \text{ m}^3/\text{m/d}$  induced by rainfall, the SGD increased by only less than half of that  
242 amount ( $0.28 \text{ m}^3/\text{m/d}$ ).

243 These results demonstrate strong interactions among the forces in controlling the nearshore  
244 groundwater processes: rainfall-induced freshwater discharge, and seawater circulations in the  
245 USP and SW driven by tides and density-gradients, respectively. Such interactions must be  
246 considered in estimating SGD, particularly when Eq. 1 is used. The coupling effects of different

247 forces need to be taken into account in determining each flux term. For example,  $Q_t$  depends on  
248 not only the tidal condition but also the freshwater influx and discharge including the  
249 component induced by rainfall. Each term in Eq. 1 must be determined as a function of all  
250 forces. This applies to rainfall-induced  $Q_f$ , which can be influenced by the tidal condition as  
251 evident in the difference between Cases 2 and 5.

252 Two additional simulations (Cases 3 and 6) were conducted with the rainfall infiltration  
253 simulated indirectly by increasing the inland freshwater flux to account for the daily averaged  
254 infiltration rate. Both simulations produced similar results (Fig. S1 in Supplemental material  
255 and Table 1), which suggest that under both non-tidal and tidal conditions, the long-term  
256 rainfall effect on nearshore groundwater (in terms of yearly averaged SGD and salt distribution)  
257 is determined largely by the amount of infiltration generated by rainfall.

### 258 **3.2. Short-term effect of episodic rainfall based on daily variations of SGD and SWI**

259 The SGD and associated salt distribution varied temporally in response to alternating rain  
260 events and dry weather. These variations are expected to increase the variability of the  
261 nearshore groundwater system, which was previously examined in relation to tidal fluctuations  
262 [Robinson *et al.*, 2007a; Xin *et al.*, 2010]. The analysis presented here focused on the daily  
263 averaged results and aimed to determine how they were related to the episodic rainfall data.

264 The maximum daily average rainfall rate, 0.048 m/d, appeared on day 97 (Fig. 2). However,  
265 the peak in the water efflux (SGD) occurred on day 101 for both Cases 2 (without tide) and  
266 Case 5 (with tide, Fig. 5), i.e., the SGD response was delayed by 4 d. From day 101, an 8-d dry  
267 period started (Fig. 2). However, the SGD in Cases 2 and 5 declined until day 110, when a

268 small peak appeared (Fig. 5). These results indicated that SGD responded to rainfall events in a  
269 delayed and prolonged fashion.

270 The rainfall effect also influenced the variations of daily averaged  $SM_{SW}$  (Fig. 6). The trend  
271 was, however, opposite to that observed for the SGD. Figure 6b shows that in Case 5,  $SM_{SW}$   
272 increased during days 118-150 while the SGD exhibited an overall decline (Fig. 5). This inverse  
273 relationship is consistent with previous findings [Kuan *et al.*, 2012; Michael *et al.*, 2005]. An  
274 inhibiting effect of rainfall was evident in the variations of the  $SM_{USP}$  (Figs. 7 and 8, Case 5). A  
275 nadir appeared on day 112 (Fig. 7d), when the USP was at its shallowest position (Figs. 7 and  
276 8). With a similar amount of rainfall infiltration added directly to the inland boundary, Case 6  
277 captured a similar  $SM_{USP}$  trend in comparison with Case 5 (Fig. 8). This suggests that the salt  
278 mass stored in the USP ( $SM_{USP}$ ) was mainly controlled by the inland freshwater input, rather  
279 than the dilution due to the rainfall-induced infiltration across the intertidal zone, which was  
280 small in comparison with the total infiltration into the aquifer platform.

281 Simple regression models were found to be inadequate for describing the relationships of  
282 daily averaged SGD and salt storage with the daily average rainfall rate. We explored an  
283 approach based on functional data analysis (FDA), used in a wide range of research fields,  
284 including hydrology [Ramsay and Silverman, 2005; Suhaila *et al.*, 2011; Wang *et al.*, 2011; Xin  
285 *et al.*, 2014]. The effect of rainfall events was considered to follow a continuous and smooth  
286 function at the relevant (daily) temporal scale.

287 To quantify the prolonged and cumulative effect of (past) rainfall events, we hypothesized  
288 that these events can be weighted in the form of convolution:

289

$$DRI = \frac{\sum_{j=n}^m \zeta_j R_{t-j\Delta t}}{\sum_{j=n}^m \zeta_j} \quad (2)$$

290 where  $DRI$  is a parametric regressor, i.e., the weighted rainfall events combined in a  
 291 cumulative fashion;  $t$  is the present time,  $t - j\Delta t$  is the given past time with  $\Delta t$  being the  
 292 increment (set to 1 d as the daily averaged results were used for the analysis),  $R_{t-j\Delta t}$  is the daily  
 293 average rainfall at that time. The minimum and maximum values of  $j$  are, respectively,  $n$  and  
 294  $m$ , which define the past time period considered.  $\zeta_j$  is a time-dependent weighting factor  
 295 described by a Gamma distribution with the following probability density function (PDF):

296

$$\zeta_j \square \text{Gamma}(\alpha, \beta, j\Delta t) = \beta^\alpha \frac{1}{\Gamma(\alpha)} (j\Delta t)^{\alpha-1} \exp(-\beta j\Delta t) \quad (3)$$

297 where  $\alpha$  and  $\beta$  are, respectively, the shape and scale factors. The ratio  $\alpha/\beta$  controls the tail of  
 298 the distribution and reflects the weight of past forcing conditions. It should be noted that we  
 299 chose Gamma distribution function because it can be non-monotonic (if  $\alpha > 1$ ) and has the  
 300 advantage of characterizing the delayed and prolonged effects of rainfall on SGD and SWI.  
 301 With two parameters, it is widely used to describe flow and solute transport in various  
 302 hydrological systems, e.g., for transit time modelling in catchment systems [Kirchner *et al.*,  
 303 2000; McGuire and McDonnell, 2006]. Furthermore, the Gamma distribution has no value at  
 304 zero (i.e., required that  $j\Delta t > 0$ ). In this study, we set  $n$  and  $m$ , respectively, to 1 and 365 (a  
 305 year) and thus Eq. 2 does not consider the effect of the present rainfall event.

306 We then explored how daily averaged SGD,  $SM_{USP}$  and  $SM_{SW}$  might be related to  $DRI$   
 307 based on a generalized linear model (GLM):

308 
$$Y = aDRI + b \tag{4}$$

309 This regression model contains only four coefficients ( $\alpha$ ,  $\beta$ ,  $a$  and  $b$ ), which assists in  
310 assessing the effect of rainfall on the considered subterranean estuary.

311 This model (Eq. 4) fitted the simulated results well (summarized in Table 2). For Case 2  
312 without the tide, the slope of the regression ( $a$ ) of Eq. 4 was positive (87.91 m) for the SGD  
313 but negative ( $-3.49 \times 10^5$  kgd/m<sup>2</sup>) for the SM<sub>SW</sub>, which is consistent with the overall effect that  
314 rainfall increased the SGD but inhibited the SWI. The two fitted Gamma distribution PDFs  
315 were non-monotonic with  $\alpha > 1$ , suggesting that the past rainfall effect did not decay  
316 immediately (Fig. 9 and Table 2). For the SGD, the peak of the fitted PDF appeared on day 4,  
317 corresponding with the occurrence of the maximum rainfall effect. We further calculated the  
318 backward elapsed time when the rainfall effect decayed to 10% (defined as memory time, MT)  
319 based on the fitted PDF. For Case 2, the MT for the SGD was 22 d, suggesting that the present  
320 SGD was still affected considerably by rainfall events 22 d before. The past rainfall effect on  
321 SM<sub>SW</sub> was more long-lasting. The peak occurred on day 35 with MT = 224 d. A similarly strong  
322 past rainfall effect was found for Case 3 (in which the equivalent rainfall infiltration was added  
323 to the inland boundary, Table 2 and Fig. S2). The peak occurred on day 41 with MT = 197 d.

324 In the tidally influenced aquifer, the SGD and SWI were also significantly affected by past  
325 rainfall events (Case 5, Fig. 10 and Table 2). While the MT for the SGD differed little from the  
326 non-tidal case, the MT for the SM<sub>SW</sub> was dramatically reduced from 224 (Case 2) to 46 (Case 5)  
327 d under the tidal influence (Table 2). This shows the competition between tides and rainfall  
328 infiltration in affecting SWI. The tidal effect weakened the influence of past rainfall and hence



329 shortened its MT. For  $SM_{USP}$ , both the peak (day 21) and MT (56 d) were longer than those for  
330  $SM_{SW}$  (day 3 and 46 d, respectively). This suggests that the effect of (past) rainfall on USP  
331 lasted longer than that on SW. This behavior is also evident in the comparison between Cases 5  
332 and 6 (Fig. 10 and Fig. S3). With the equivalent rainfall infiltration rate added to the inland  
333 boundary, Case 6 simulated well the rainfall effect on USP with the regression model for  $SM_{USP}$   
334 close to that of Case 5 (Table 2).

335 The GLM is essentially a memory-dependent linear signal filter. Despite the simplicity, it  
336 appears to capture the characteristics of episodic rainfall effects on the different metrics of the  
337 simulated subterranean estuary since all the adjusted  $R^2$  values are larger than 0.8 (Table 2).

### 338 **3.3. Predictability of the SGD and SWI affected by episodic rainfall**

339 We next consider if the GLM given by Eq. 4 captures the behavior of the nearshore aquifer  
340 when subjected to rainfall of different patterns. For this purpose, we generated another yearlong  
341 rainfall series using the Markov-chain Monte-Carlo simulator with the same statistical  
342 parameters (Fig. 11a). We continued to run the SUTRA simulations for the four cases with  
343 rainfall considered, i.e., using the results at the end of the year (day 365) as the initial  
344 conditions of the new simulations. The GLM, derived from previous simulations based on the  
345 rainfall dataset in Fig. 2, satisfactorily predicted the newly predicted SGD,  $SM_{SW}$  and  $SM_{USP}$   
346 averaged over a daily cycle (Fig. 11 and Figs. S4-6). The model performed even better for the  
347 tidal case (Fig. 11, Case 5). For the  $SM_{USP}$ , the simulated and predicted results largely overlap  
348 with adjusted  $R^2$  up to 0.97 (Figs. 11d and g).

### 349 **3.4. Influence of model domain**

350 With the model domain extended in either the upward (Case 7) or landward (Case 8)  
351 directions, the yearly averaged SGD,  $SM_{SW}$  and  $SM_{USP}$  did not change considerably (Table 1).  
352 This suggests that the total freshwater input controlled the overall long-term behavior of the  
353 nearshore aquifer system. However, the responses of the daily averaged SGD,  $SM_{SW}$  and  $SM_{USP}$   
354 were further delayed as indicated by postponed peaks of the fitted PDFs for daily averaged  
355 SGD,  $SM_{SW}$  and  $SM_{USP}$  curves (Figs. S7-S9). As expected, the travel time of the freshwater  
356 increased for both the aquifer with a thickened vadose zone (Case 7) and that with the landward  
357 boundary moved inland (Case 8). The prolonged effects of rainfall were well quantified by the  
358 regression model (Figs. S10-S12). Both the peak time (time for the maximum historic effect)  
359 and MT (time for the rainfall effect to decay to 10%) given by the PDFs increased (Table 2).  
360 For example, the peak time increased from 7 d for Case 5 to 13 d for Case 7, while MT  
361 increased from 31 to 42 d. These increases are consistent with the theory of groundwater wave  
362 propagation in unconfined aquifers [*Li et al.*, 1997; *Li et al.*, 2000; *Nielsen*, 2009; *Parlange et*  
363 *al.*, 1984].

364

#### 365 **4. Discussion and concluding remarks**

366 Rainfall generates freshwater influx to coastal aquifers, which subsequently discharges to  
367 the sea. As rainfall events are episodic, this influx tends to be highly variable. However, most  
368 previous modeling studies incorporated the freshwater input via the inland boundary of the  
369 aquifer with a fixed flux or head, overlooking the variability and randomness of natural systems  
370 [*Lu et al.*, 2015; *Michael et al.*, 2013; *Werner et al.*, 2013]. This paper quantified the SGD and

371 SWI processes in a nearshore aquifer subjected to the influence of episodic rainfall, and  
372 uncovered the delayed and prolonged rainfall effect. The findings have the following  
373 implications for future investigations on coastal and offshore environments:

- 374 • Different forces on the nearshore groundwater system interact strongly. While simple  
375 models such as Eq. 1 may still be applicable for predictions of SGD, each term attributed to  
376 a particular force must be determined with consideration of the influence of other forces.
- 377 • The interactions of the forces also affect the short-term behavior of the nearshore  
378 groundwater. Tides appear to shorten the period of past rainfall influence on nearshore  
379 groundwater dynamics, particularly seawater circulations through the USP and SW.
- 380 • The rainfall effect coupled with the influence of other forces must be considered in the  
381 studies of coastal groundwater dynamics. In particular, field investigations need to account  
382 for the effect of past rainfall events during both data collection and analysis.
- 383 • Meteorological data including rainfall are available widely in coastal zones around the world.  
384 Combined with data of other forcing factors such as tides and waves, these meteorological  
385 data allow the development of FDA models for predicting SGD and associated solute fluxes  
386 worldwide. These predictive models have a simple form and would be of direct use in  
387 developing strategies for protection of nearshore environments and groundwater resources  
388 management.

389 While the present study has generated insights into the SGD and SWI in a nearshore  
390 aquifer subjected to the influence of episodic rainfall, further investigations are needed to  
391 explore the following aspects:

392 • Soil hydraulic conductivity, capillarity and beach slope are key aquifer properties and  
393 worthy of detailed studies, particularly to explore how these parameters modify the  
394 coefficients of the generalized linear model. The model domain was a 2D vertical section  
395 perpendicular to the shoreline, and the aquifer was homogeneous and isotropic.  
396 Heterogeneous aquifer properties should be investigated. Three-dimensionality linked  
397 strongly to the beach morphology and land surface topography is likely to alter the SGD and  
398 SWI [Zhang *et al.*, 2016]. Local topographic variations, rather than the idealized geometry  
399 used here, are expected to affect rainfall infiltration and groundwater flow in both cross- and  
400 along-shore directions.

401 • Wave forcing and multiple tidal constituents (e.g., combined semi-diurnal solar and lunar  
402 tides) were not considered. These factors would provide additional forcing on the flow and  
403 associated solute transport in a nearshore aquifer. Particularly, wave motions are highly  
404 variable. It remains to be determined how this variability combined with episodic rainfall  
405 events would be manifested in the SGD and SWI.

406 • Variations of SGD and SWI over the tidal cycle are significantly altered by tidal fluctuations.  
407 While we have quantified the daily variation of SGD and SWI, an improved statistical model  
408 with high-order terms is needed to unravel the intra-tidal variations of SGD and SWI.

409 Although these research questions remain unsolved, the generalized linear model  
410 developed based on functional data analysis is a potentially useful approach to characterizing  
411 and quantifying the complex SGD and SWI processes in a nearshore aquifer, subjected to  
412 irregular forcing factors such as rainfall.

413

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421

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608

609 **Table 1. Simulated cases with model setup and key results of long-term SGD and salt mass<sup>#</sup>.**

Case	Model domain	Tide	Rainfall		Per unit width influx (m <sup>3</sup> /m/d)				Per unit width efflux (SGD) (m <sup>3</sup> /m/d)	Salt mass stored in per unit width aquifer (kg/m)	
					$Q_f$	$Q_t$	$Q_d$	$Q_r$		Saltwater wedge	Upper saline plume
1	Fig. 1	Without	Without	NA	2.10	NA	0.16	NA	2.26	32,499	NA
2	Fig. 1	Without	With	Top	2.10	NA	0.17	0.62	2.89	26,583	NA
3	Fig. 1	Without	With*	Left	2.10+0.62*	NA	0.16	NA	2.88	26,867	NA
4	Fig. 1	With	Without	NA	2.10	2.56	0.56	NA	5.22	16,801	3,498
5	Fig. 1	With	With	Top	2.10	2.21	0.58	0.61	5.50	15,255	2,485
6	Fig. 1	With	With*	Left	2.10+0.62*	2.21	0.58	NA	5.51	15,352	2,526
7	AF in Fig. 1 was extended upwards by 2 m	With	With	Top	2.10	2.14	0.58	0.61	5.43	15,569	2,560
8	AB in Fig. 1 was extended landwards by 50 m	With	With*	Left	2.10+0.62*	2.21	0.58	NA	5.51	15,343	2,504

610 <sup>#</sup> All the results are yearly averaged.  $Q_f$  is the inland freshwater input;  $Q_t$  is the circulating flux induced by tide;  $Q_d$  is the density-  
611 driven flux;  $Q_r$  is the rainfall infiltration. \* indicates that the rainfall infiltration was considered as the inland freshwater input across  
612 the inland boundary. NA means not applicable.

613 **Table 2. Summary of regression results for daily averaged SGD and salt mass in SW and**  
 614 **USP<sup>#</sup>.**

		Case 2	Case 3	Case 5	Case 6	Case 7	Case 8
SGD	$\alpha$	1.50	2.00	1.76	1.50	2.40	1.6
	$\alpha/\beta$	0.21	0.26	0.20	0.16	0.26	0.1
	Adjusted $R^2$	0.80	0.83	0.89	0.99	0.87	0.98
	$a$	87.91	63.32	64.12	65.16	72.10	67.66
	$b$	2.52	2.76	5.08	5.09	4.92	5.08
	Peak (d)	4	8	7	5	13	9
	MT (d)	22	30	31	29	42	53
SM <sub>SW</sub>	$\alpha$	1.62	1.80	1.20	3.80	1.20	3.52
	$\alpha/\beta$	0.02	0.03	0.07	0.58	0.04	0.37
	Adjusted $R^2$	0.91	0.94	0.87	0.97	0.88	0.96
	$a$	$-3.49 \times 10^5$	$-4.04 \times 10^5$	$-1.76 \times 10^5$	$-1.34 \times 10^5$	$-2.79 \times 10^5$	$-1.31 \times 10^5$
	$b$	$2.84 \times 10^4$	$2.85 \times 10^4$	$1.60 \times 10^4$	$1.59 \times 10^4$	$1.67 \times 10^4$	$1.59 \times 10^4$
	Peak (d)	35	41	3	18	5	24
	MT (d)	224	197	46	42	79	58
SM <sub>USP</sub>	$\alpha$	NA	NA	3.10	3.30	3.60	3.52
	$\alpha/\beta$	NA	NA	0.30	0.34	0.34	0.31
	Adjusted $R^2$	NA	NA	0.98	0.99	0.96	0.99
	$a$	NA	NA	$-2.29 \times 10^5$	$-2.13 \times 10^5$	$-2.53 \times 10^5$	$-2.03 \times 10^5$
	$b$	NA	NA	$3.43 \times 10^3$	$3.41 \times 10^3$	$3.61 \times 10^3$	$3.35 \times 10^3$
	Peak (d)	NA	NA	21	22	27	29
	MT (d)	NA	NA	56	56	66	70

615 <sup>#</sup> SGD is the submarine groundwater discharge; SM<sub>SW</sub> is the salt mass stored in the saltwater  
 616 wedge (per unit width aquifer); SM<sub>USP</sub> is the salt mass stored in the upper saline plume;  $\alpha$  and  
 617  $\beta$  are, respectively, the shape and scale factors of Gamma distribution function;  $a$  and  $b$  are  
 618 coefficients for the regression. Peak indicates the backward elapsed time for the maximum  
 619 historic effect; MT is the memory time, i.e., the backward elapsed time for the rainfall effect to  
 620 decay to 10%. NA means not applicable.



621 **Figure captions**

622

623 Fig. 1. Conceptual diagram of an unconfined near-shore aquifer (subterranean estuary)  
624 including major flow processes: (1) density-driven recirculation, (2) tide-induced recirculation,  
625 (3) recirculation driven by wave setup and (4) terrestrial groundwater discharge including  
626 freshwater influx generated by rainfall infiltration. The colors represent the salinity (red for  
627 seawater and yellow for freshwater). Boundary **ABCDEF** is the model domain. The  $x$ - $z$   
628 coordinate origin was set at the mean shoreline. The coordinates of the domain reference points  
629 for Cases 1-6 are given in the unit of m. The upper boundary (AF) was extended upwards by 2  
630 m in Case 7 and the left boundary (AB) was extended landwards by 50 m in Case 8. Note that  
631 wave forcing is not considered in the present study.

632

633 Fig. 2. Annual rainfall time series used in the simulations. The red line indicates the daily  
634 averaged results.

635

636 Fig. 3. Yearly averaged salinity distributions in the subterranean estuary. Cases are indicated in  
637 the figure titles. The left hand side panels are for the non-tidal cases, in which the black lines  
638 indicate the static sea level. The right side panels are for the tidal cases, in which the black lines  
639 indicate the tidal range. The results for Cases 3 and 6 were, respectively, similar to those for  
640 Cases 2 and 4 (see Fig. S1 in Supplemental material).

641  
642 Fig. 4. Yearly averaged water influx and efflux rates per-unit-area along the aquifer-ocean  
643 interface. (a) is for the non-tidal cases. The lines for the influx of Cases 1, 2 and 3 overlap as do  
644 the lines for the efflux of Cases 2 and 3. (b) is for the tidal cases. Note that the influx excluded  
645 the rainfall infiltration. The lines for the influx and efflux of Cases 5 and 6 overlap.

646  
647 Fig. 5. Daily averaged water efflux (SGD) across the per-unit-width aquifer-ocean interface.

648  
649 Fig. 6. Daily averaged salt mass stored in the per-unit-width saltwater wedge.

650  
651 Fig. 7. Snapshots of daily averaged salinity distributions for Case 5. The time is given in the figure  
652 titles and the salt mass stored in the per-unit-width upper saline plume is marked on the figure. Two  
653 black lines indicate the high and low tidal levels.

654  
655 Fig. 8. Daily averaged salt mass stored in the per-unit-width upper saline plume.

656  
657 Fig. 9. (a) Gamma distribution functions used for quantifying the effect of past rainfall events  
658 on the subterranean estuary (Case 2); (b and c) Fitted results versus those simulated.

659  
660 Fig. 10. (a) Gamma distribution functions used for quantifying the effect of past rainfall events

661 on the subterranean estuary (Case 5); (b-d) Fitted results versus those simulated.

662

663 Fig. 11. (a) Annual rainfall time series used for the prediction (series generated using the

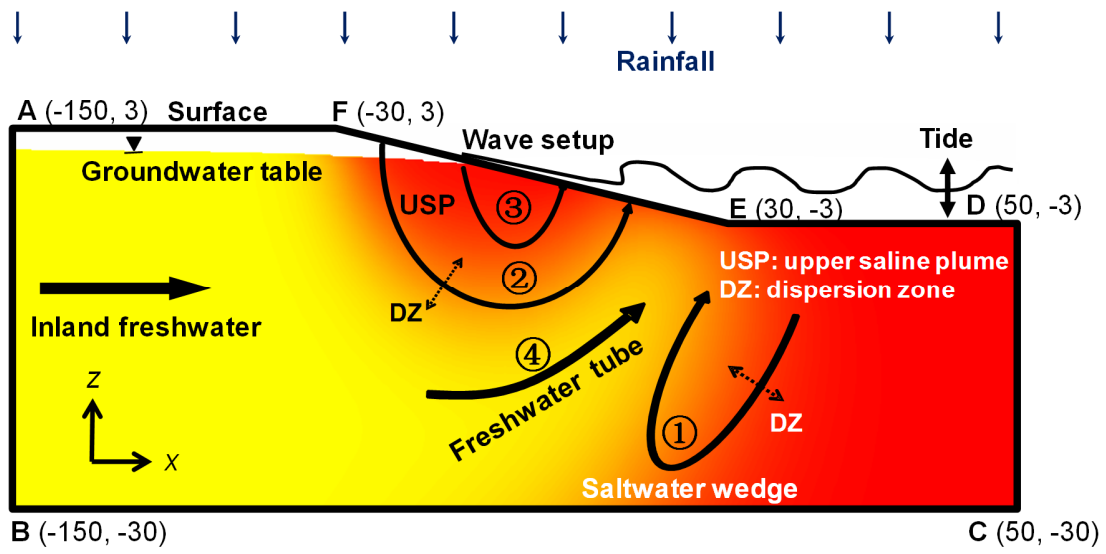
664 Markov-chain Monte-Carlo simulator with the same statistical parameters as the rainfall time

665 series in Fig. 2). The red line indicates the daily averaged results. (b-d) Daily averaged SGD,

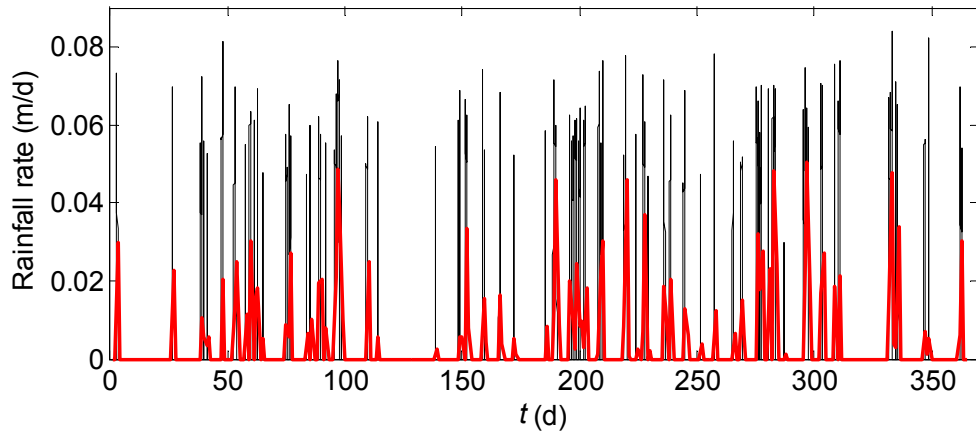
666  $SM_{SW}$  and  $SM_{USP}$  predicted by the regression model in comparison with the simulated results

667 (Case 5). (e-g) Predicted results versus those simulated.

**Figure 1.**

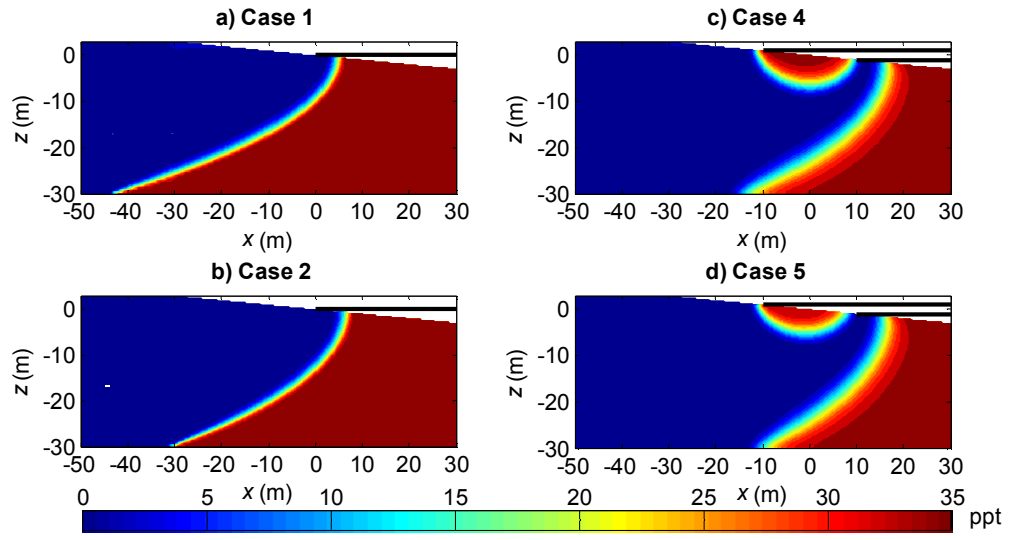


**Figure 2.**

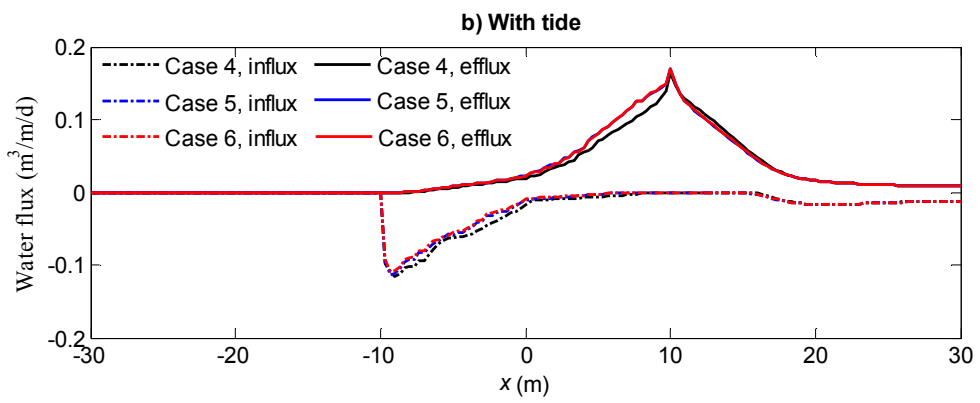
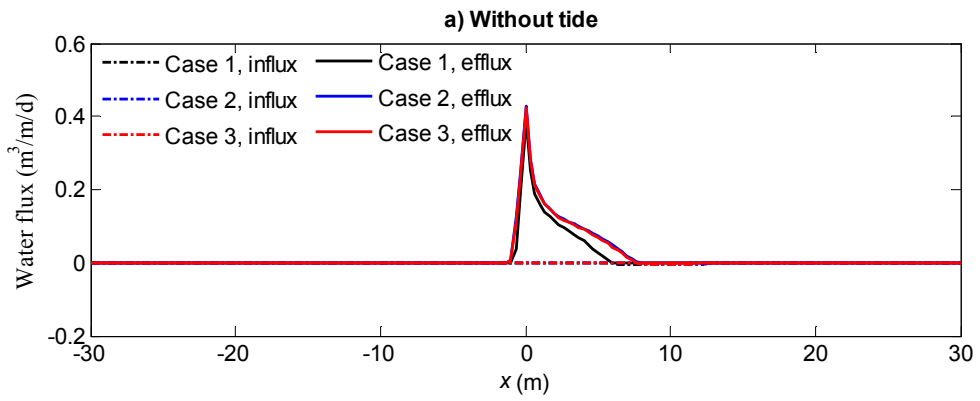


**Figure 3.**

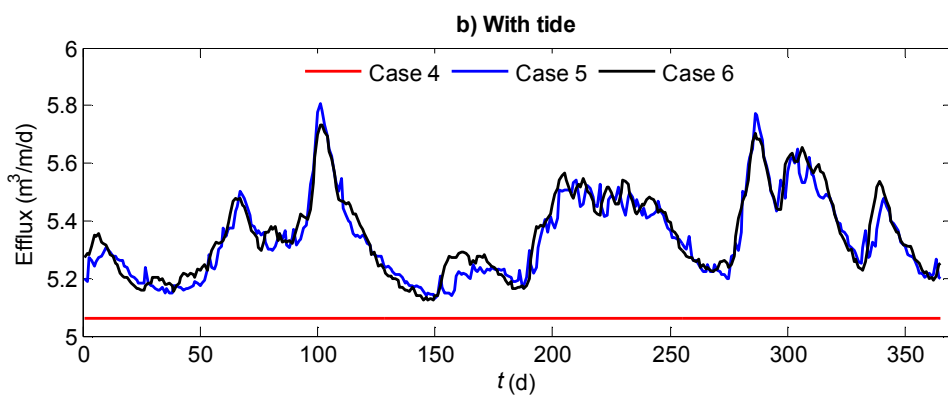
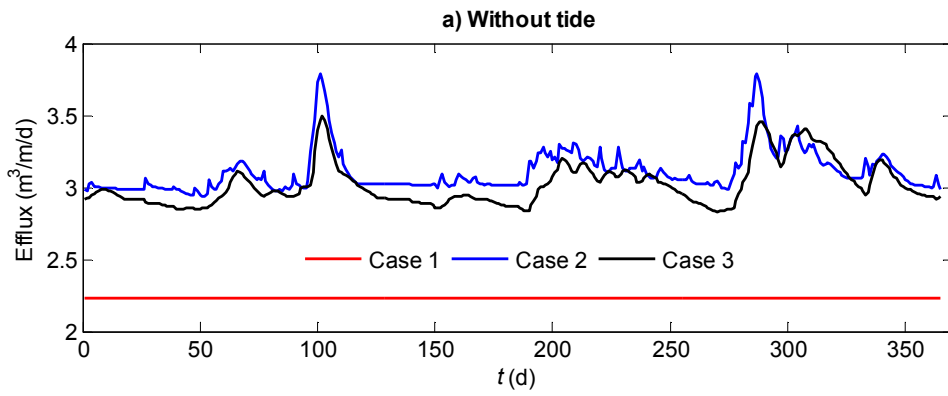




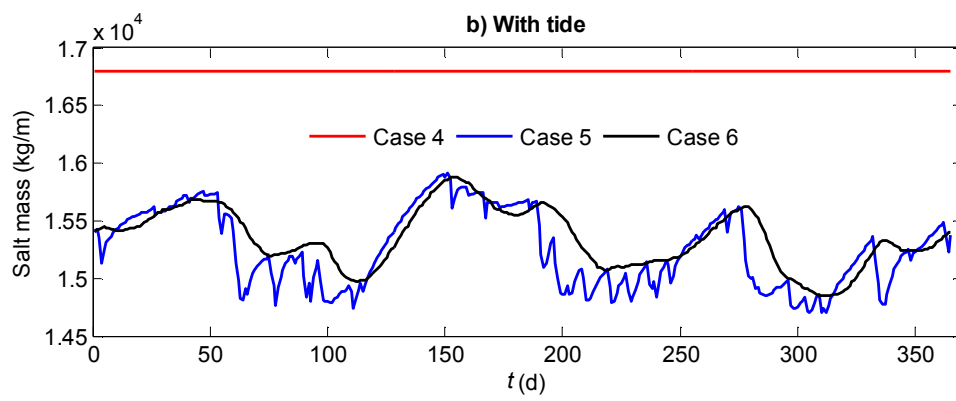
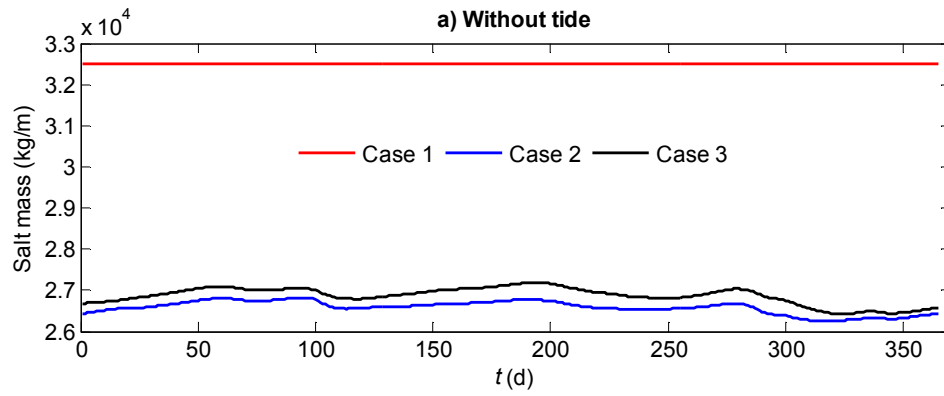
**Figure 4.**



**Figure 5.**

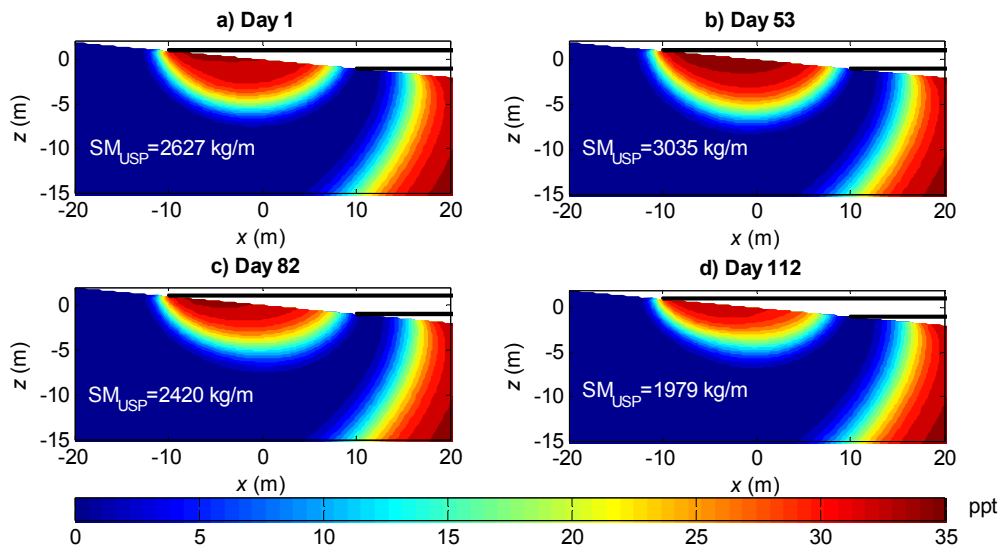


**Figure 6.**

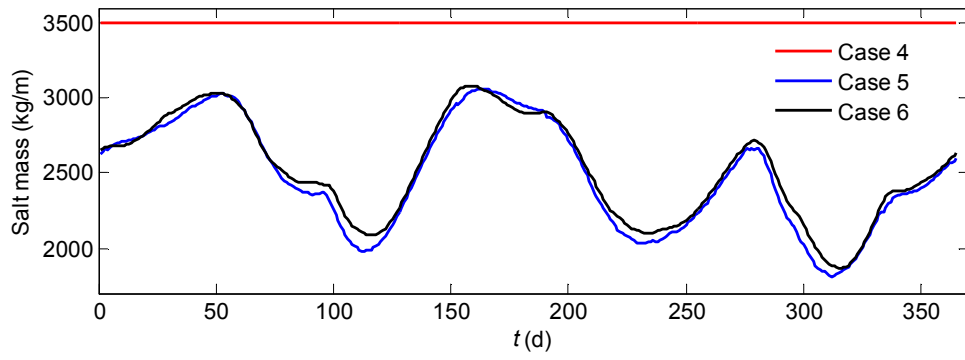


**Figure 7.**

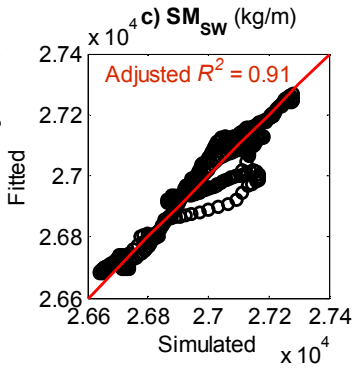
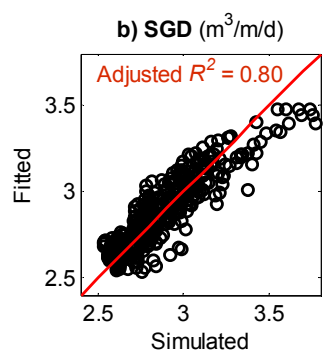
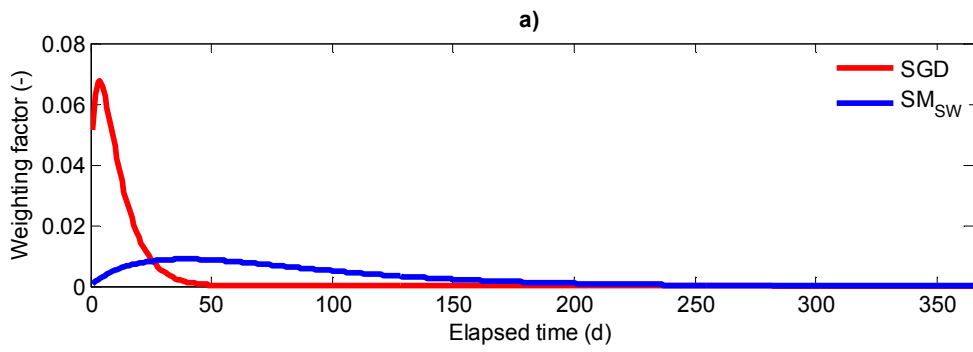




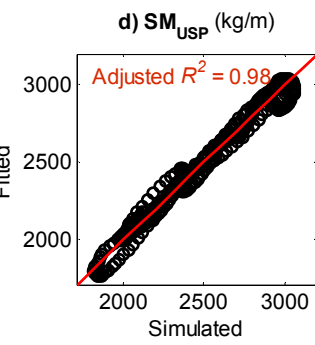
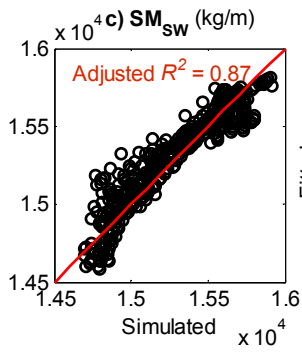
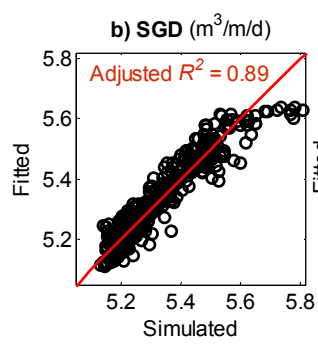
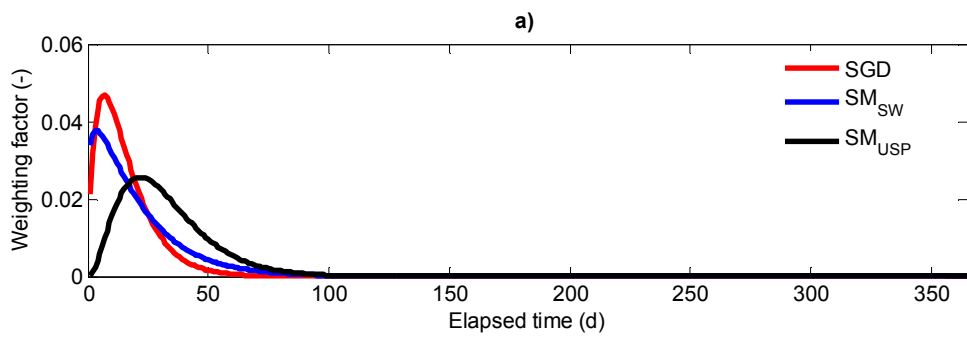
**Figure 8.**



**Figure 9.**



**Figure 10.**



**Figure 11.**



