Minimization of Ionic Transport Resistance in Porous Monoliths for Application in Integrated Solar Water Splitting Devices

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Supporting Information

ABSTRACT: Monolithic solar water splitting devices consist of photovoltaic materials integrated with electrocatalysts and produce solar hydrogen by water splitting upon solar illumination in one device. Upscaling of monolithic solar water splitting devices is obstructed by high ohmic losses in the electrolyte due to long ionic transport distances. A new design overcomes the problem by introducing micron sized pores in a silicon wafer substrate coated with electrocatalysts. A porous solar hydrogen device was simulated by applying a current corresponding to ca. 10% solar-to-hydrogen efficiency. Porous monoliths of 550 μm thickness with varying pore size and spacing were fabricated by laser ablation and electrochemically characterized. Ohmic losses well below 100 mV were reached at 14.4% porosity with 77 μm pores spaced 250 μm apart in 0.25 M KOH electrolyte. In 1 M KOH, 100 mV was reached at 6% porosity with 1 mm pore spacing. Our results suggest ohmic losses below 50 mV can be achieved when using 10 μm thick substrates at 0.2% porosity. These findings make it possible for monolithic solar water splitting devices to be scaled without loss of efficiency.

INTRODUCTION

Hydrogen is one of the promising energy vectors that will likely be part of the future sustainable energy portfolio.1 Using sunlight to split water into hydrogen and oxygen is a viable option for solar hydrogen production and several technologies exist that achieve water splitting at high efficiency.2 A direct way to produce solar hydrogen is by using a solar water splitting device which combines light absorption, charge separation and electrochemical reactions in an integrated device.3 High solar-to-hydrogen (STH) efficiencies are reached using high-end photovoltaics (PV) coupled to electrocatalysts submerged in concentrated aqueous electrolyte.4−7 The use of robust earth-abundant catalysts and stable light absorbing materials with suitable band gaps has also been demonstrated.8−11 These approaches show great promise at lab scale and development of practical systems is ongoing.12−16 Beside the performance of catalysts and light absorbers, cell design is important and ohmic losses need to be minimized to maximize overall efficiency.17,18 There are two common design types.19,20 In the “wired” design (Figure 1A) planar anode and cathode have opposed surfaces at close proximity such that the interelectrode distance to be covered by ions in the liquid electrolyte is minimized.9−11

The “wireless” or “monolithic” layout (Figure 1B) simplifies cell design by eliminating electrical contacts and wires through integration of all components in a monolithic flat assembly.10

These two designs differ in the way ionic transport is organized.10 The overall transport distance between electrodes dictates the ohmic losses of the ions in the electrolyte and can contribute significantly to the overall operating voltage.19,21 Ohmic losses are often minimized by using concentrated acid or alkaline electrolytes such as H2SO4, HClO4 or KOH at concentrations of 0.5 M or higher.4,5,14,22,23 In wireless systems with flat monoliths consisting of dense PV and electrocatalysts mounted on either side, ions need to travel around the dense monolith to cover the distance between anode and cathode. Already at the centimeter scale unacceptable ohmic losses of hundreds of millivolts and more are to be expected.19,21

A straightforward way to achieve anode−cathode proximity in a flat monolithic system is by providing ionic shortcuts. Recently an innovative concept was reported that efficiently achieves low ionic transport distances and low ohmic losses in a monolithic assembly by Si microwires into an electrical and ionic conducting membrane.24 This concept suffers from complicated manufacturing procedures and generates low photovoltage, which can be alleviated by the application of passivation strategies.25,26 In this work, we propose another way of achieving short ion transport distances, namely by

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perforation of monolithic assemblies (Figure 1C). Systematic perforation could be applied to monoliths whatever their size. Additionally such design can easily achieve product separation by introducing a membrane, avoiding dangerous mixing of hydrogen and oxygen and requiring low membrane quantities, depending on the porosity.

We have investigated the ionic transport aspects of the new design type by using an oxidized silicon wafer, coated with electrocatalysts and perforated using laser ablation. Different pore designs and their influence on the ohmic losses of the device were studied. By application of a current across anode and cathode (without illumination), a porous monolithic solar water splitting device with ca. 10% STH efficiency was simulated. Minimization of ohmic losses well below 100 mV in KOH electrolyte is demonstrated. Guidelines for optimum pore configuration are provided.

## EXPERIMENTAL SECTION

### Preparation of Porous Monolithic Assemblies

N-type silicon wafers (Cemat Silicon, 4″ unpolished, 3–10 ohm cm) with a thickness of 525–575 μm were used as substrate for porous monoliths. RCA cleaning was followed by wet oxidation at 1100 °C for 2 h to obtain an insulating layer of SiO₂ on both sides of the wafer. Thin catalyst films were sputtered on the wafer using Balzers BAE 370 sputtering tool. First, a Ti/W (Ti₃₂W₆₈ target, 99.95%) adhesion layer was sputtered at 2.10⁻³ mbar Ar and 150 W for 1 min on both sides. Then, for the cathode, Pt (Pt target, 99.95%) was sputtered at 100 W for 3 min, other parameters unchanged. The anode was sputtered with Ir (Ir target, 99.9%) under Ar atmosphere at 200 W for 5 min. Subsequently an IrOₓ layer was sputtered under Ar/O₂ (10:1 volume ratio) at 200 W for 2 min. As deposited anode and cathode catalyst layers measured 400 and 120 nm in thickness, respectively. Pores were introduced in the as prepared wafers by laser ablation (HDYAG, 1064 nm, spot size ca. 65 μm). A porosity of 5.3% for all samples was targeted by adjusting the pore radius at preset pore spacing (center to center) (Table 1). Actual pore diameter deviated from targeted diameter at small dimensions. This resulted in a porosity substantially exceeding the aimed value for sample A and B (Table 1). The pores in sample A and B were narrower at the anode side compared to the cathode side. The design of monolith A is schematically represented in Figure 2. Activation of IrOₓ to Ir³⁺O₂ thin film was achieved by repetitive cycling from 0 to 1.46 V vs. RHE in 0.5 M H₂SO₄ solution (Figure S3, Supporting Information).

### Table 1. Properties of Porous Monolithic Samples

<table>
<thead>
<tr>
<th>Sample</th>
<th>A</th>
<th>B</th>
<th>C</th>
<th>D</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pore diameter at anode side [μm]</td>
<td>77</td>
<td>232</td>
<td>1340</td>
<td>4600</td>
</tr>
<tr>
<td>Pore diameter at cathode side [μm]</td>
<td>135</td>
<td>316</td>
<td>316</td>
<td>4600</td>
</tr>
<tr>
<td>Pore spacing [mm]</td>
<td>0.25</td>
<td>1</td>
<td>5</td>
<td>17.7</td>
</tr>
<tr>
<td>Number of pores</td>
<td>5030</td>
<td>316</td>
<td>12</td>
<td>1</td>
</tr>
<tr>
<td>Porosity [%]</td>
<td>14.4</td>
<td>6.0</td>
<td>5.3</td>
<td>5.3</td>
</tr>
<tr>
<td>Pore configuration</td>
<td><img src="image1.png" alt="Image" /></td>
<td><img src="image2.png" alt="Image" /></td>
<td><img src="image3.png" alt="Image" /></td>
<td><img src="image4.png" alt="Image" /></td>
</tr>
</tbody>
</table>

Figure 1. Design types of solar water splitting devices and indication of acid (H⁺) or alkaline (OH⁻) ion transport pathways. A = anode, C = cathode, PA = photoabsorber, and E = electrolyte.

Figure 2. Schematic of porous monolith A.
**Electrochemical Characterization of Monolithic Assemblies.** Electrochemical characterization was done in an H-type electrochemical cell in two- or three-electrode setup (Figure S4). Experiments were performed in KOH electrolyte with increasing concentration (0.0625, 0.25, and 1 M) and corresponding decreasing resistivity of (73.5 Ω cm, 18.4 Ω cm and 5.6 Ω cm) measured with a calibrated conductivity measuring tool (Tetracon, VWR). Chronopotentiometric (CP) measurement were performed at an applied current density of 7.84 mA cm$^{-2}$. This corresponds to an STH efficiency of ca. 10% (assuming 100% Faradaic efficiency). Galvanostatic electrochemical impedance spectroscopy (EIS) measurements were performed in 0.0625 M KOH at 1 mA in the frequency range from 1 MHz to 100 Hz in a 2-electrode setup.

**Non Ohmic Losses.** CP measurements of anode and cathode were performed in a 3-electrode setup. For HER and OER determination, O$_2$ and H$_2$ was purged through the respective compartment at 20 mL min$^{-1}$. The solution was not stirred during measurement. Ag/AgCl (3 M KCl) electrode served as the reference and a Pt ring as the counter electrode. CP measurements were carried out for 60 s and corrected for uncompensated $iR$ losses.

**Ohmic Losses.** CP measurements of the porous monolith were performed in a 2-electrode setup. To avoid transient contributions of concentration polarization by the reaction products, purging of O$_2$ in the anode compartment and H$_2$ in the cathode compartment was done to saturate the compartments prior to measurement. The solution was not stirred during measurement. Ohmic losses were obtained by subtracting average kinetic and mass transport losses of both catalysts from the total operating overpotential (Supporting Information). The linear correlation between ohmic losses and resistivity was used to calculate the cell constant. Ohmic loss for sample A in 1 M KOH was below the detection limit via CP measurement (Supporting Information) and was obtained by linear extrapolation.

**Product Measurement and Crossover.** Product analysis was done by mass spectrometry (Quantitative Gas Analyzer, Hiden Analytical, Warrington, U.K.) with N$_2$ and Ar as carrier gas at a fixed flow rate (50 mL min$^{-1}$) in anode and cathode compartment, respectively. Calibration was done using the carrier gas signal. Faradaic efficiency and crossover were calculated from the measured O$_2$ and H$_2$ formation rates.

## RESULTS AND DISCUSSION

The problem of ohmic losses in integrated solar water splitting devices due to long ionic transport distances is revealed by a simple calculation. Consider a typical wired device (Figure 1A) operating at a current density of 10 mA cm$^{-2}$ in 0.5 M H$_2$SO$_4$ electrolyte at 25 °C (conductivity of 211 mS cm$^{-1}$) and with anode and cathode separated by 1 cm. The ohmic loss corresponds to 47 mV. Even for such a favorable position of electrodes in close proximity, the ionic transport resistance is of the order of magnitude of a typical kinetic overpotential at a platinum hydrogen evolving electrode.$^{22}$ With wireless setups, the ohmic losses are even larger. To illustrate this, a dense square monolith measuring 2.5 × 2.5 cm was immersed vertically in KOH electrolyte solution leaving 0.5 cm of space above and below. Ohmic losses were significant and amounted to 70, 195, and 771 mV in 1.0, 0.25, and 0.0625 M KOH solution, respectively. For the case of 1 M KOH, the ohmic losses already amounted to 15% of the total device overpotential. It illustrates the use of dense submerged monolithic assemblies is no option for designing a scalable and efficient solar water splitting device, in which large ohmic losses cannot be tolerated.$^{21}$ The combination of highly active catalysts with a state-of-the-art triple junction solar cell is able to reach 10% STH efficiency if ohmic losses are kept below 100 mV. Therefore, 100 mV is assumed as an upper target in this work (see Supporting Information).

Porous monolithic silicon wafers, coated with electrocatalysts were fabricated and tested for their ohmic losses in a water splitting experiment in alkaline electrolyte. Figure 3 shows the different pore designs that were tested (details in the Experimental Section). A constant porosity for all samples was targeted.

**Ohmic losses during water splitting obtained from the perforated monoliths A–D are given in Table 2.** The lowest ohmic losses were recorded on monolith A, having the smallest pores and highest porosity. Sample A exhibits ohmic losses below 100 mV in 1 M KOH as well as 0.25 M KOH solution. Monolith B having wider pores and lower porosity achieves the targeted ohmic loss at 1 M KOH. The 1.3 mm size pores in sample C and the single pore measuring 4.6 mm in sample D representing 5.3% porosity are insufficient to reduce ohmic losses to the desired value. Samples C and D show ohmic losses which exceed kinetic overpotentials in a typical solar water splitting device.$^{21}$ For each monolith ohmic losses decrease with increasing electrolyte concentration, which is to be expected from Ohm's law.

Ohmic losses are plotted against pore spacing in Figure 4. For the three investigated KOH concentrations, the ohmic losses increase with increasing pore spacing, highlighting the dominant role of this parameter. Larger pore spacing results in longer transport distances for ions between both electrodes. For samples C and D in 1 M KOH, the ohmic losses are 145 and 346 mV respectively, amounting to more than 30% and 50% of the total required overpotential of the device, showing the dominant effect of large ionic transport distances even at high concentrations. Accepting 100 mV ohmic losses, maximally 1 mm spacing of pores is allowed when operating in 1 M KOH. In 0.25 M solution, the spacing needs to be limited to 250 μm. At these small ionic transport distances,

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**Table 2. Overview of Ohmic Losses (in mV) Depending on Electrolyte Concentration and Cell Constants $K_{cell}$ [cm$^{-1}$] for Perforated Monoliths**

<table>
<thead>
<tr>
<th>Electrolyte Concentration</th>
<th>Ohmic Losses (in mV)</th>
<th>$K_{cell}$ [cm$^{-1}$]</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.0625 M KOH</td>
<td>234</td>
<td>0.13</td>
</tr>
<tr>
<td>0.25 M KOH</td>
<td>78</td>
<td>0.36</td>
</tr>
<tr>
<td>1 M KOH</td>
<td>19</td>
<td>0.83</td>
</tr>
<tr>
<td></td>
<td>5</td>
<td>1.64</td>
</tr>
</tbody>
</table>

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**Figure 3.** Schematic of the porous monolithic samples A–D with increasing pore size and spacing between pores (pores not to scale). Detailed information can be found in the Experimental Section and in the Supporting Information.
Ohmic losses only contribute 5% to the total overpotential of the device.

Faradaic efficiencies for hydrogen were over 97% in all instances. Back reaction is expected to be minimal as hydrogen oxidation reaction is poor on the IrO₂ surface.²⁸ This was evidenced by the lack of a hydrogen adsorption peak in the cyclovoltammetric activation of IrO₂ to Ir²⁺O₂ (Supporting Information).

Over 15% of the produced hydrogen was present in the anode compartment, revealing significant transport through the pores from cathode to anode compartment (Figure 5).

Figure 5. Hydrogen collection yields in cathode and anode compartments. Experimental conditions: 1 M KOH, 25 °C, ca. 10% simulated STH efficiency, collection during continuous operation for 1h and averaged over 7 collection periods.

Hydrogen crossover was little dependent on pore size. In a functional solar water splitting device with porous monolith the pores need to be filled with molecular barrier material to prevent crossover of gaseous products.

In an electrochemical circuit representing the perforated monoliths (Figure 6), the operating potential (ΔE) is a sum of the thermodynamic equilibrium potential (E°) and any overpotential resulting from the resistances in the circuit (IRcell) at a given current. The main contributions are kinetic overpotential (IRkinetic), concentration overpotential (IRconc) and ohmic losses caused by ion transport (IRohmic). Note that kinetic and concentration overpotentials are not linear and thus do not follow Ohm’s law. Other losses such as metallic film resistance (Rfilm) and bubble formation (IRrest) may contribute as well.

\[
ΔE = E° + IRcell \tag{1}
\]

\[
R_{cell} = R_{kinetic} + R_{ohmic} + R_{cp} + R_{met} + R_{rest} \tag{2}
\]

Ohmic losses relate here to the resistance of an ionic current in an electrolyte and this resistance is denoted as

\[
R_{ohmic} = \frac{l}{Aρ} = \frac{K}{ρ} \tag{3}
\]

where \(l \, [\text{cm}]\) is the distance between anode and cathode, \(A \, [\text{cm}²]\), the cross section of the ionic pathway, and \(ρ \, [\Omega \, \text{cm}]\), the electrolyte resistivity. The ratio of \(l \) over \(A \) is defined as the cell constant \(Kcell \, [\text{cm}⁻¹]\) (Table 2). The cell constants were calculated for all porous monoliths and galvanostatic EIS proved a useful tool to measure this property (Figure S9, Supporting Information). In a porous monolith, the ohmic losses \(R_{ohmic}\) can be subdivided into a pore \(R_{pore}\) and a surface \(R_{surface}\) contribution with corresponding cell constants \(K_{pore}\) and \(K_{surface}\). As both contributions are connected in series, the total ohmic losses can be written as

\[
R_{ohmic} = K_{cell}ρ = (K_{pore} + 2K_{surface})ρ \tag{4}
\]

\(K_{surface}\) is determined by the electrolyte height above the surface, pore spacing and porosity pattern. This value cannot be calculated analytically as the exact pathway of ions from the surface to the pore may occur in different ways. In general, a large pore spacing implies that on average an ion produced on the surface will have to travel a longer distance to reach a pore and will thus give rise to larger ohmic resistance or \(R_{surface}\) as is represented in Figure 6.

\(K_{pore}\) can be calculated because it is dependent only on pore length \(l_{pore}\) i.e., device thickness, and cross sectional surface area of all pores \(A_{pore}\) i.e., monolith porosity \(ϕ\). Assuming a uniform ionic current density over the pore volume, \(K_{pore}\) is obtained from

\[
K_{pore} = \frac{l_{pore}}{A_{pore}} \tag{5}
\]

Figure 7 depicts the contribution of pore and surface losses to total ohmic losses during water splitting. For large pore spacing (C and D) ohmic losses are dominated by surface losses but this tendency reverses for smaller spacing (A and B). With pores spaced less than 1 mm apart, surface ohmic losses become marginal but pore ohmic losses are still substantial.

These losses can only be mitigated by increasing the porosity or reducing the substrate thickness. For example, a device of 55 μm thickness will exhibit a 10-fold decrease in pore ohmic losses compared to a device with 550 μm thickness. Additionally, less concentrated electrolytes could be used while maintaining low ohmic losses, implying less stringent conditions for photoactive materials and catalysts.

Possible drawbacks of porous monoliths for solar hydrogen are the reduced surface area for light absorption, damage to the photosorbber, and product crossover. To counter these side effects, advanced fabrication methods, the introduction of molecular barriers, and photon management to maximize light absorption at nanoscale will be needed. The introduction of macro pores into photovoltaic devices has already been...
successfully demonstrated by Ernst et al.\textsuperscript{29} Carrier lifetimes were enhanced by passivation of pore walls with a thermally grown oxide layer.

\section*{CONCLUSIONS}

effective ionic transport management is a key element of the design of efficient, stable and cost-effective monolithic solar water splitting devices. Excessive ohmic losses due to long ion transport distances around flat PV–electrocatalyst assemblies confirm their inherently nonscalable nature. Perforating the monolithic assembly provides short ionic transport pathways and reduces ohmic losses to acceptable levels. Such porous monoliths were fabricated by laser ablation of oxidized silicon wafer coated with electrocatalysts. At a simulated STH efficiency of ca. 10\% and using KOH electrolyte, the ohmic losses are easily kept below 100 mV, provided a pore spacing of 1 mm or less is respected and 1 or 0.25 M KOH electrolyte is used. Low ohmic losses could even be achieved at reduced electrolyte concentrations which has the additional benefit of lowering the stringent requirement for both catalysts as well as encapsulation materials when working at extreme pH values.

At a pore spacing of 1 mm and less, a simple electrochemical circuit model suggests ohmic losses inside the pores start to dominate over surface ohmic losses. At lower device thickness, ohmic losses are expected to decrease further, even at lower porosity. Multiphysics and multiscale models of porous monoliths are needed to gain deeper insight in concentration, current and potential gradients depending on pore architecture. The results presented here show that porous monolithic solar water splitting devices are to be considered a viable option for large scale solar fuel production systems.

\section*{ASSOCIATED CONTENT}

\subsection*{Supporting Information}

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.jpcc.6b06766.

Detailed description of sample preparation, OER catalyst activation, electrochemical setup, CP measurements, ohmic losses calculations, galvanostatic EIS, and product crossover measurements (PDF)

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The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

\subsection*{Notes}

The authors declare no competing financial interest.

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\subsection*{REFERENCES}

(1) IEA. Hydrogen and Fuel Cells; 2015.


