

INT 145/88

PROGRAMME ISTART 4  
C o u r a n t d ' a c c r o c h a g e d ' u n g y r o t r o n  
t r a v a i l l a n t e n m o d e T E m p q

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42 GHz gyrotron ( $TE_{02}$ )	
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## 1. BUT DU PROGRAMME ISTART4

Dessiner le courant d'accrochage en fonction du champ magnétique statique  $B$ , pour différents modes  $TE_{mpq}$ .

A la différence du code ISTART3, on tient compte cette fois de l'indice axial  $q$ .

## 2. MODELE ET EQUATIONS UTILISEES

Le calcul analytique est basé sur les hypothèses suivantes:

Champ électrique dans la cavité cylindrique [1, 2]:

$$\underline{E} = (E_r \hat{r} + E_\phi \hat{\phi}) e^{i(\omega t + \psi)} \quad \text{avec:}$$

$$\begin{cases} E_r = i \frac{m}{k_{\perp} r} E_0 g(z) J_m(k_{\perp} r) e^{-im\phi} \\ E_\phi = E_0 g(z) J'_m(k_{\perp} r) e^{-im\phi} \end{cases}$$

A un instant donné, le champ électrique physiquement mesurable est la partie réelle de  $\underline{E}$ .

$$k_{\perp} = \frac{\nu_{mp}}{a} ; \quad \nu_{mp} : p^{\text{ième}} \text{ zéro non nul de } J'_m(x)$$

$a$  = rayon de la cavité

Le champ  $E$  a un profil sinusoïdal selon  $z$ , l'axe du faisceau d'électrons:

$$g(z) = \sin(k_{\parallel} z) \quad \text{avec } k_{\parallel} = \frac{q\pi}{L}$$

$L$  = longueur de la cavité ( $\neq L$  du programme ISTART3)

$L = 3/2 \cdot \text{FWHM}$  de  $g(z)$

La pulsation propre de la cavité est donnée par

$$\left(\frac{\omega}{c}\right)^2 = k^2 = k_{\perp}^2 + k_{\parallel}^2 \quad \text{d'où } \omega = c \sqrt{\left(\frac{\nu_{mp}}{a}\right)^2 + \left(\frac{q\pi}{L}\right)^2}$$

[1] Generalized Nonlinear Harmonic Gyrotron Theory, B.G. Danly and R.J. Temkin, PFC, MIT, April 85.

[2] High Frequency Gyrotrons and Their Application to Tokamak Plasma Heating, K.E. Kreisher and R.J. Temkin, Infrared and MM Waves, Vol. 7, chap. 8, 1983.

Le faisceau électronique est caractérisé par sa tension  $V_0$ , son anisotropie  $\alpha = \beta_{\perp} / \beta_{\parallel}$ , son rayon  $R_e$ .

$$\gamma_0 = 1 + \frac{eV_0}{mc^2} \quad ; \quad \beta_{\parallel} = \frac{w}{c} = \sqrt{\frac{1 - \gamma_0^{-2}}{1 + \alpha^2}} \quad ; \quad \beta_{\perp} = \frac{u}{c} = \alpha \beta_{\parallel}$$

Pulsation de Larmor non relativiste:  $\Omega_0 = \frac{eB_0}{m_e}$

Condition de résonance:  $\omega - \underline{k} \cdot \underline{v} = \Omega_0 / \gamma_0$

Soit, en projection:  $\omega + k_{\parallel} u = \Omega_0 / \gamma_0$

Il est alors d'usage de définir  $x = \frac{\Omega_0 / \gamma_0 - \omega}{k_{\parallel} u}$

Il y a résonance lorsque:  $\begin{cases} x = -1 & \text{avec l'onde progressive} \\ x = +1 & \text{avec l'onde rétrograde.} \end{cases}$

Bien que dans la cavité, l'onde stationnaire doit être une superposition de ces 2 ondes, c'est la condition  $x = -1$  qui est intéressante en pratique. (Voir la discussion dans [1].)

En fonction de  $x$ , le champ magnétique s'écrit:  $B_0 = \frac{m_e \gamma_0}{e} (\omega + x k_{\parallel} u)$

Le courant d'accrochage en Ampères est alors donné par

$$I = \frac{\epsilon_0 m_e}{e} \frac{\omega}{Q_{mpq}} |P_0|^2 \frac{(k_{\parallel} u)^2}{G(R_e)} \left[ \beta_{\perp}^2 \frac{dF_c}{dx} - 2 F_c \right]$$

avec:

$$|P_0|^2 = \frac{\pi L}{2} k^{-2} (\gamma_{mp}^2 - m^2) J_m^2(\gamma_{mp})$$

$$G(R_e) = J_{m\pm 1}^2(k_{\perp} R_e)$$

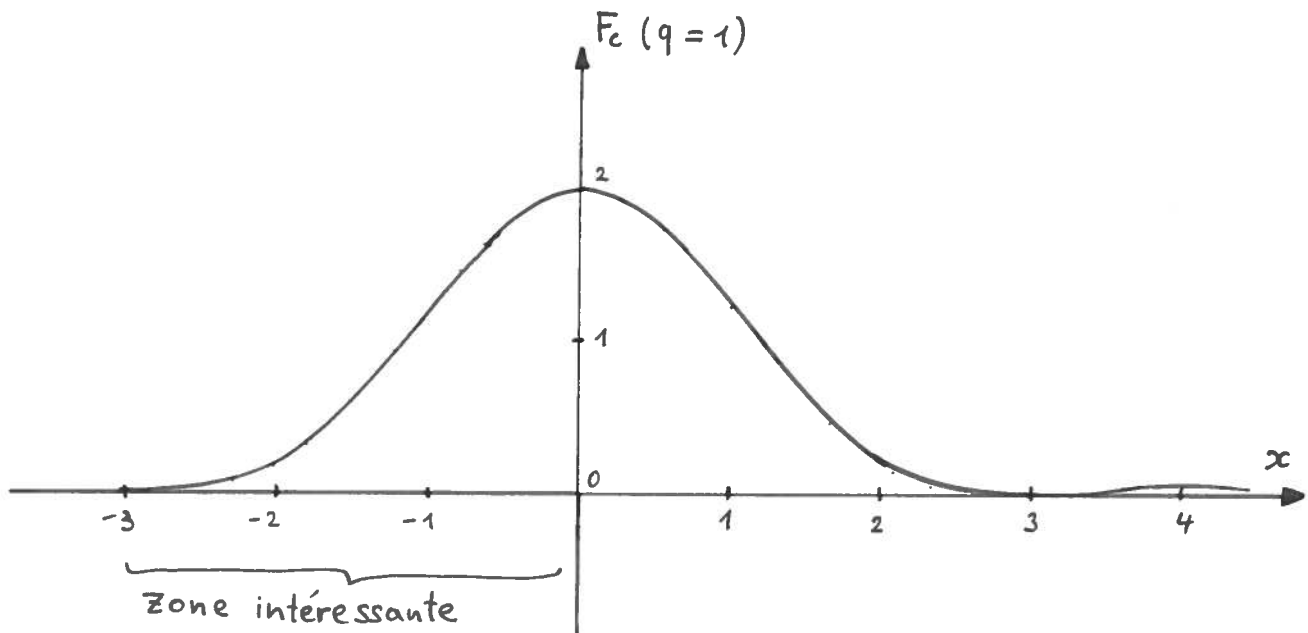
$$F_c(x, q) = \frac{2}{(1-x^2)^2} \sin^2 \frac{(x+1)\pi q}{2}$$

$$s = \frac{\Omega_0}{\gamma_0 k_{\parallel} u}$$

$Q_{mpq}$  = facteur de qualité du mode  $TE_{mpq}$

$J_{m\pm 1}$  : le signe dépend de la polarisation du mode ( $\pm im\phi$ ).  
Donc pour  $m \neq 0$ , il y aura 2 courbes  $I(B_0)$ .

Allure de  $F_c(x, q)$  :



En posant  $F_c = 2f^2$  avec  $f = \frac{1}{1-x^2} \sin \frac{(x+1)\pi q}{2}$

On a  $\lim_{x \rightarrow -1} f = \frac{\frac{x+1}{2} \pi q}{(1+x)(1-x)} = \lim_{x \rightarrow -1} \frac{\pi q}{2} \frac{1}{1-x} = \frac{\pi q}{4}$  d'où  $\lim_{x \rightarrow -1} F_c = \frac{\pi^2 q^2}{8}$

$$F' = 4ff'$$

$$\lim_{x \rightarrow -1} f' = \frac{\pi q}{2} \lim_{x \rightarrow -1} \left( \frac{1}{1-x} \right)' = \lim_{x \rightarrow -1} \frac{\pi q}{2} \frac{1}{(1-x)^2} = \frac{\pi q}{8}$$

$$\text{d'où } \lim F'_c = 4 \frac{\pi q}{4} \frac{\pi q}{8} = \frac{\pi^2 q^2}{8}$$

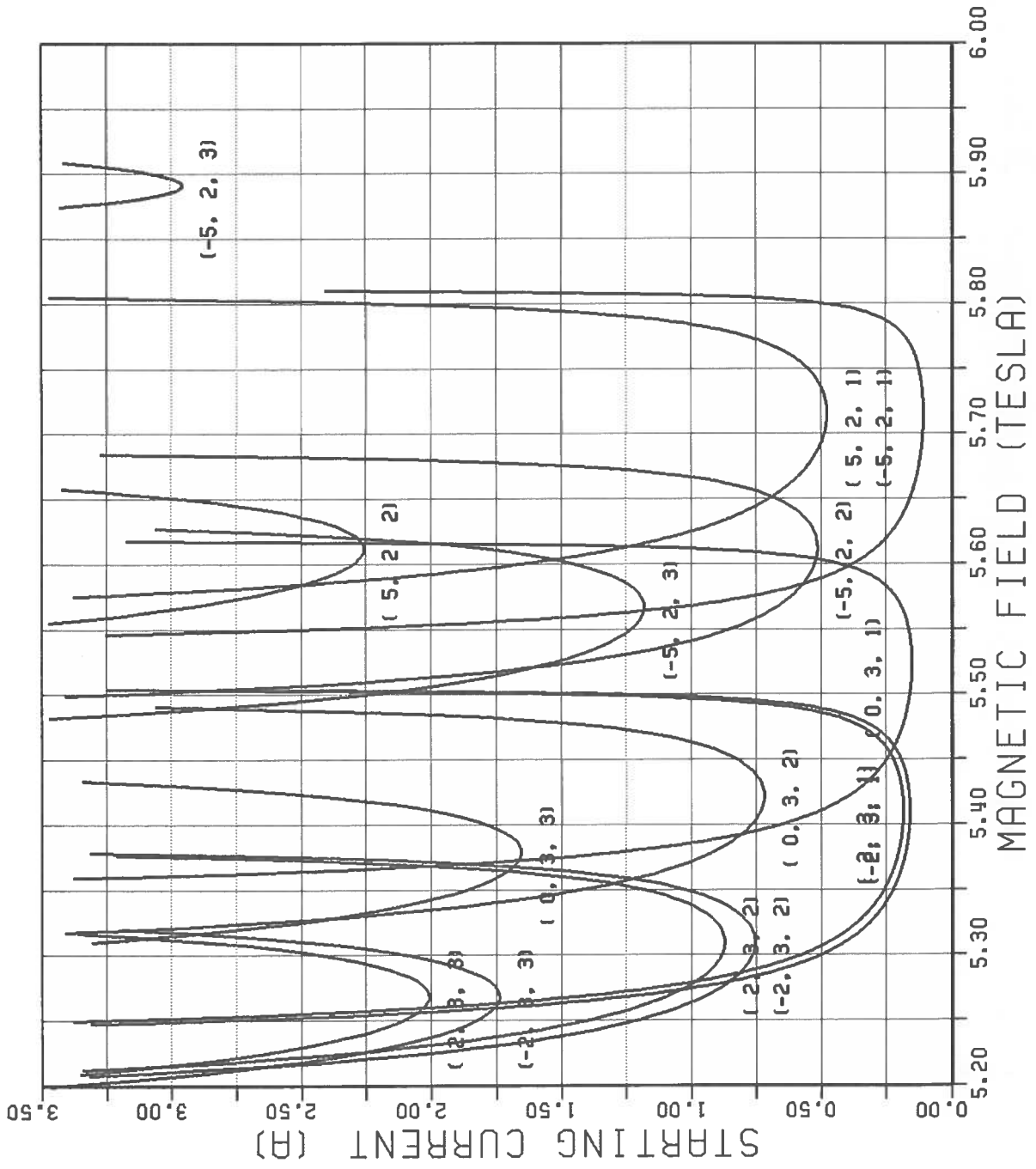
Pour  $x \rightarrow +1$ :  $\lim f = -\frac{\pi q}{4}$  ;  $\lim F_c = \frac{\pi^2 q^2}{8}$  ;  $\lim F' = -\frac{\pi^2 q^2}{8}$  .



MIT 140 GHZ GYROTRON  
 =====

CRPP - 88/07/11. 14.31.25.  
 GYROTRON PROJECT

STARTING CURRENT VERSUS STATIC MAGNETIC FIELD PROGRAM ISTART4

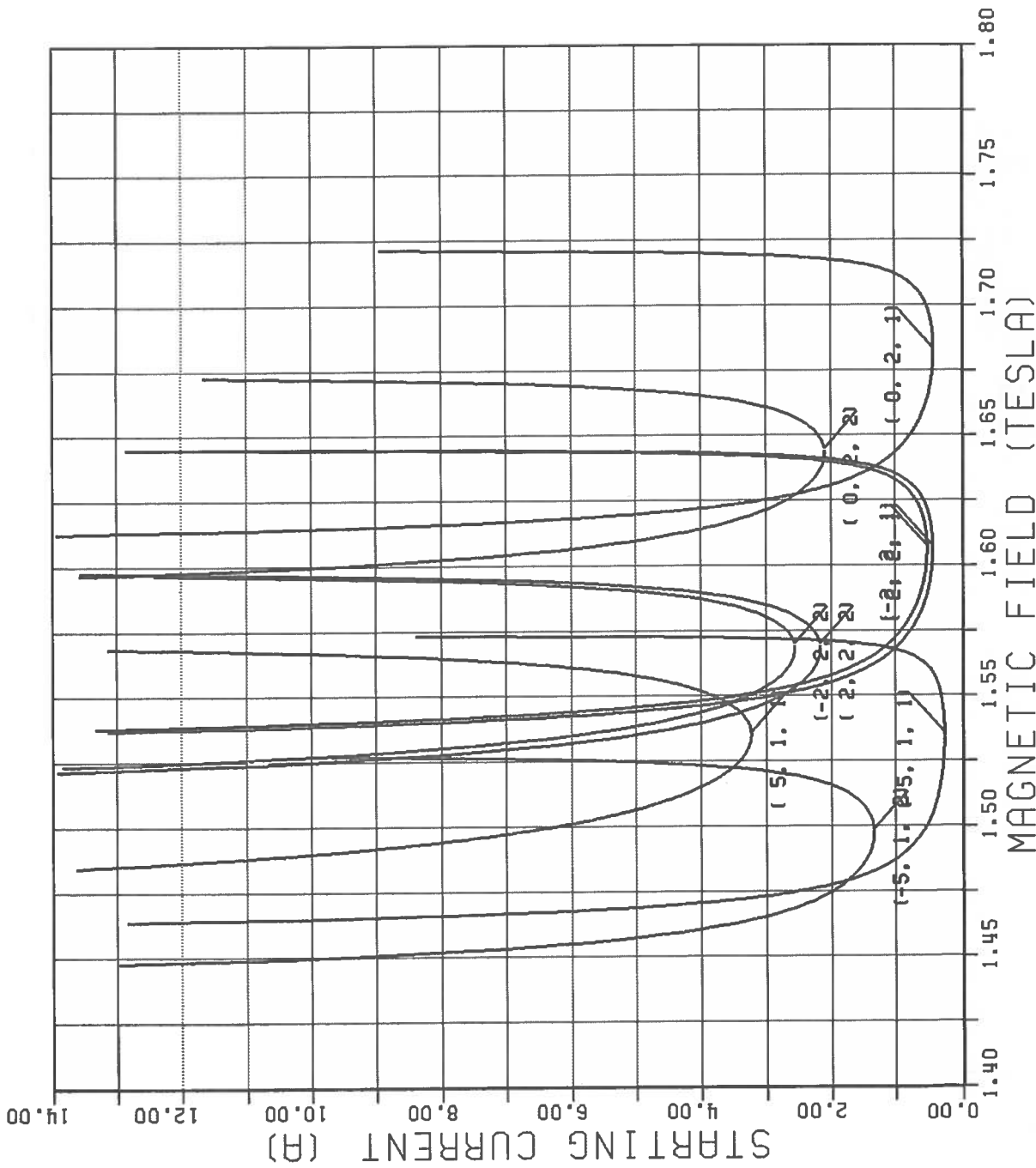


MODE	L [CM]	Q	FREQUENCY [GHZ]
TE (0, 3, 1)	15.0	1450.	140.244
TE (0, 3, 2)	15.0	963.	141.309
TE (0, 3, 3)	15.0	161.	143.064
TE (2, 3, 1)	15.0	1400.	137.447
TE (2, 3, 2)	15.0	350.	138.532
TE (2, 3, 3)	15.0	156.	140.323
TE (5, 2, 1)	15.0	1300.	144.996
TE (5, 2, 2)	15.0	325.	146.025
TE (5, 2, 3)	15.0	144.	147.725

RESONATOR RADIUS: 3.47 MM  
 GAMMA: 1.1272  
 ALPHA: 1.5000  
 BEAM VOLTAGE: 65.00 KV  
 ANNULAR BEAM RADIUS: 1.82 MM  
 HARMONIC #: 1

42 GHz Gyrotron

STARTING CURRENT VERSUS STATIC MAGNETIC FIELD PROGRAM ISTART4



CRPP - 88/07/09. 10.45.06.  
GYROTRON PROJECT

RESONATOR RADIUS: 8.00 MM  
GAMMA: 1.1566  
ALPHA: 1.5000  
BEAM VOLTAGE: 80.00 KV  
ANNULAR BEAM RADIUS: 6.00 MM  
HARMONIC #: 1

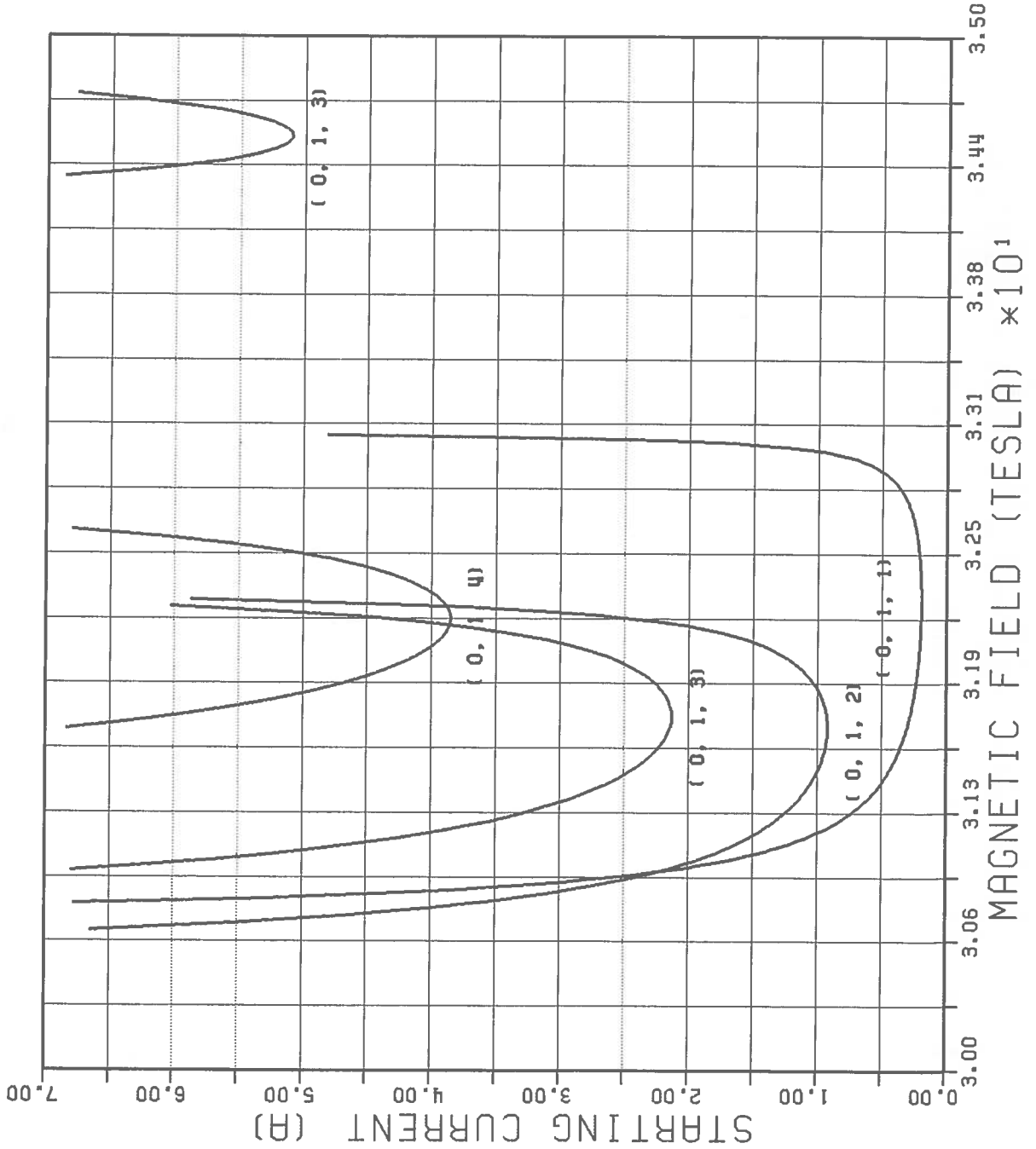
MODE	L [MM]	Q	FREQUENCY [GHZ]
(0, 2, 1)	40.0	618.	42.010
(0, 2, 2)	40.0	155.	42.508
(2, 2, 1)	40.0	556.	40.172
(2, 2, 2)	40.0	139.	40.693
(5, 1, 1)	40.0	503.	38.447
(5, 1, 2)	40.0	126.	38.991



8 GHz GYROTRON

CAPP - 88/07/11. 14.20.52.  
GYROTRON PROJECT

STARTING CURRENT VERSUS STATIC MAGNETIC FIELD PROGRAM ISTART4



RESONATOR RADIUS: 22.80 MM  
GAMMA0: 1.1566  
ALPHA: 1.8900  
BEAM VOLTAGE: 80.00 KV  
ANNULAR BEAM RADIUS: 11.18 MM  
HARMONIC # : 1

MODE	L [MM]	Q	FREQUENCY [GHZ]
( 0, 1, 1)	164.0	227.	8.071
( 0, 1, 2)	164.0	57.	8.224
( 0, 1, 3)	164.0	25.	8.474
( 0, 1, 4)	164.0	14.	8.813

PROGRAM ISTART4 (INPUT, OUTPUT, TAPES=INPUT, TAPE6=OUTPUT)  
 COMPUTATION OF THE STARTING CURRENT OF A CONVENTIONAL GYROTRON  
 OPERATING NEAR THE FUNDAMENTAL OF THE LARMOR FREQUENCY

PLOT ON VERSATEC (CYBER)  
 - MODE TE(M,P,G) (SIMPLE CAVITY)  
 - ANALYTICAL APPROXIMATION (LINEAR REGIME)  
 - MKSA UNITS  
 - DOCUMENTATION: INT 145/88

ANDRE PERRENDOU CRPP/EPFL VERSION 1 09 JULY 1988

PARAMETERS  
 NMAX NUMBER OF MODES (M,P)  
 NPOINT MAX NUMBER OF B FIELD POINTS  
 MMAX MAX AZYMUTHAL INDEX ( MMAX < 51 )  
 IPMAX MAX RADIAL INDEX  
 IGMAX MAX AXIAL INDEX

INPUT DATA  
 NCAS NUMBER OF (M,P) MODES TO BE CONSIDERED  
 MAXG MAX AXIAL INDEX  
 MM(1... NCAS) TOTAL NUMBER OF CCOMPUTED URVES WILL BE NCAS\*MAXG  
 PP(1... NCAS) AZYMUTHAL INDEX  
 QQ(1... NCAS) RADIAL INDEX  
 LL(1... NCAS) QUALITY FACTOR OF MODE TE(M,P,1)  
 A CAVITY LENGTH OF MODE TE(M,P,1)  
 BMIN RADIUS OF RESONATOR (CYLINDRICAL CAVITY)  
 BMAX LOWEST VALUE OF B FIELD ( " " )  
 IAMAX HIGHEST VALUE OF CURRENT ( " " )  
 VO HIGHEST VALUE OF CURRENT ( " " )  
 ALPHA BEAM VOLTAGE  
 RE BEAM ANISOTROPY (VPERP/VPARA)  
 BEAM RADIUS

PARAMETER (NMAX=10, NPOINT=300, MMAX=5, IPMAX=5, IGMAX=5)  
 INTEGER P, PP  
 REAL IAMAX, IA, MUO, L, LL, LAMBDA, KRE, KPERP, KPARA,  
 \* KPU, NUMP, JMNUMP, JMPN  
 DIMENSION BO(NPOINT), IA(NPOINT), BJZP(MMAX+1, IPMAX), BJ(50)  
 CHARACTER DATE\*10, TIME\*10, DATE1\*10, TIME1\*10, LABEL\*80

COMMON /TITRE1/ LABEL(2)  
 COMMON /TITRE2/ DATE1, TIME1  
 COMMON /BEAM/ VO, ALPHA, RE, GAMMAO  
 COMMON /CAVITY/ A, M, P, IQ, ISIG, MAXG  
 COMMON /MODE/ NCAS, MM(NMAX), PP(NMAX), QQ(NMAX), LL(NMAX),  
 \* FREQ(NMAX, IGMAX)  
 COMMON /PAGE/ XA4, YA4, DXL, DXR, DYU, DYD, CH, XO, YO, AXEX, AXEY

NAMELIST /GYRO/ NCAS, MM, PP, QQ, LL, MAXG, BMIN, BMAX, IAMAX,  
 \* VO, ALPHA, RE, A

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60 C 1. CAS STANDARD (BENCHMARK)
61 DATA LABEL(1) / 'M I T 1 4 0 G H Z G Y R O T R O N' /
62 DATA LABEL(2) / '======' /
63 DATA NCAS/1/, MAXG/3/
64 DATA MM(1), PP(1), GG(1), LL(1)/0, 3, 1450., 0.0150/
65 DATA MM(2), PP(2), GG(2), LL(2)/2, 3, 1400., 0.0150/
66 DATA MM(3), PP(3), GG(3), LL(3)/5, 2, 1300., 0.0150/
67 DATA VO, ALPHA, RE, A/ 65000., 1.5, 1.82E-03, 3.47E-03/
68 DATA BMIN, BMAX, IMAX/ 5.2, 6.0, 7.0/
69
70 C DO 10 NC= NCAS+1, NMAX
71 MM(NC)=0
72 PP(NC)=0
73 GG(NC)=0
74 LL(NC)=0.
75
76 C
77 C 2. CONSTANTS
78
79 C DATA CLIGHT/2.99792458E+08/
80 DATA EMASS,ECHARG/9.1093897E-31, 1.60217733E-19/
81 PI = ACOS(-1.)
82 MUO = 4.E-07*PI
83 EPSO = 1./ (MUO*CLIGHT**2)
84
85 C DATE1=DATE()
86 TIME1=TIME()
87 WRITE(6,100) DATE1, TIME1
88 FORMAT('1'///, 'PROGRAM ISTART4',4X,2A10/
89 * '======'//)
90
91 C
92 WRITE (6,105)
93 FORMAT ('ZEROS OF DERIVATIVES OF BESSEL FUNCTIONS')
94 CALL BEPZERO(BJZP,MMAX,IPMAX)
95
96 C
97 C 3. READ INPUT DATA
98
99 C REWIND (5)
100 READ (5, '(A)') LABEL
101 WRITE (6, '(//1X,A//)') LABEL
102 READ (5, GYRO)
103 WRITE (6, GYRO)
104
105 C GAMMAO = 1. + (ECHARG*VO)/(EMASS*CLIGHT**2)
106 BPARA = SQRT ((1.-1./GAMMAO**2)/(1.+ALPHA**2))
107 BPERP = ALPHA * BPARA
108 WRITE (6,110) 'GAMMAO =', GAMMAO
109 FORMAT (1X,A,G14.6)
110 WRITE (6,110) 'BETA PERP =', BPERP
111 WRITE (6,110) 'BETA PARA =', BPARA
112
113 C CF = EPSO*EMASS/ECHARG
114 WRITE (6,110) 'CONST =', CF
115
116 C
117 C 4. CALCULS
118
119 C IF (MAXQ.GT. IQMAX) STOP 'AXIAL INDEX Q TOO LARGE'
120 IFIRST = 1

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121 DO 490 NC=1,NCAS
122 M = MM(NC)
123 P = PP(NC)
124 Q = QQ(NC)
125 L = LL(NC)
126 IF (M .GT. MMAX) STOP ' M TOO LARGE '
127 IF (P .GT. IPMAX) STOP ' P TOO LARGE '
128 NUMP = BJZP(M+1,P)
129 CALL BESSEL (M, NUMP,BJ)
130 JMNUMP = BJ(M+1)
131
132 C
133 WRITE (6,120) M,P
134 FORMAT (///, MODES TE(' , I2, ' , I2, ' , * )' /
135 * =====//)
136 WRITE (6,110) ' INTERACTION LENGTH= ' , L
137 WRITE (6,110) ' NUMP = ' , NUMP
138 WRITE (6,110) ' JM (NUMP) = ' , JMNUMP
139
140 C
141 KPERP = NUMP/A
142 WRITE (6,110) ' KPERP ' , KPERP
143 KRE = KPERP*RE
144 WRITE (6,110) ' KPERP*RE ' , KRE
145 POZ = 0.5*PI*L*(NUMP**2 - M**2)*JMNUMP**2 /KPERP**2
146
147 C
148 NSIG = 2
149 IF (M.EQ.O) NSIG=1
150 DO 480 NS=1,NSIG
151 ISIG = 3 - 2*NS
152 MN = M + ISIG
153 IF (M.NE.O) WRITE (6,435) ISIG
154 FORMAT (/, ROTATING MODE: ' , I2)
155 CALL BESSEL (MN, KRE, BJ)
156 JMPN = BJ(MN+1)
157 WRITE (6,110) ' JMPN = ' , JMPN
158 GRE = JMPN**2
159 WRITE (6,110) ' G(RE) = ' , GRE
160
161 C
162 DO 470 IQ= 1,MAXG
163 WRITE (6,125) M,P, IQ
164 FORMAT (///, MODE TE(' , I2, ' , I2, ' , I2, ' )' /
165 * -----//)
166 KPARA = (IQ*PI)/L
167 WRITE (6,110) ' KPARA ' , KPARA
168 OMEGA = CLIGHT * SQRT(KPERP**2 + KPARA**2)
169 GMPQ = Q/(IQ**2)
170 FREQ(NC, IQ) = OMEGA/(2.*PI)
171 WRITE (6,110) ' FREQUENCY = ' , FREQ(NC, IQ)
172 LAMBDA = CLIGHT/FREQ(NC, IQ)
173 WRITE (6,110) ' WAVELENGTH = ' , LAMBDA
174 WRITE (6,110) ' QUALITY FACTOR = ' , GMPQ
175 KPU = KPARA*BPARA*CLIGHT
176 WRITE (6,110) ' KPU ' , KPU
177
178 C-----
179 C
180 C 5. COMPUTES POINTS (BO, IA) FOR -3. < X < 0.
181
182 J = 0
183 DX = 3./NPOINT
184 X = -3.
185 IF (X.GE.O.) GOTO 440

```



SUBROUTINE CFCQ 74/855 OPT=1, ROUND= A/ S/ M/ -D, -DS FTN 5. 1+670 88/07/12. 17. 09. 57  
 DO=-LONG/-OT, ARG=-COMMON/-FIXED, CS= USER/-FIXED, DB=-TB/-SB/ -SL/ -ER/ -ID/ -PMD/ -ST, -AL, PL=5000  
 FTN5, I=ISTART4, L=LIS, ANSI=0, LO=S/-A, PN.

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C
SUBROUTINE CFCQ(X, IQ, PI, FC, DFC)
  PIQ2 = 0.5*PI*IQ
  UNPX = 1. +X
  UNMX = 1. -X
  IF (ABS(UNPX).LT.0.001) THEN
    F = 0.5*PIQ2
    DF = 0.5*F
  ELSE IF (ABS(UNMX).LT.0.001) THEN
    F = 0.5*PIQ2
    DF = -0.5*F
  ELSE
    UNMX2 = UNPX*UNMX
    F = SIN(PIQ2*UNPX) / UNMX2
    DF = (PIQ2*COS(PIQ2*UNPX) + 2. *X*F) / UNMX2
  ENDIF
  FC = 2. *F*F
  DFC = 4. *F*DF
END
C

```

```

1 SUBROUTINE BEPZERO(BJZP, M, N)
2
3 C COMPUTES THE ZEROES OF THE DERIVATIVES OF BESSEL FUNCTION
4 C OF INTEGER ORDER (M=0, 1, 2, . . . 5)
5 C
6 C ON RETURN: BJZP(K+1, L) = LTH ZERO OF J'K(X) (L = 1, 2 3. . . N)
7 C
8 C PARAMETER (EPS=1.E-12, MMAX=5, IPMAX=5)
9 C
10 C DIMENSION BJZP(MMAX+1, IPMAX), BJ(50)
11 C
12 C PI =ACOS(-1.)
13 C IF (M.GE.0 .AND. M.LE.MMAX) GOTO 5
14 C WRITE (6,1) M
15 C FORMAT (' SUBROUTINE BEPZERO CALLED WITH M=', I3)
16 C STOP
17 C IF (N.GE.1 .AND. N.LE.IPMAX) GOTO 10
18 C WRITE (6,2) N
19 C FORMAT (' SUBROUTINE BEPZERO CALLED WITH N=', I3)
20 C STOP
21 C
22 C FIND ROOTS USING NEWTON ALGORITHM FOR J'M(X)=0
23 C
24 C DO 30 IM=0, M
25 C DO 30 IN=N, 1, -1
26 C
27 C IF (IN.GE.N-1) THEN
28 C
29 C     X0 = PI/4. * (2*IM + 4*IN -3)
30 C     IF (IM.EQ.0) X0 = X0 + PI
31 C     ELSE
32 C     X0 = 2*BJZP(IM+1, IN+1) - BJZP(IM+1, IN+2)
33 C     ENDIF
34 C     ITER=0
35 C
36 C     NEWTON SCHEME: X1 = X0 - JM'(X0)/JM"(X0)
37 C
38 C CALL BESSEL(IM+2, X0, BJ)
39 C BJM = BJ(IM+1)
40 C BJMP = -BJ(IM+2) + IM/X0*BJM
41 C BJMP1P = -BJ(IM+3) + (IM+1)/X0*BJ(IM+2)
42 C BJM2P = -BJMP1P + IM/X0*(BJMP - BJM/X0)
43 C X1 = X0 - BJMP/BJM2P
44 C ITER = ITER + 1
45 C IF (ABS(X1-X0) .LT. EPS) GOTO 20
46 C X0=X1
47 C IF (ITER.LT.50) GOTO 15
48 C WRITE (6,16) IM, IN
49 C FORMAT (' NO CONVERGENCE REACHED FOR M=', I3, ' N=', I3)
50 C X1=0.
51 C BJZP(IM+1, IN)=X1
52 C WRITE (6,17) IM, IN, X1, ITER
53 C FORMAT (' J'(', I3, ', ', I3, ') = ', F12.8, ' ITER=', I3)
54 C CONTINUE
55 C END

```

```

1 SUBROUTINE BESSEL(LMAX, X, BJ)
2
3 C
4 CALCULATE BESSEL FUNCTIONS BY BACKWARD RECURSION
5
6 C
7 ON RETURN: BJ(1)=JO(X), BJ(2)=J1(X), ... BJ(LMAX+1)=BJLMAX(X)
8
9 C
10 PARAMETER (XMIN=.00001, XMAX=100., MSTART=200, DEL=1.E-60)
11 DIMENSION TEMP(MSTART), BJ(*)
12
13 C
14 IF ( LMAX .GT. 50 ) STOP 'BESSEL: ORDER TOO BIG'
15 IF (ABS(X).GT.XMAX) STOP 'BESSEL: ARGUMENT TOO BIG'
16 IF (ABS(X).GT.XMIN) GOTO 20
17 BJ(1)=1.
18 IF (LMAX.EQ.0) RETURN
19 DO 10 L=1, LMAX
20 BJ(L+1)=X/FLOAT(2*L)*BJ(L)
21 RETURN
22
23 C
24 LSTART=2*(5*INT(ABS(X))+(LMAX+1)/2+10)+1
25 ORDER OF HIGHEST BESSEL FUNCTION IS EVEN TO GUARANTEE CORRECT
26 C..... PARITY (JN(X) = (-1)**N *JN(-X) )
27 IF (LSTART.GT.MSTART) LSTART=MSTART
28 TEMP(LSTART)=DEL
29 TEMP(LSTART-1)=DEL*FLOAT(2*(LSTART-2))/X
30 DO 30 L=LSTART-1, 2, -1
31 TS=TEMP(LSTART)**2
32 TEMP(L-1)=FLOAT(2*(L-1))/X*TEMP(L)-TEMP(L+1)
33 TS=1./SQRT(TEMP(L)**2)
34 DO 40 L=1, LMAX+1
35 BJ(L)=TS*TEMP(L)
36 RETURN
37 END

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```

1 SUBROUTINE PLOTST(BO,IA,J, BMIN,BMAX,IAMAX,IFIRST)
2 C
3 COMMON /PAGE/ XA4,YA4,DXL,DXR,DYU,DYD, CH, XO,YO,AXEX,AXEY
4 C
5 REAL BO(*), IA(*), IAMAX, IAKM1
6 INTEGER P
7 CHARACTER T*20
8 C
9 COMMON /CAVITY/ A, M, P, IQ, ISIG, MAXQ
10 C
11 DATA XA4,YA4/29.,21./, DXL,DXR,DYU,DYD/3.,2.,2.5,3./, CH/O.2/
12 DATA XO,YO,AXEX,AXEY/3.,2.5,16.,14./
13 C
14 IF (IFIRST.EQ.O) GOTO 25
15 CALL PLOTS ('VERSATEC',100.,8224,0,1)
16 C
17 CALL FRAME(BMIN,BMAX,O.,IAMAX, XO,YO,AXEX,AXEY)
18 CALL CHPEN(3)
19 IFIRST=O
20 C
21 CONTINUE
22 IPEN=3
23 IPL = O
24 DO 30 K=1,J
25 CURR=IA(K)
26 IF (CURR.LT.O. .OR. CURR.GT. IAMAX) THEN
27 IPEN=3
28 IPL =O
29 IAKM1=IAMAX+1.
30 ELSE
31 XX = XO + (BO(K)-BMIN)/(BMAX-BMIN) * AXEX
32 YY = YO + CURR/IAMAX * AXEY
33 CALL PLOT(XX,YY,IPEN)
34 DIA = CURR-IAKM1
35 IAKM1=CURR
36 IF (DIA.GT.O. .AND. IPL.EQ.O .AND. IPEN.EQ.2) THEN
37 WRITE MODE #
38 XYP = XX - 1.2
39 YYP = YY - 0.5
40 IF (YYP.LT.(YO+O.5)) YYP = YYP + 1.
41 WRITE (T,50) ISIG*M, P, IQ
42 FORMAT( ',I2,',',I2,',',I2,',',I2,',')
43 CALL SYMBOL(XXP,YYP,O.2,T,O.,10)
44 IPL = 1
45 CALL PLOT(XX,YY,3)
46 ENDIF
47 IPEN=2
48 END IF
49 CONTINUE
50 END

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1 SUBROUTINE FRAME(BMIN,BMAX,ISMIN,ISMAX)
2 COMMON /PAGE/ XA4,YA4,DXL,DXR,DYU,DYD, CH, XO,YO,AXEX,AXEY
3
4 REAL ISMIN,ISMAX
5
6 DATA MASK/0"5252525252525252525252"/
7
8 CH = CHARACTER HEIGHT
9
10 A4 FRAME
11 CALL CHPEN(2)
12 CALL PLOT(O, 1, 3)
13 CALL PLOT(O, 0, 2)
14 CALL PLOT(1, 0, 2)
15 CALL PLOT(XA4-1, 0, 3)
16 CALL PLOT(XA4, 0, 2)
17 CALL PLOT(XA4, 1, 2)
18 CALL PLOT(XA4-1, YA4, 3)
19 CALL PLOT(XA4, YA4, 2)
20 CALL PLOT(XA4, YA4-1, 2)
21 CALL PLOT(O, YA4-1, 3)
22 CALL PLOT(O, YA4, 2)
23 CALL PLOT(1, YA4, 2)
24
25 AXES AND GRID
26
27 DB=(BMAX-BMIN)/AXEX
28 CALL AXIS(XO,YO,AXEX,O, BMIN,DB, 'MAGNETIC FIELD (TESLA)',22)
29
30 DIS=(ISMAX-ISMIN)/AXEY
31 CALL AXIS(XO,YO,AXEY,90, ISMIN,DIS, 'STARTING CURRENT (A)',-20)
32 CALL CHPEN(3)
33 CALL PLOT(XO,YO,3)
34 CALL PLOT(XO,YO+AXEY,2)
35 CALL PLOT(XO+AXEX,YO+AXEY,2)
36 CALL PLOT(XO+AXEX,YO,2)
37 CALL PLOT(XO,YO,2)
38 CALL CHPEN(1)
39 IAXEX=AXEX
40 IAXEY=AXEY
41 CALL GRID(XO,YO, IAXEX,1, IAXEY,1, MASK)
42 CALL CHPEN(2)
43 RETURN
44 END
45

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1  SUBROUTINE TITLE
2
3  C
4  PARAMETER (NMAX=10, IQMAX=5)
5  COMMON /PAGE/ XA4, YA4, DXL, DXR, DYU, DYD, CH, XO, YO, AXEX, AXEY
6  COMMON /TITRE1/ LABEL(2)
7  COMMON /TITRE2/ DATE1, TIME1
8  COMMON /BEAM/ VO, ALPHA, RE, GAMMAO
9  COMMON /CAVITY/ A, M, P, IQ, ISIG, MAXG
10 COMMON /MODE/ NCAS, MM(NMAX), PP(NMAX), QQ(NMAX), LL(NMAX),
11 * FREQ(NMAX, IQMAX)
12
13 C
14 INTEGER P, PP
15 REAL LL
16 CHARACTER T*80, DATE1*10, TIME1*10, LABEL*80
17 YTOP=YA4-DYU
18 CALL CHPEN(2)
19 CALL SYMBOL(DXL, YTOP, CH, LABEL(1), O., 80)
20 CALL SYMBOL(DXL, YTOP-2., *CH, CH, LABEL(2), O., 80)
21 WRITE(T, 100)
22 FORMAT('STARTING CURRENT VERSUS STATIC MAGNETIC FIELD', 5X,
23 * 'PROGRAM ISTART4')
24 CALL SYMBOL(DXL, YTOP-5., *CH, CH, T, O., 66)
25
26 C
27 WRITE(T, 1) DATE1, TIME1
28 FORMAT('CRPP - ', 2A10)
29 CALL SYMBOL(O.8*XA4, YTOP, O.8*CH, T, O., 27)
30 WRITE(T, 2)
31 FORMAT('GYROTRON PROJECT')
32 CALL SYMBOL(O.8*XA4, YTOP-2., *CH, O.8*CH, T, O., 16)
33
34 XT=XO+AXEX+1.
35 YT=YO+AXEY
36 WRITE(T, 3) A*1000.
37 FORMAT('RESONATOR RADIUS: ', F7.2, ' MM')
38 CALL SYMBOL(XT, YT, CH, T, O., 27)
39 YT=YT-2.*CH
40 WRITE(T, 7) GAMMAO
41 FORMAT('GAMMAO: ', F7.4)
42 CALL SYMBOL(XT, YT, CH, T, O., 14)
43 YT=YT-2.*CH
44 WRITE(T, 8) ALPHA
45 FORMAT('ALPHA: ', F7.4)
46 CALL SYMBOL(XT, YT, CH, T, O., 14)
47 YT=YT-2.*CH
48 WRITE(T, 9) VO/1000.
49 FORMAT('BEAM VOLTAGE: ', F6.2, ' KV')
50 CALL SYMBOL(XT, YT, CH, T, O., 22)
51 YT=YT-2.*CH
52 WRITE(T, 10) RE*1000.
53 FORMAT('ANNULAR BEAM RADIUS: ', F6.2, ' MM')
54 CALL SYMBOL(XT, YT, CH, T, O., 29)
55 YT=YT-2.*CH
56 WRITE(T, 11) 1
57 FORMAT('HARMONIC # : ', I2)
58 CALL SYMBOL(XT, YT, CH, T, O., 14)
59
60 C
61 YT=YT-3.*CH
62 T=' MODE
63 CALL SYMBOL(XT, YT, CH, T, O., 35)
64
65 C
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60 YT=YT-2.*CH
61 T=TE
62 CALL SYMBOL(XT, YT, CH, T, O., 35)
63 DO 20 NC=1, NCAS
64 DO 20 IGG=1, MAXG
65 YT=YT-2.*CH
66 WRITE(T, 21) MM(NC), PP(NC), IGG, LL(NC)*1000., GG(NC)/IGG**2,
67 * FORMAT(' ', I2, ', ', I2, ', ', I2, ', ', I2, ', ', F7.1, F7.0, F9.3)
68 CALL SYMBOL(XT, YT, CH, T, O., 34)
69
70 RETURN
71 END
72

```

21  
20  
C