



France

Setting the Standard for Automation™

Real-Time Optimization of Industrial Processes

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En partenariat avec



Maîtrise et optimisation des processus complexes – Angers - 22 octobre 2014

Outline

1. Optimization of process operation
 - Numerical vs. real-time optimization
 - Static optimization for continuous and batch plants
2. Real-time optimization schemes
 - Two explicit strategies (repeat numerical optimization)
 - One implicit strategy (use feedback control)
3. Experimental cases studies
 - Fuel-cell stack (a continuous plant)
 - Batch polymerization (a batch plant)
4. Conclusions

Ideas

Concepts



Optimization of a Continuous Plant

Disturbances

Long term
week/month

Market Fluctuations,
Demand, Price

Medium term
day

Catalyst Decay,
Changing Raw
Material Quality

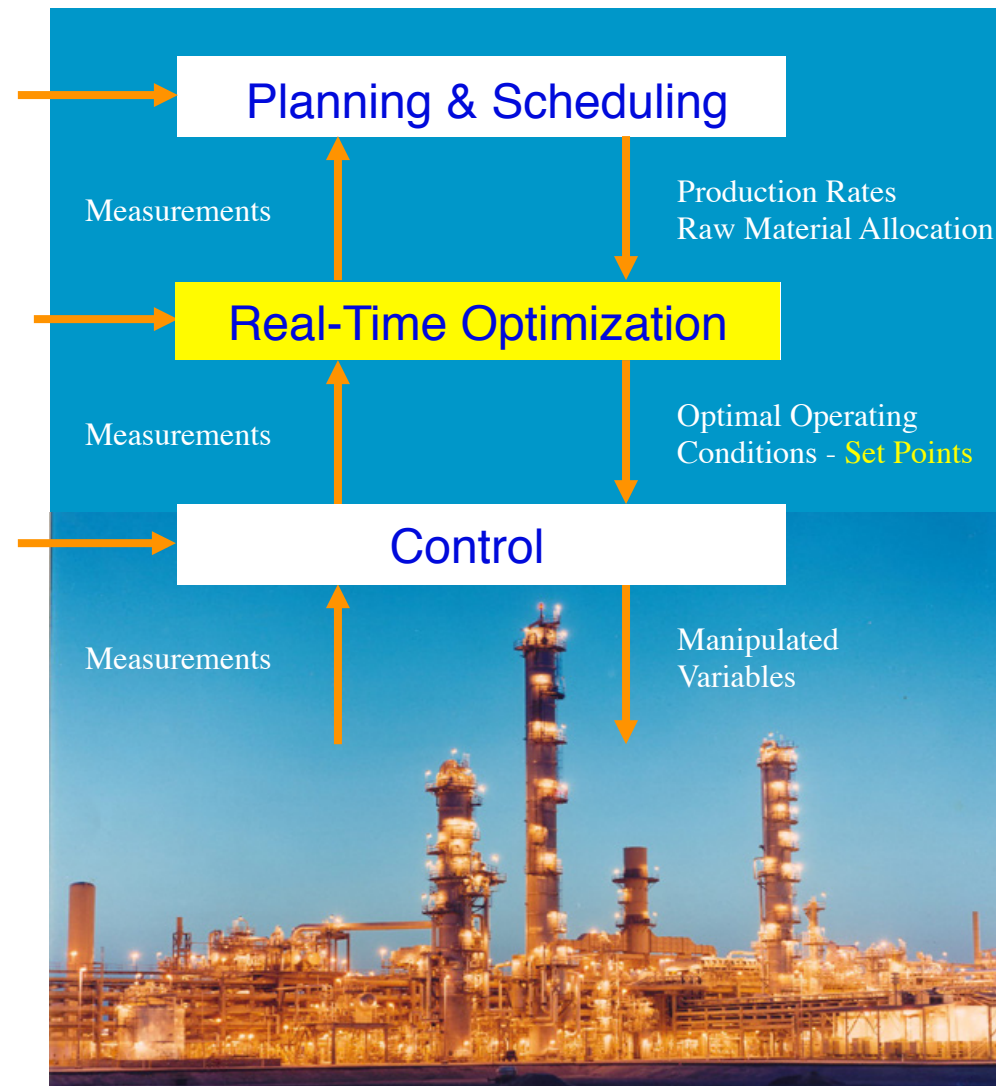
Short term
second/
minute

Fluctuations in
Pressure, Flow
Rates, Compositions

Large-scale complex
processes

Changing conditions
→ Real-time adaptation
of set points

Decision Levels



Optimization of a Continuous Plant

Problem formulation

Optimize the steady-state **performance** of a (dynamic) process
while satisfying a number of operating **constraints**

Plant

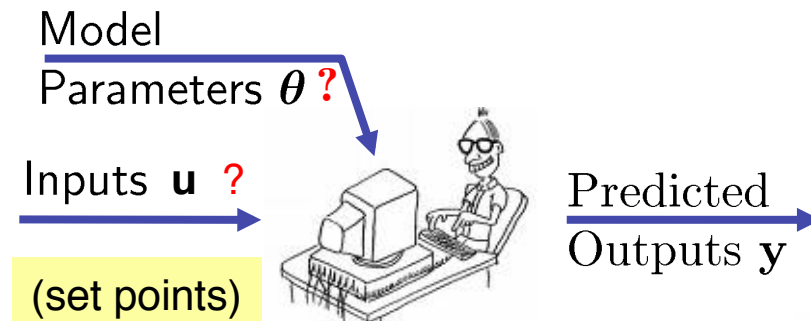
$$\begin{aligned} \min_{\mathbf{u}} \quad & \phi_p(\mathbf{u}, \mathbf{y}_p) \\ \text{s. t.} \quad & \mathbf{g}_p(\mathbf{u}, \mathbf{y}_p) \leq \mathbf{0} \end{aligned}$$



Model-based Numerical Optimization

$$\begin{aligned} \mathbf{F}(\mathbf{u}, \mathbf{y}, \boldsymbol{\theta}) &= \mathbf{0} \\ \min_{\mathbf{u}} \quad & \Phi(\mathbf{u}, \boldsymbol{\theta}) := \phi(\mathbf{u}, \mathbf{y}) \\ \text{s. t.} \quad & \mathbf{G}(\mathbf{u}, \boldsymbol{\theta}) := \mathbf{g}(\mathbf{u}, \mathbf{y}) \leq \mathbf{0} \end{aligned}$$

NLP



Optimization of a Batch Plant

Optimize the dynamic **performance** of a batch process
while satisfying a number of operational **constraints**

Batch unit with uncertainty regarding initial conditions, raw
material quality and model accuracy



Uncertainty → Real-time adaptation of trajectories

Run-to-run Optimization of a Batch Plant

Problem formulation



Batch plant with finite terminal time

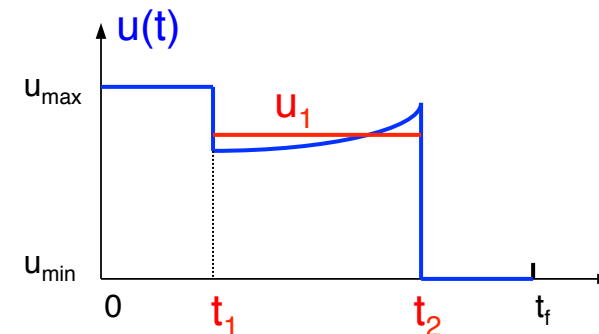
$$\begin{aligned}
 & \min_{\mathbf{u}[0, t_f]} \quad \Phi := \phi(\mathbf{x}(t_f)) \\
 & \text{s. t.} \quad \dot{\mathbf{x}} = \mathbf{F}(\mathbf{x}, \mathbf{u}, \boldsymbol{\theta}) \quad \mathbf{x}(0) = \mathbf{x}_0 \\
 & \quad \quad \mathbf{S}(\mathbf{x}, \mathbf{u}) \leq \mathbf{0} \\
 & \quad \quad \mathbf{T}(\mathbf{x}(t_f)) \leq \mathbf{0}
 \end{aligned}$$

Input Parameterization

$$\mathbf{u}[0, t_f] = \mathbf{U}(\boldsymbol{\pi})$$



Batch plant viewed as a static map



$$\begin{aligned}
 & \min_{\boldsymbol{\pi}} \quad \Phi(\boldsymbol{\pi}, \boldsymbol{\theta}) \\
 & \text{s. t.} \quad \mathbf{G}(\boldsymbol{\pi}, \boldsymbol{\theta}) \leq \mathbf{0}
 \end{aligned}$$

NLP

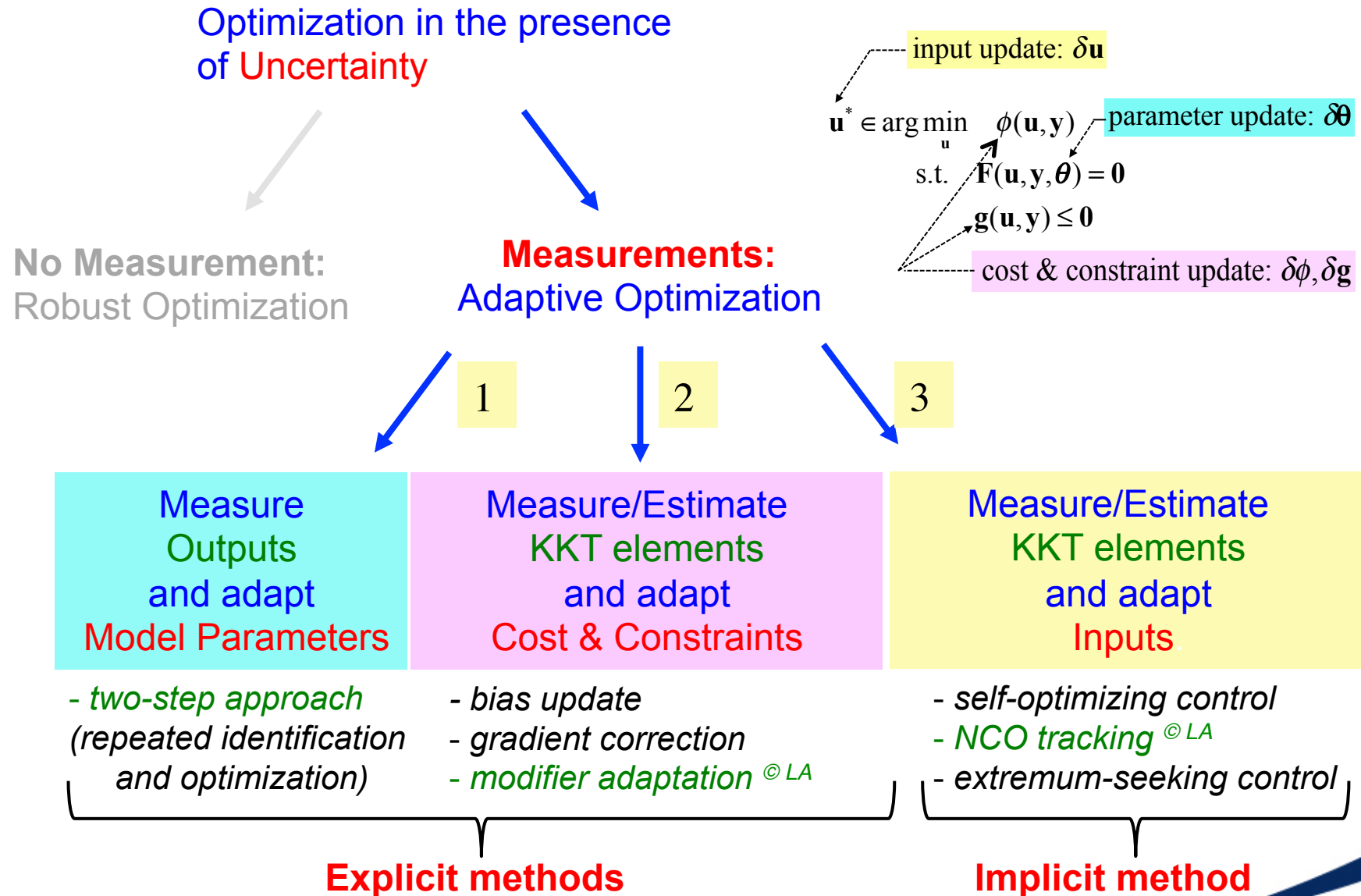
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Three Approaches for Static RTO

What to measure and what to adapt?



1. Adaptation of Model Parameters

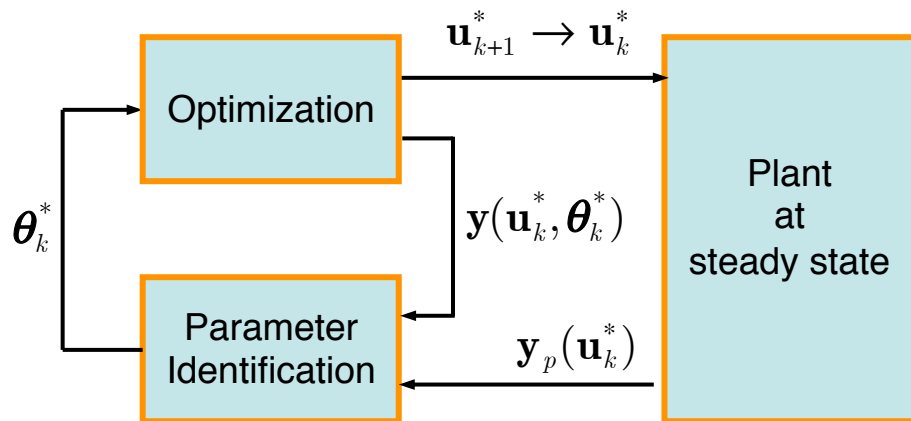
Two-step approach

Parameter Identification Problem

$$\theta_k^* \in \arg \min_{\theta} J_k^{\text{id}}$$
$$J_k^{\text{id}} = \left[\mathbf{y}_p(\mathbf{u}_k^*) - \mathbf{y}(\mathbf{u}_k^*, \theta) \right]^T \mathbf{Q} \left[\mathbf{y}_p(\mathbf{u}_k^*) - \mathbf{y}(\mathbf{u}_k^*, \theta) \right]$$

Optimization Problem

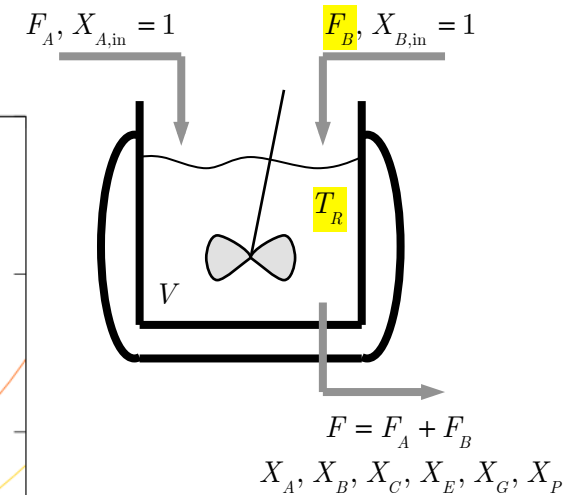
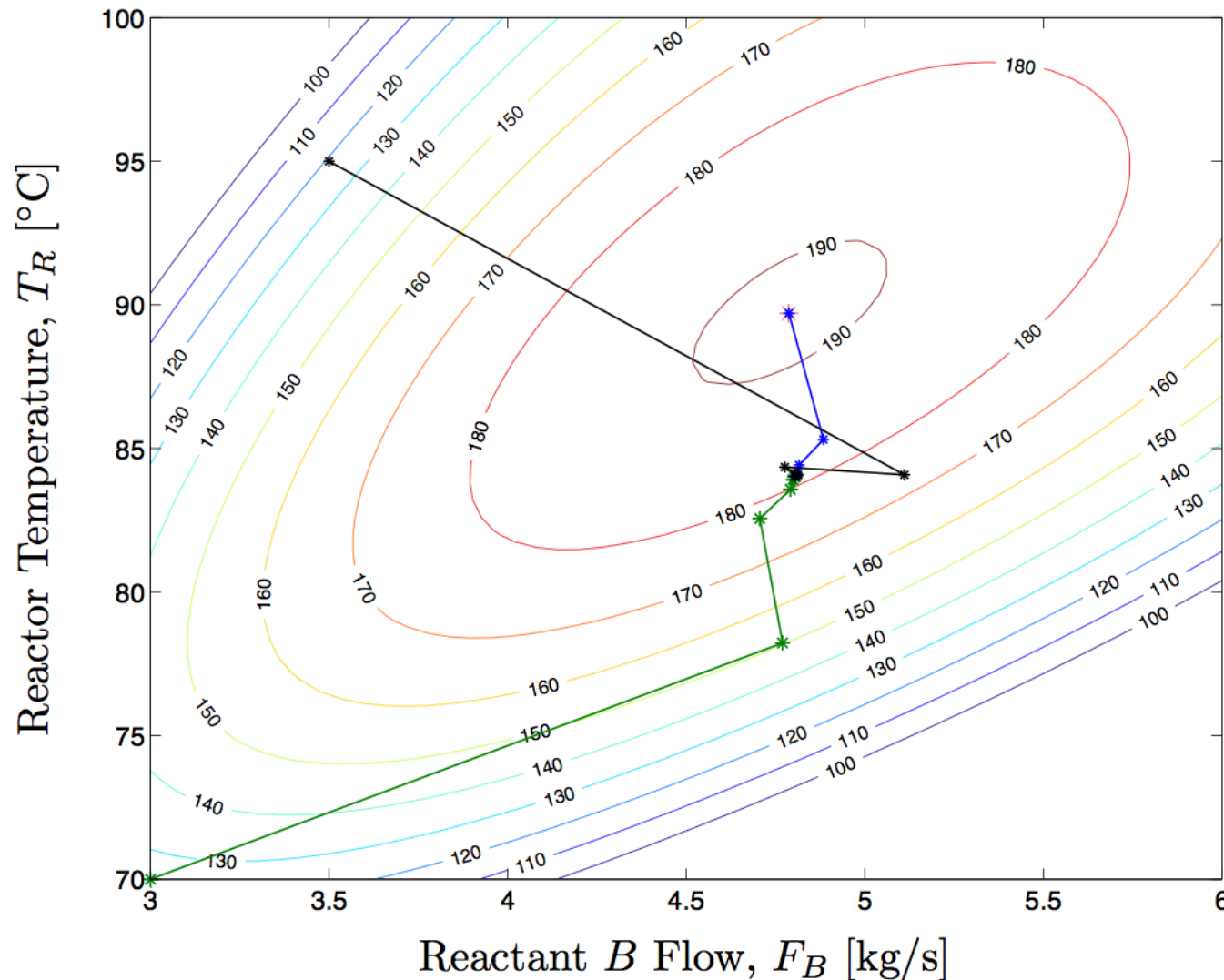
$$\mathbf{u}_{k+1}^* \in \arg \min_{\mathbf{u}} \phi(\mathbf{u}, \mathbf{y}(\mathbf{u}, \theta_k^*))$$
$$\text{s.t.} \quad \mathbf{g}(\mathbf{u}, \mathbf{y}(\mathbf{u}, \theta_k^*)) \leq 0$$
$$\mathbf{u}^L \leq \mathbf{u} \leq \mathbf{u}^U$$



Current Industrial Practice
for tracking the changing optimum
in the presence of disturbances

Two-step Approach

With structurally incorrect model



Williams-Otto Reactor

- 4th-order model
- 2 inputs
- 2 adjustable par.

Does not
converge to plant
optimum

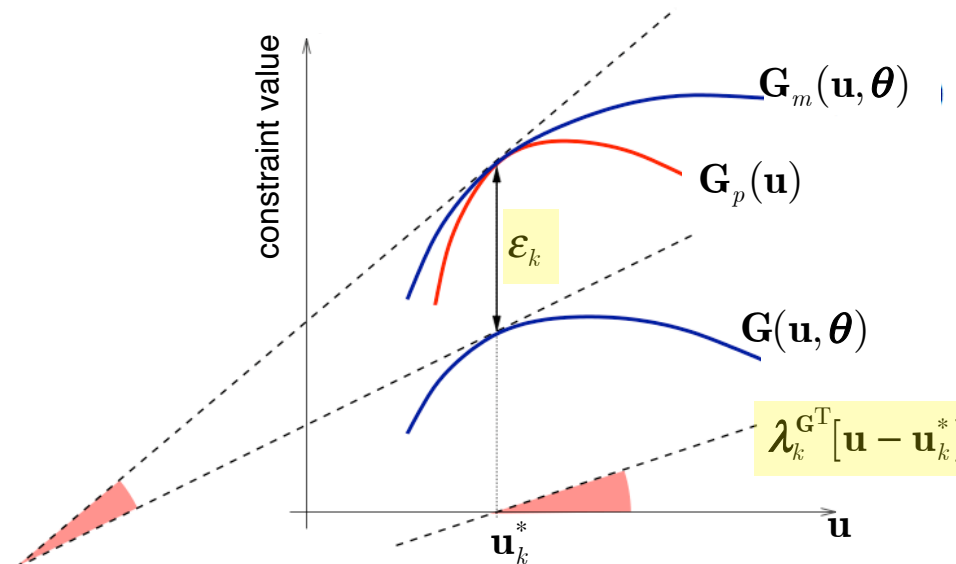
2. Adaptation of Cost & Constraints

Input-affine correction to the model

Modified Optimization Problem

$$\begin{aligned} \mathbf{u}_{k+1}^* \in \arg \min_{\mathbf{u}} \quad & \Phi_m(\mathbf{u}, \boldsymbol{\theta}) := \Phi(\mathbf{u}, \boldsymbol{\theta}) + \lambda_k^{\Phi^T} [\mathbf{u} - \mathbf{u}_k^*] \\ \text{s.t.} \quad & \mathbf{G}_m(\mathbf{u}, \boldsymbol{\theta}) := \mathbf{G}(\mathbf{u}, \boldsymbol{\theta}) + \boldsymbol{\varepsilon}_k + \lambda_k^{G^T} [\mathbf{u} - \mathbf{u}_k^*] \leq 0 \\ & \mathbf{u}^L \leq \mathbf{u} \leq \mathbf{u}^U \end{aligned}$$

Affine corrections of cost and constraint functions. The modified problem satisfies the first-order optimality conditions of the plant

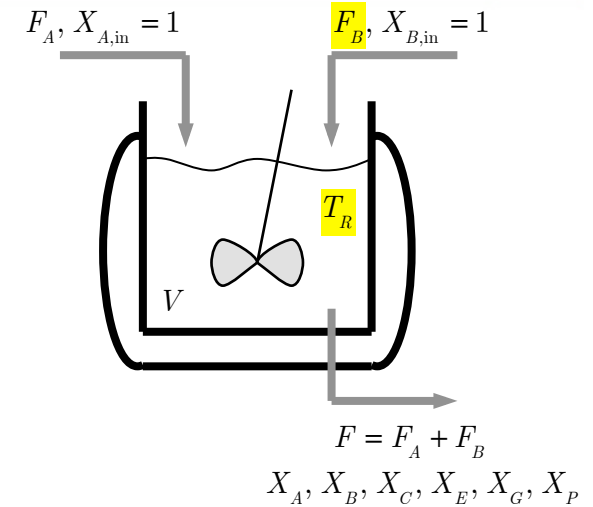
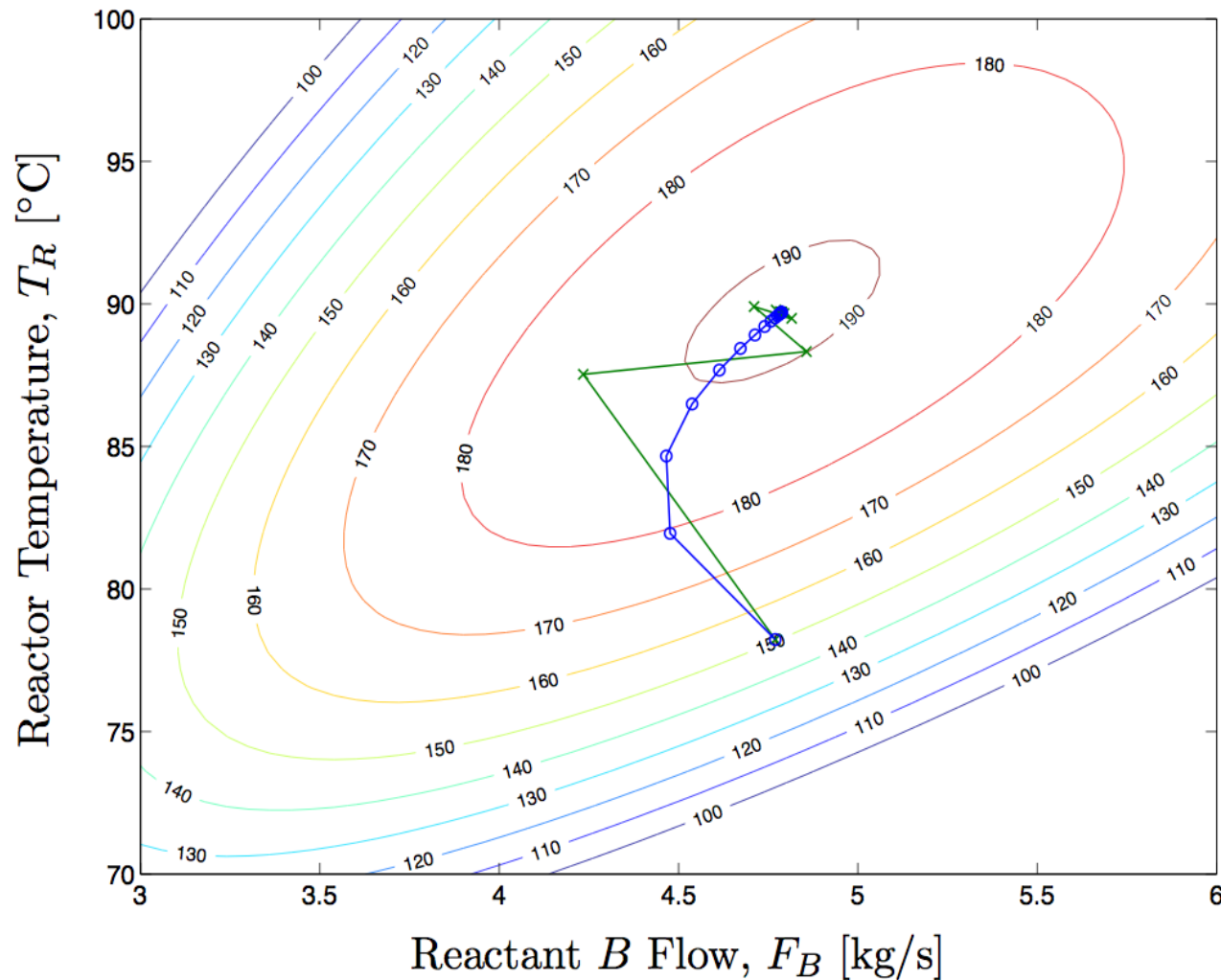


$$\lambda_k^G = \frac{\partial \mathbf{G}_p}{\partial \mathbf{u}}(\mathbf{u}_k^*) - \frac{\partial \mathbf{G}}{\partial \mathbf{u}}(\mathbf{u}_k^*, \boldsymbol{\theta})$$

plant gradients

Example Revisited

Modifier adaptation © LA



Williams-Otto Reactor

- 4th-order model
- 2 inputs
- 2 adjustable par.

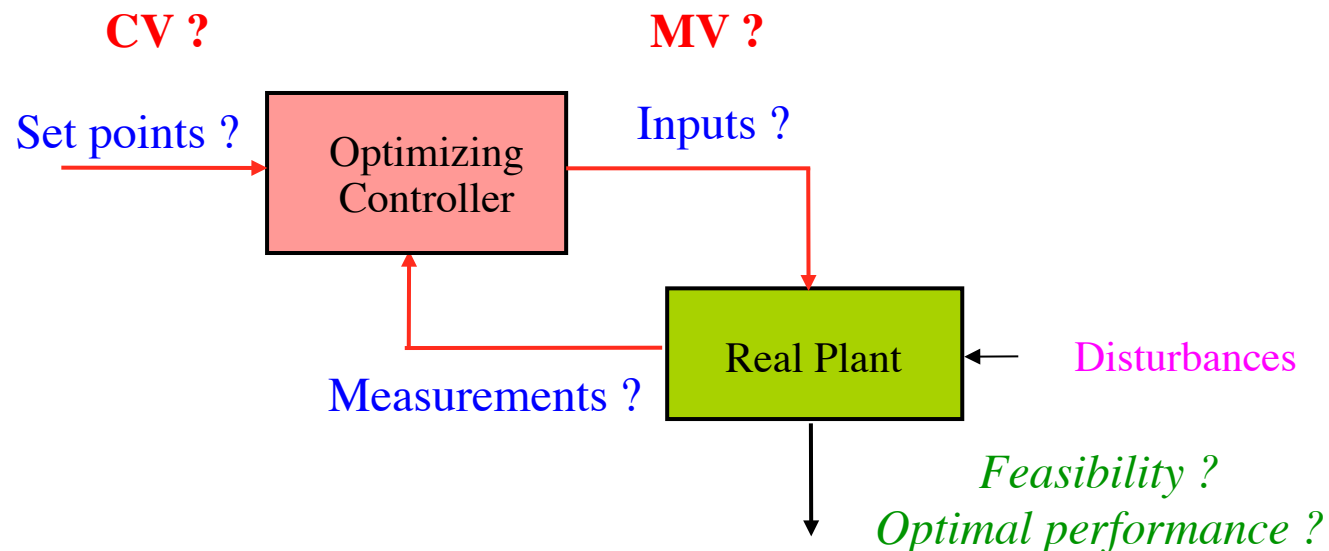
Converges to plant optimum

Requires estimation of experimental gradient

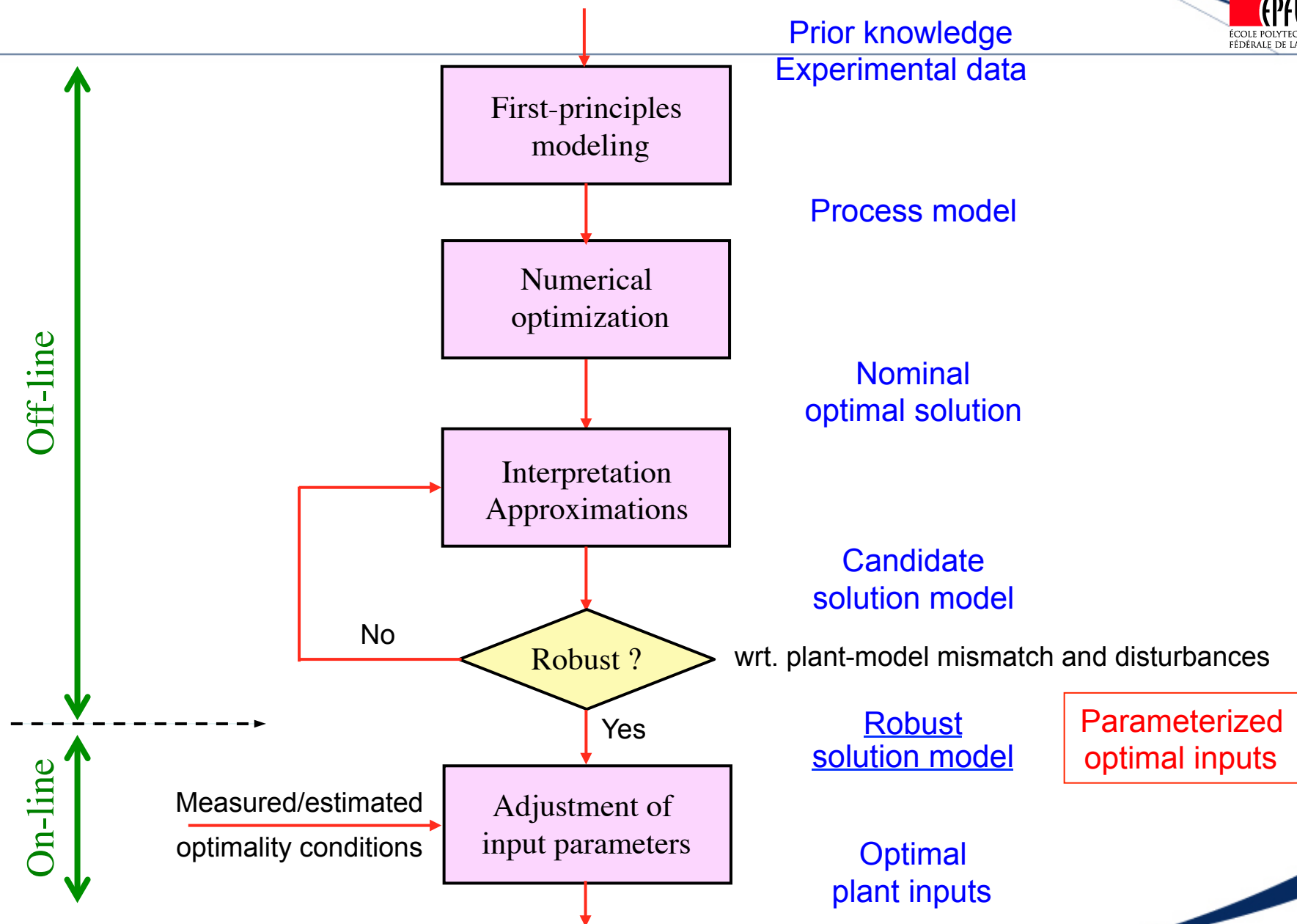
3. Direct Adaptation of Inputs

NCO tracking © LA

- Transform the optimization problem into a control problem
- Which setpoints to track for optimality?
 - The **optimality conditions** (active constraints, gradients)
 - Requires corresponding measurements



Generation of a Solution Model



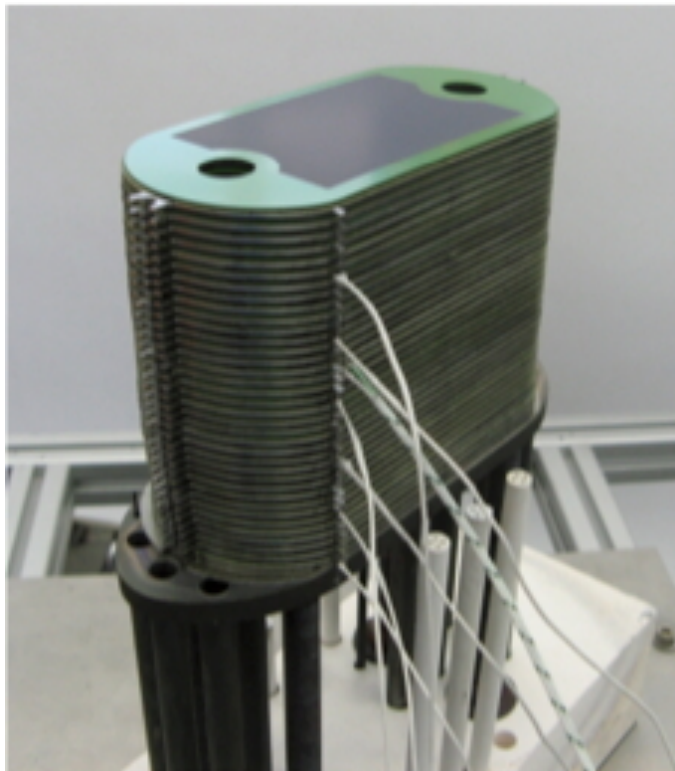
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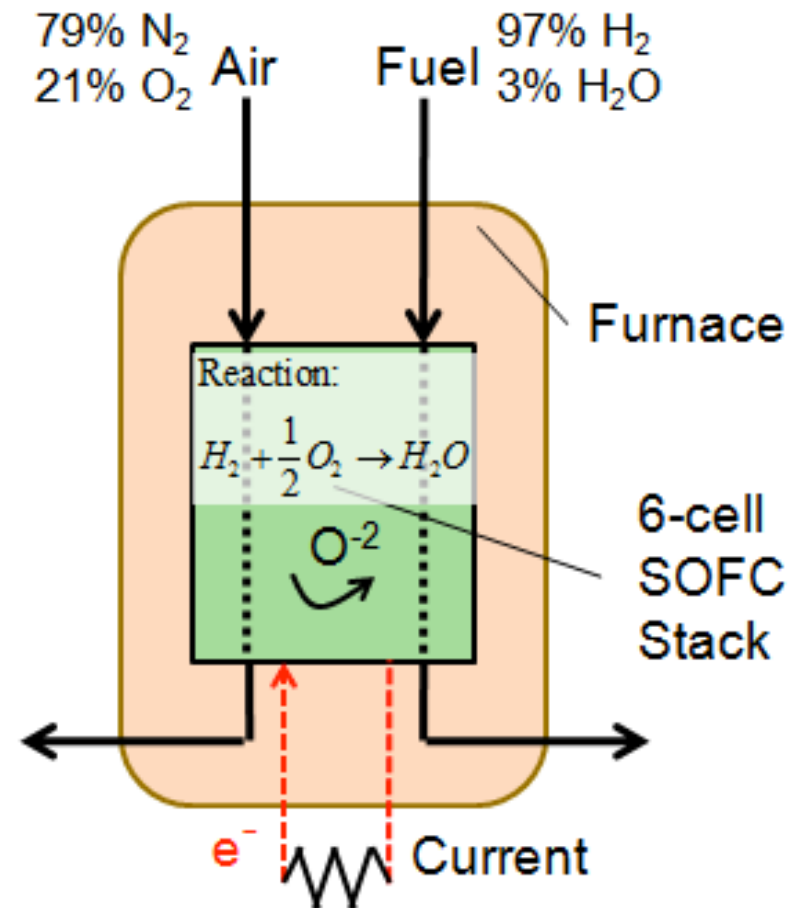


Solid Oxide Fuel Cell Stack

RTO via modifier adaptation © LA



- Stack of 6 cells, active area of 50 cm², metallic interconnector
- Anodes : standard nickel/yttrium stabilized-zirconia (Ni-YSZ)
- Electrolyte : dense YSZ.
- Cathodes: screen-printed (La, Sr)(Co, Fe)O₃
- Operation temperatures between 650 and 850°C.



Experimental Features

- **Objective:** maximize electrical efficiency
- Meet power demand that changes unexpectedly
- **Inputs:** flowrates of H_2 and O_2 , current
- **Outputs:** power density, cell potential
- Time-scale separation
 - *slow temperature dynamics, treated as process drift !*
 - *static model (for the rest)*
- Inaccurate model in the operating region (power, cell)

Strategy for Online Optimization

Repeated Numerical Optimization

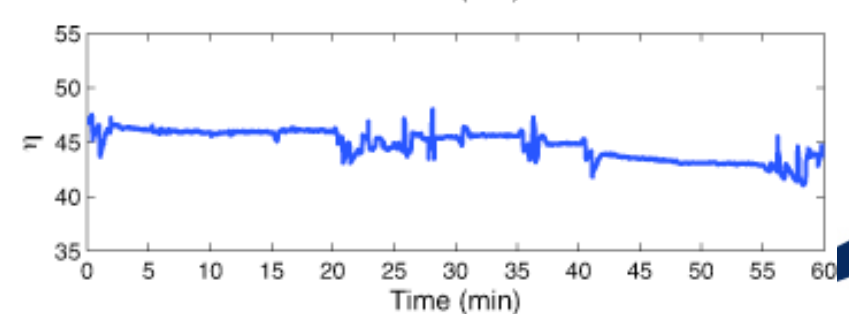
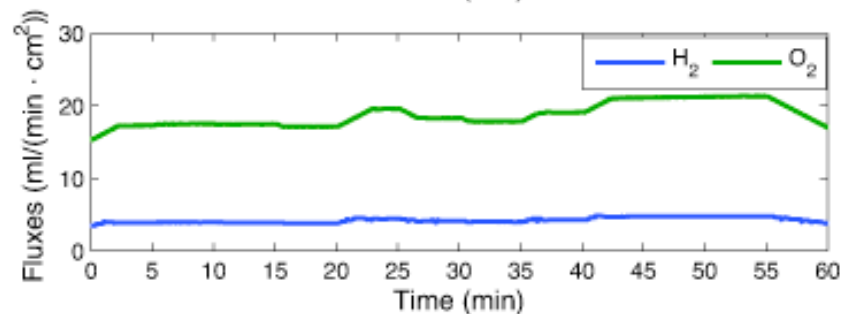
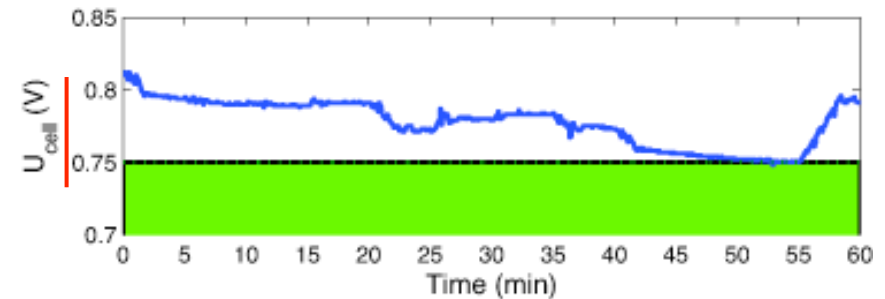
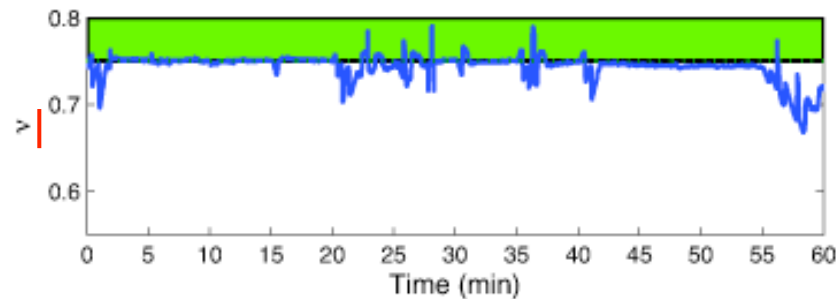
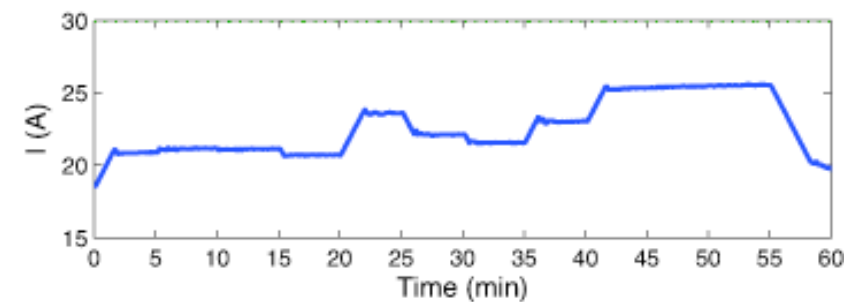
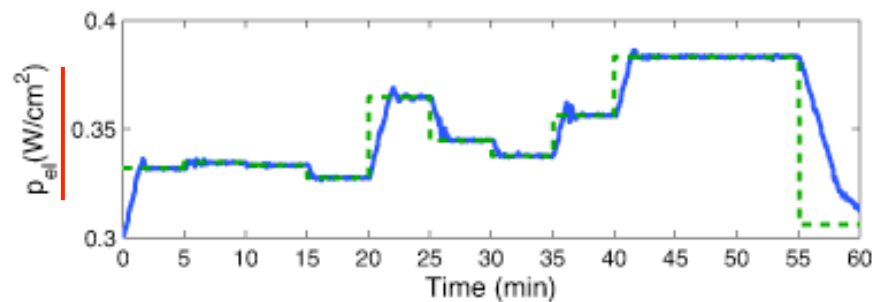
- Solve a static optimization problem every 10 sec
- Apply the optimal inputs to the fuel cell stack
- Measure the resulting constraint values
- Adapt the modifiers ε to match the active constraints

$$\begin{aligned}
 \max_{\mathbf{u}_k} \quad & \eta(\mathbf{u}_k, \boldsymbol{\theta}) \\
 \text{s.t.} \quad & p_{\text{el}}(\mathbf{u}_k, \boldsymbol{\theta}) + \varepsilon_{k-1}^{p_{\text{el}}} = \underline{p_{\text{el}}^s} \\
 & U_{\text{cell}}(\mathbf{u}_k, \boldsymbol{\theta}) + \varepsilon_{k-1}^{U_{\text{cell}}} \geq \underline{0.75 \text{ V}} \\
 & \nu(\mathbf{u}_k) \leq \underline{0.75} \\
 & 4 \leq \lambda_{\text{air}}(\mathbf{u}_k) \leq 7 \\
 & \mathbf{u}_{1,k} \geq 3.14 \text{ mL}/(\text{min cm}^2) \\
 & \mathbf{u}_{3,k} \leq 30 \text{ A}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{u}_k &= \begin{bmatrix} u_{1,k} = \dot{n}_{\text{H}_2,k} \\ u_{2,k} = \dot{n}_{\text{O}_2,k} \\ u_{3,k} = I_k \end{bmatrix} \\
 \varepsilon_k^{p_{\text{el}}} &= (1 - K_{p_{\text{el}}}) \varepsilon_{k-1}^{p_{\text{el}}} + K_{p_{\text{el}}} [p_{\text{el,p,k}} - p_{\text{el}}(\mathbf{u}_k, \boldsymbol{\theta})] \\
 \varepsilon_k^{U_{\text{cell}}} &= (1 - K_{U_{\text{cell}}}) \varepsilon_{k-1}^{U_{\text{cell}}} + K_{U_{\text{cell}}} [U_{\text{cell,p,k}} - U_{\text{cell}}(\mathbf{u}_k, \boldsymbol{\theta})]
 \end{aligned}$$

Experimental Results

- Random power changes every 5 min
- RTO every 10 sec, matches the active constraints at steady state



Optimization of Polymerization Reactor

NCO tracking © LA



■ Industrial features

- 1-ton reactor, risk of runaway
- Initiator efficiency can vary considerably
- Several recipes
 - *different initial conditions*
 - *different initiator feeding policies*
 - *use of chain transfer agent*
 - *use of reticulant*

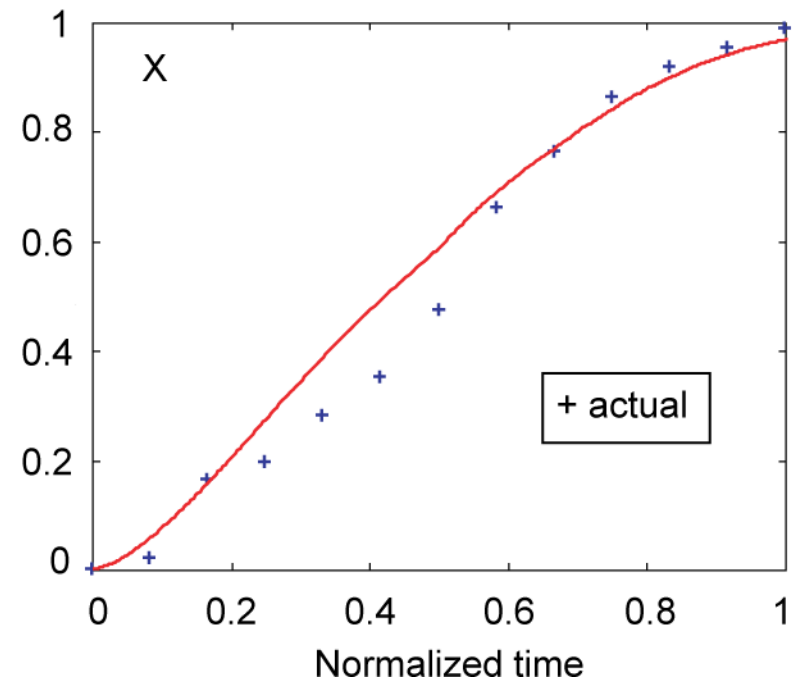
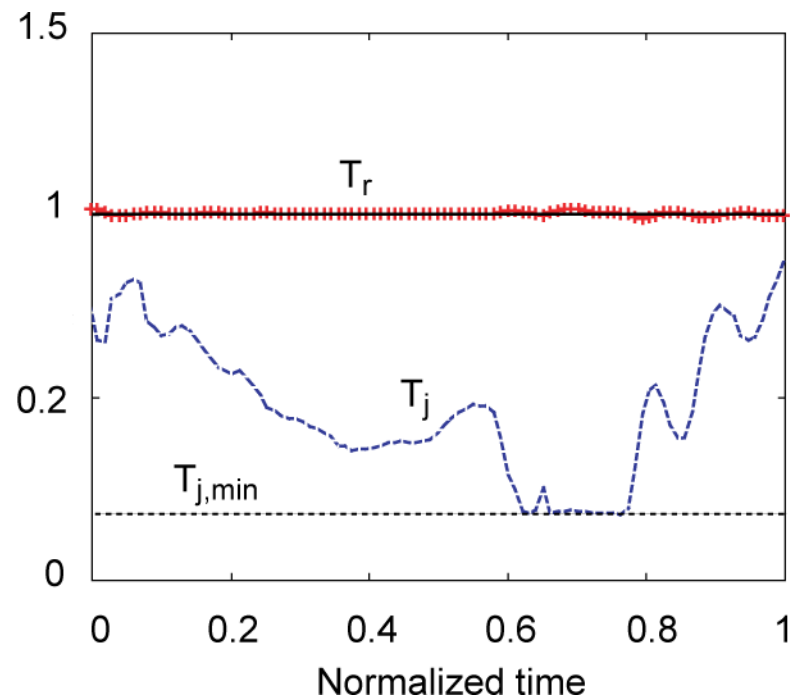


- Modeling difficulties
- Uncertainty

■ Challenge: Implement (near) optimal operation for various recipes

G. François *et al.*, Run-to-Run Adaptation of a Semi-Adiabatic Policy for the Optimization of an Industrial Batch Polymerization Process, *I&EC Research*, 43, 7238-7242 (2004)

Industrial Practice



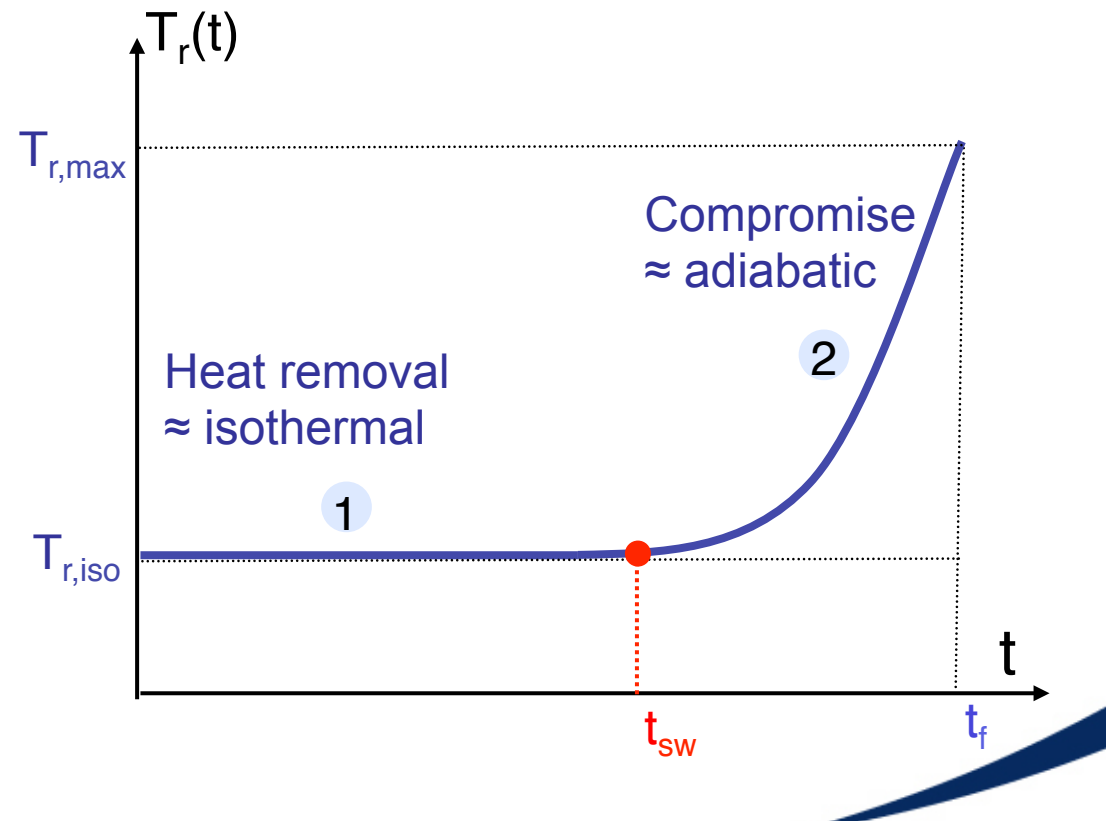
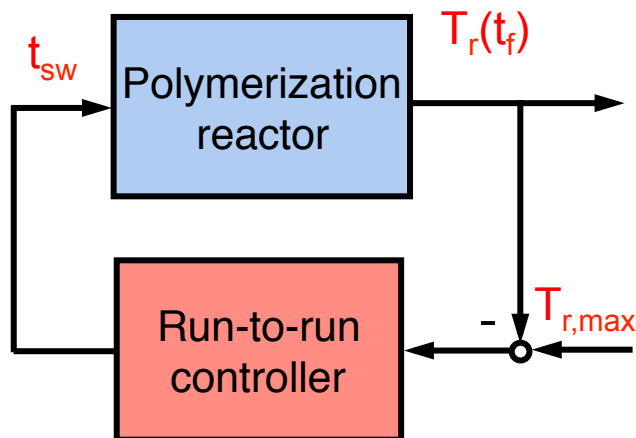
$T_r(t)$ to minimize the batch time ?

Strategy for Run-to-run Optimization

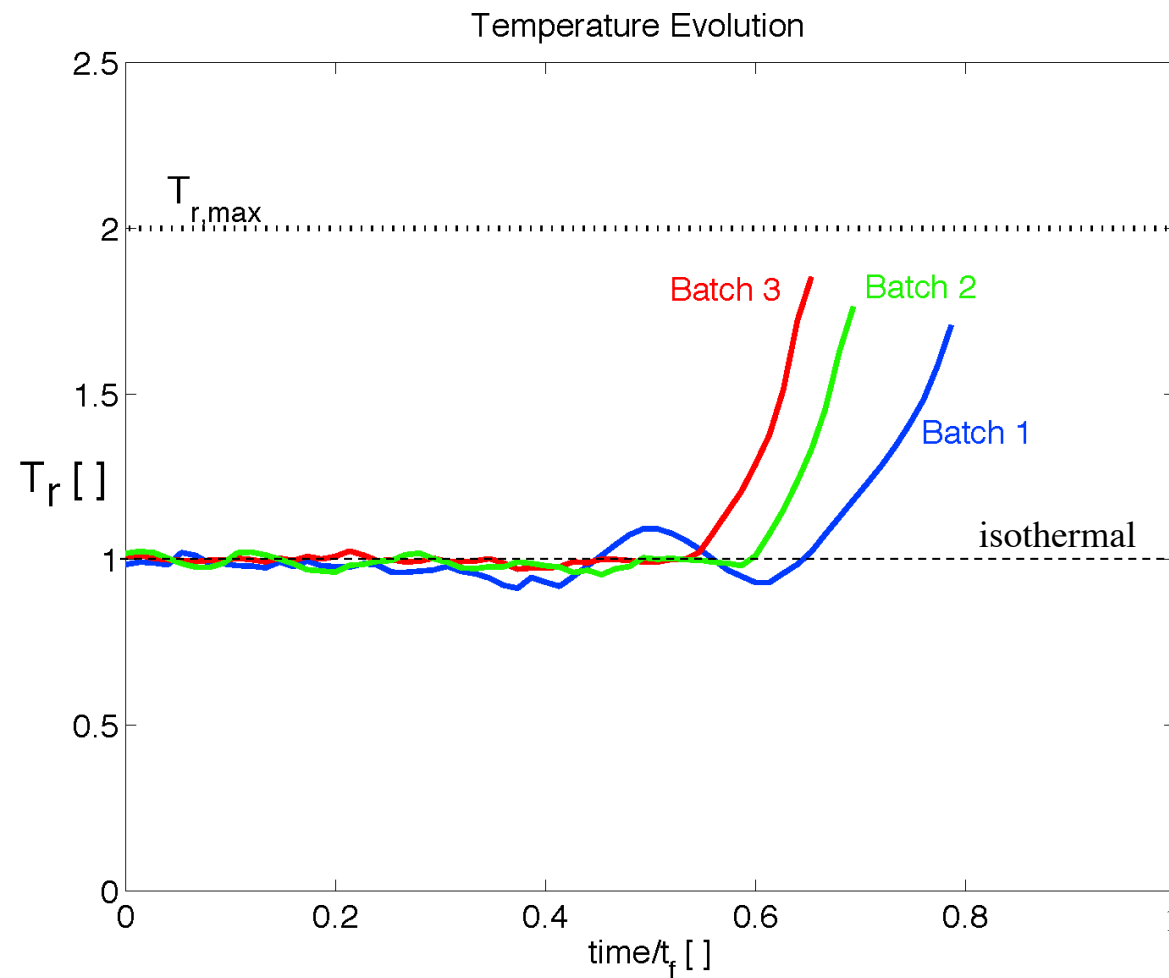
Tendency model

Optimality is linked with meeting the most restrictive constraint $T_r(t_f) = T_{r,max}$

Strategy: Manipulate t_{sw} on a run-to-run basis to force $T_r(t_f)$ at $T_{r,max}$



Industrial Results



Final time

- Isothermal: 1.00
- Batch 1: 0.78
- Batch 2: 0.72
- Batch 3: 0.65

Conclusions

- Process models are often inadequate for optimization
 - use **real-time measurements** for appropriate adaptation
- Which measurements to use? How to best exploit them?
 - **Outputs**: easily available, not necessarily appropriate
 - **KKT modifiers** allow meeting KKT conditions
 - modifier adaptation (explicit optimization)
 - NCO tracking (implicit optimization)
- Key challenge is **estimation of plant gradient**