

Supplementary Materials for

Closed-loop neuromodulation of spinal sensorimotor circuits controls refined locomotion after complete spinal cord injury

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Other Supplementary Material for this manuscript includes the following:

(available at

www.sciencetranslationalmedicine.org/cgi/content/full/6/255/255ra133/DC1)

Movie S1 (.avi format). Real-time monitoring and control platform.

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SUPPLEMENTARY METHODS

Surgical procedure and post-surgical care

Surgical interventions were performed under general anesthesia and aseptic conditions. All 8 animals examined in this study exhibited a complete transection of the mid-thoracic spinal cord (~ spinal segment T7). The completeness of the spinal cord transections was verified during surgery by two independent surgeons by lifting the cut ends of the cord (14). Gel foam was inserted into the gap created by the transection as a coagulant and to separate the cut ends of the spinal cord. The transections led to permanent and complete paralysis of the hindlimbs in all the tested rats ($n=8$) (Fig. 1C). The spinal cord tissue was kept postmortem for histological evaluations in order to verify lesion completeness (fig. S1). The tissue was stained against glial fibrillary acidic protein (GFAP) and no remaining neural tissue was observed at the site of the lesion.

Stimulating electrodes were created by removing a small part (1 mm notch) of insulation from Teflon-coated stainless steel wires (AS632, Cooner Wire). These were subsequently secured during surgery at the midline overlying spinal level L2 and S1 by suturing the wires to the dura. A common ground wire (1 cm of Teflon removed at the distal end) was inserted subcutaneously over the right shoulder. Bipolar intramuscular EMG electrodes (AS632; Cooner Wire) were implanted using the same wire type, into the tibialis anterior and medial gastrocnemius muscles, bilaterally. All electrode wires were connected to a percutaneous amphenol connector (Omnetics Connector Corporation) cemented to the skull of the rat. The rats then received a complete transection of the spinal cord (~T7). The proper location of the epidural and EMG electrodes was verified post-mortem, along with the extent and location of the lesion.

Kinematic, ground reaction force, and electromyographic recordings

Bilateral hindlimb kinematics were recorded using 12 infrared motion capture cameras (200 Hz; Vicon). Reflective markers were attached bilaterally overlying iliac crest, greater trochanter (hip), lateral condyle (knee), lateral malleolus (ankle) and the distal end of the fifth metatarsal (limb endpoint) (Fig. 1A). Nexus (Vicon) was used to obtain 3D coordinates of the markers. The body was modeled as an interconnected chain of rigid segments, and joint angles were generated accordingly. EMG signals (12.207 kHz) were amplified, filtered (10–5,000-Hz bandpass) and recorded synchronized to kinematic and ground reaction force data. Vertical ground reaction forces were measured using a biomechanical force plate (2 kHz; HE6X6, AMTI) located below the treadmill belt, or along the runway. Video recordings (200

Hz) were obtained using two cameras (Basler Vision Technologies) oriented at 90° and 270° with respect to the direction of locomotion.

A minimum of 10 step cycles was extracted for each experimental condition and rat. A total of 147 parameters quantifying gait, kinematics, ground reaction force, and EMG features were computed for each limb and gait cycle according to methods described in detail previously (14, 39, 42, 43). These parameters provide a comprehensive quantification of gait patterns ranging from general features of locomotion to fine details of limb motion. The entire list of 147 computed parameters is described in table S1.

Reflex analysis

EES-evoked motor potentials were recorded in TA and MG muscles. Each pulse of stimulation elicits a medium-latency and late-latency response, which were determined based on their respective latency (17), as illustrated in Fig. 4A. The peak amplitude of each response was measured through custom-made software in Matlab. Spectral analysis of EMG activity by fast Fourier transformation (FFT) was performed on the identified bursts of EMG activity recorded from the TA and MG muscles. Spectral peaks in frequency ranges from 0 to 160 Hz were calculated. Burst amplitude was calculated as the mean of the rectified EMG signal during stance and swing phase for MG and TA muscle, respectively. The area under the curve of the rectified EMG signal was calculated separately for the monosynaptic and polysynaptic responses. Both responses were aligned separately along the normalized gait cycle and their response activity calculated using a moving average with a 150 ms window size. Results are reported in percentage of the maximum value across all tested frequencies.

Principal component analysis

The various experimental conditions led to substantial modulation of gait patterns, which were evident in the modifications of a large proportion of the computed parameters. In order to extract the modulated gait characteristics in response to changes in stimulation features, we implemented a multi-step statistical procedure based on principal component (PC) analysis (14, 42). PC analyses were applied on data from all individual gait cycles for all the rats together. Data were analyzed using the correlation method, which adjusts the mean of the data to zero and the standard deviation to 1. This is a conservative procedure that is appropriate for variables that differ in their variance (e.g. kinematic vs. EMG data).

SUPPLEMENTARY FIGURES

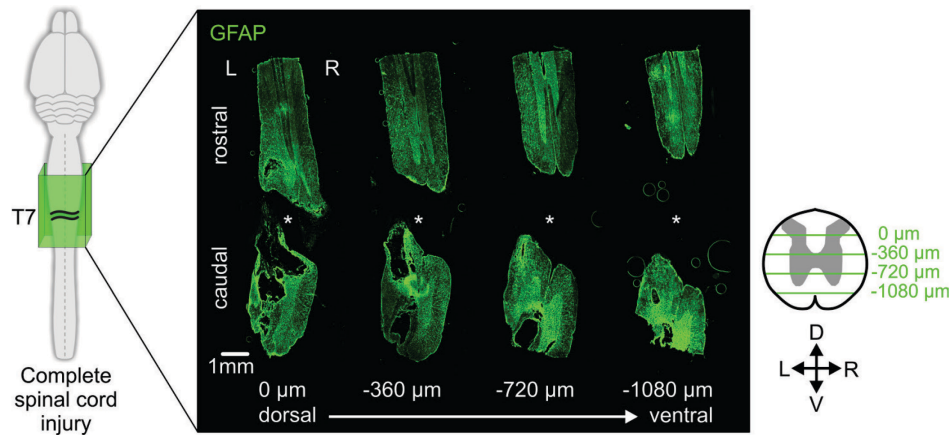


Fig. S1. Completeness of the SCI. Rats received a complete transection of the spinal cord around mid-thoracic segment T7. The completeness and location of the lesion was verified macroscopically during surgery by two independent surgeons, and post-mortem through histological evaluations. The photographs show a series of histological sections stained against glial fibrillary acidic protein (GFAP) in a representative rat. The site of lesion is marked with an asterisk (*). Images were obtained on coronal sections taken at regular intervals (360 μm) from the dorsal to ventral aspects of the spinal cord. Histological slice thickness, 30 μm . L, left; R right; D, dorsal; V, ventral.

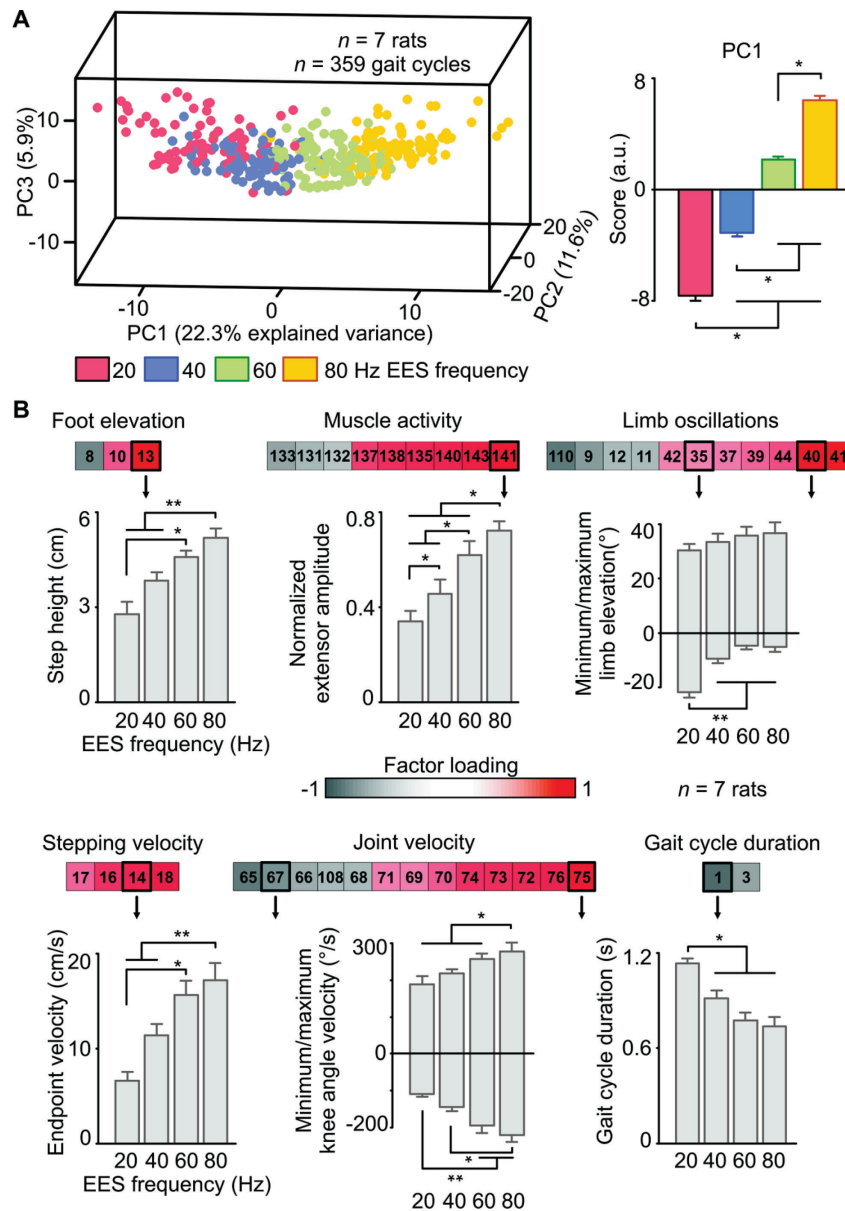


Fig. S2: Modulation of EES frequency tunes multiple aspects of gait patterns. (A) PC analysis applied on all 147 computed parameters (table S1) from all the gait cycles recorded in 7 rats for EES frequencies set at 20, 40, 60, and 80 Hz. Each data point is a gait cycle represented in the 3D space defined by PC1 to PC3. (B) Histogram plots reporting the mean values of scores on PC1 for the various EES frequencies. The variables with high factor loadings on PC1 ($|value| > 0.5$) were grouped into functional clusters. Numbers refer to the computed variables in table S1. The histogram plots report, for each functional cluster, the mean values of a representative variable at the different EES frequencies. The arrows refer to the variable illustrated in the histogram plots. Data are means \pm SEM. * $P < 0.05$, ** $P < 0.01$, Repeated measure ANOVA followed by Newman-Keuls post-hoc tests.

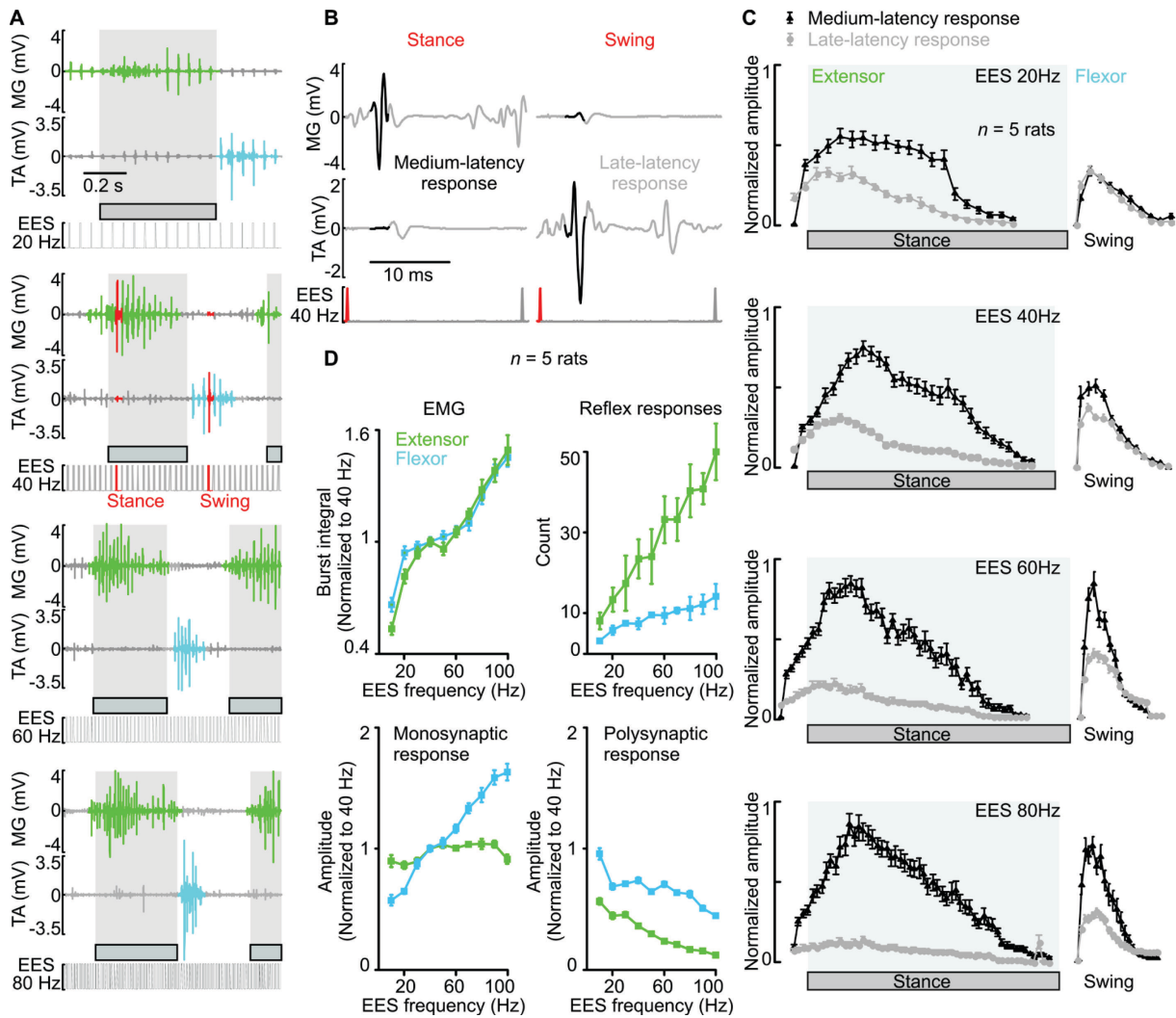


Fig. S3: Modulation of EES frequency tunes mono- and polysynaptic responses in flexor and extensor muscle during locomotion. (A) EMG activity recorded in extensor (MG) and flexor (TA) muscles during a representative gait cycle under EES frequencies set at 20, 40, 60, and 80 Hz. The bursts of EMG activity extracted for further analysis are represented in green and blue for extensor and flexor muscles, respectively. (B) Color-coded medium-latency and late-latency reflex responses elicited in extensor and flexor muscles in response to a pulse of EES during stance and swing. Responses are identified based on their respective latencies. The example is extracted from panel (A) during EES at 40 Hz. (C) Mean amplitude (\pm SEM) of each EES-induced monosynaptic (black) and polysynaptic (grey) response over the course of the stance phase for extensor muscles and swing for flexor muscles. EMG bursts were built from a succession of modulated monosynaptic and polysynaptic responses. Ten EMG bursts were analyzed per muscle, condition, and rat ($n = 5$). The amplitude of responses was normalized to the maximum amplitude recorded for each rat over all the experimental conditions. (D) Mean values (\pm SEM) of EMG burst integrals, of the total number of induced motor responses per burst, and of the averaged amplitude of monosynaptic and polysynaptic responses over the entire bursts in extensor and flexor muscles for the different EES frequencies. Data are for $n = 5$ rats.

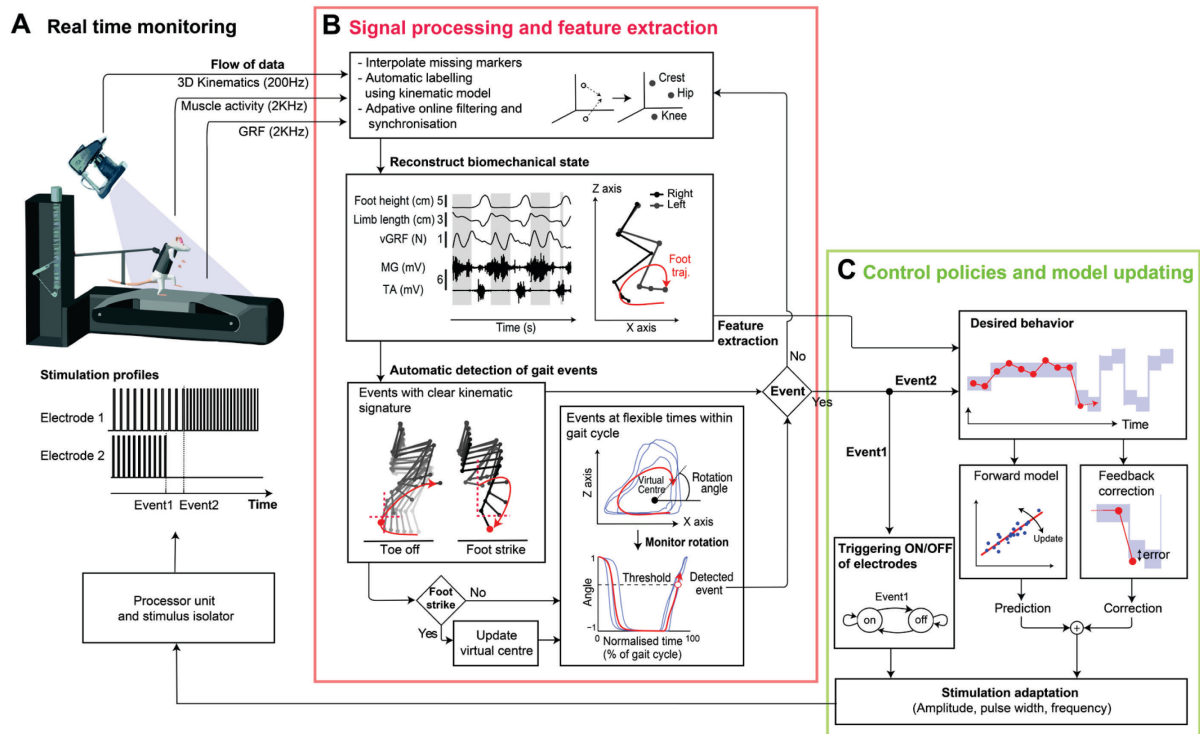


Fig. S4: Real-time monitoring and control platform. (A) The flow of kinematics, EMG, and kinetic information was continuously monitored in real-time through the integrated system Vicon. (B) All the signals were filtered online using adaptive filters (least mean squares). To deal with missing kinematic information owing to occlusion of markers, the coordinates of each marker were interpolated by triangulation. The different sources of information were synchronized to reconstruct the complete biomechanical state of the locomotor system. The signal-processing system then combined two complementary algorithms to automatically detect key gait events and extract meaningful features integrated into control policies. First, gait events with clear-cut kinematic signatures (foot strike and toe off,) were detected online based on a threshold of foot elevation in the sagittal plane. Second, custom-made algorithms monitored the circular trajectory of the foot around a virtual center updated after each cycle. The rotation angle of the foot trajectory along this circular path allowed to trigger stimulation or updated features of stimulation at any time of the gait cycle. (C) Both sets of events triggered controller calculations, which derived the appropriate corrections of EES parameters. The combination of feedback and feed-forward information generated corrections of EES frequency in order to achieve a desired locomotor output. Forward models were automatically updated after each gait cycle to account for putative time-varying characteristics of the system. Each electrode may also be turned on and off at specific times within the gait cycle to reinforce specific aspects of locomotion.

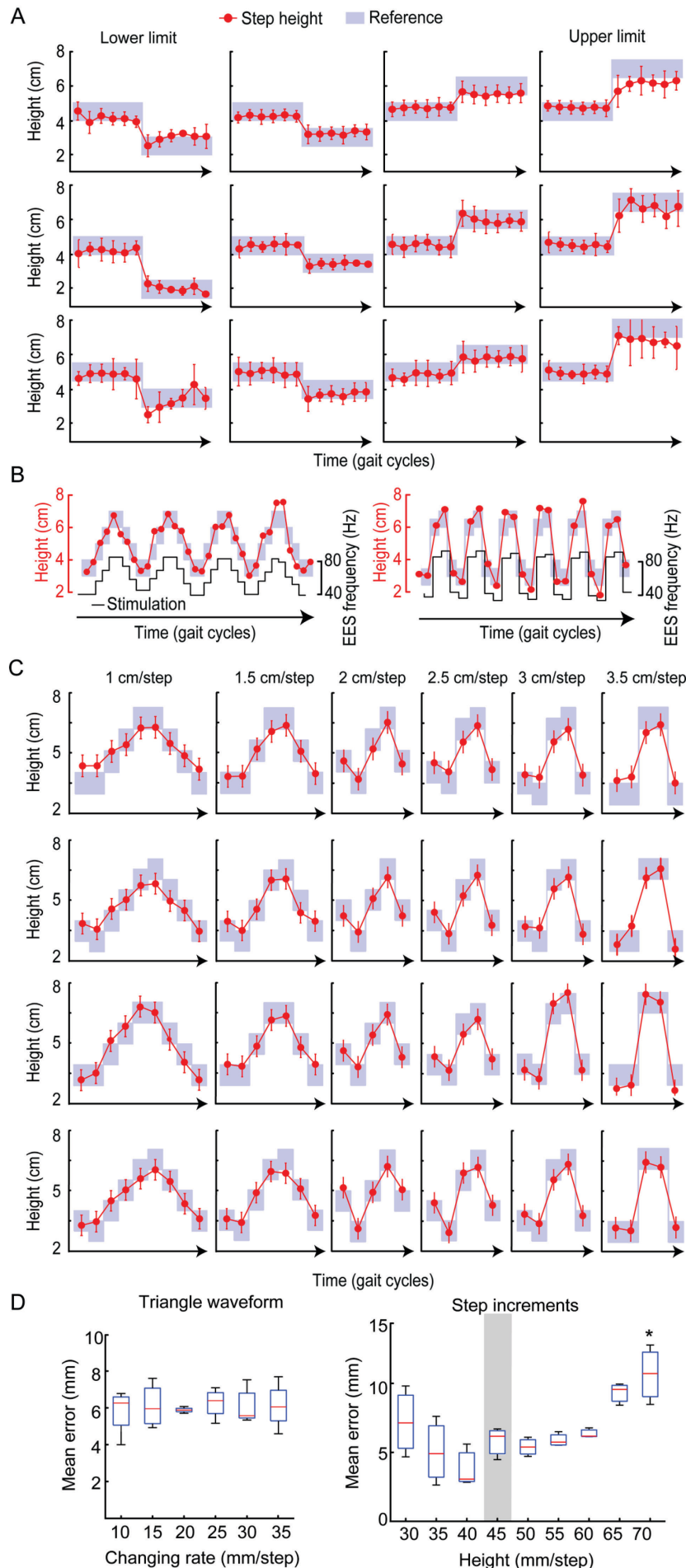


Fig. S5: High-fidelity control of complex foot trajectory.

(A) Step-increments. Data are mean step heights (\pm SD) during stepping with constant-shift of the reference band upward or downward with small and large increments/decrements until reaching steady-state (6 consecutive steps). Each horizontal panel corresponds to a distinct rat ($n = 3$). (B) Representative trials showing the step height performance during a tracking task of a periodic triangular waveform (piecewise linear increments or decrements at different rates) during stepping on a treadmill. (C) Triangle waveforms. Mean values of step heights (\pm SD) during the same type of executions shown in (B), but for the entire range of tested increment/decrement values, from left to right. Each horizontal panel corresponds to a distinct rat ($n = 4$ rats shown). (D) Boxplots reporting the median value, SD, and 95% confidence intervals for step height errors for each experimental condition. $*P < 0.05$ for the marked condition versus all the other conditions (Kruskal-Wallis test).

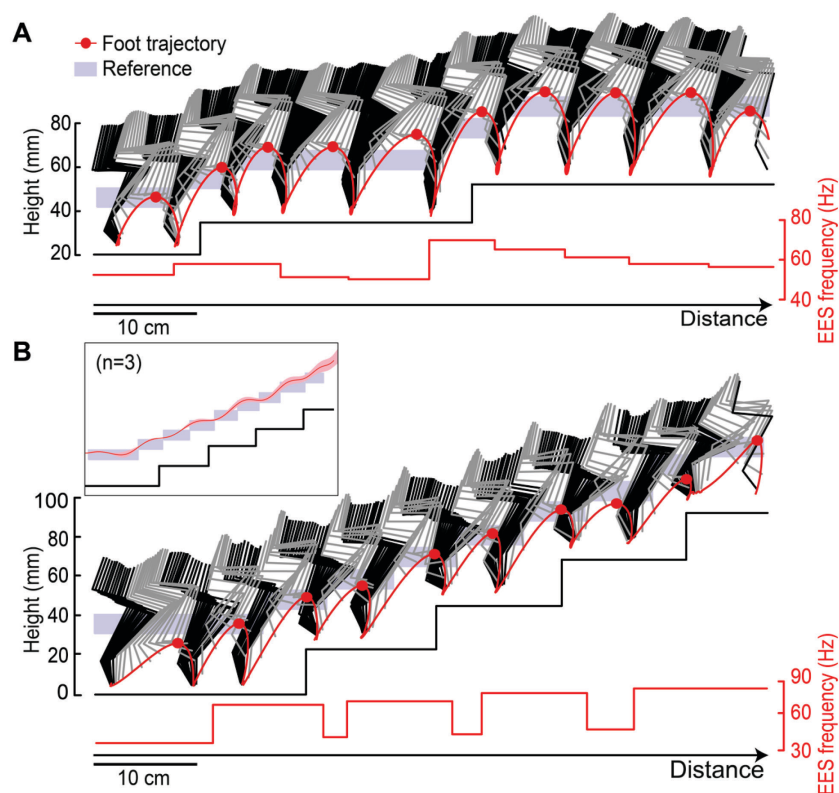


Fig. S6: Execution along staircases of various heights and lengths. (A) Representative stick diagram decomposition of hindlimb movement and limb endpoint trajectory during stance (black) and swing (grey) while walking along a succession of two staircases (1.7-cm height, 25-cm length) under controlled condition. The red dots indicate the maximum elevation of the foot during swing, defined as step height. The positions of the reference band and changes in EES frequency are represented by the shaded area and red signal, respectively. **(B)** Same representation as in (A) for an execution along a succession of 4 staircases (2-cm height, 12-cm length). The inset displays the mean foot trajectories (\pm SD) averaged over 20 successive repetitions for 3 rats.

SUPPLEMENTARY TABLE

Table S1: List of computed kinematic, kinetic, and EMG parameters.

| Parameters | Parameter number | Detailed explanation |
|---|------------------|--|
| Kinematics | | |
| Temporal features | | |
| | 1 | Cycle duration |
| | 2 | Cycle velocity |
| | 3 | Stance duration |
| | 4 | Swing duration |
| | 5 | Relative stance duration (percent of the cycle duration) |
| Limb endpoint (Metatarsal phalange) trajectory | | |
| | 6 | Interlimb temporal coupling |
| | 7 | Duration of double stance phase |
| | 8 | Stride length |
| | 9 | Step length |
| | 10 | 3D limb endpoint path length |
| | 11 | Maximum backward position |
| | 12 | Minimum forward position |
| | 13 | Step height |
| | 14 | Maximum speed during swing |
| | 15 | Relative timing of maximum velocity during swing |
| | 16 | Acceleration at swing onset |
| | 17 | Average endpoint velocity |
| | 18 | Orientation of the velocity vector at swing onset |
| | 19 | Dragging |
| | 20 | Relative dragging duration (percent of swing duration) |
| Stability | | |
| <i>Base of support</i> | 21 | Positioning of the foot at stance onset with respect to the pelvis |
| | 22 | Stance width |
| Trunk and pelvic position and oscillations | 23 | Maximum hip sagittal position |
| | 24 | Minimum hip sagittal position |
| | 25 | Amplitude of sagittal hip oscillations |
| | 26 | Variability of sagittal crest position |
| | 27 | Variability of sagittal crest velocity |
| | 28 | Variability of vertical hip movement |
| | 29 | Variability of sagittal hip movement |
| | 30 | Variability of the 3D hip oscillations |
| | 31 | Length of pelvis displacements in the forward direction |
| | 32 | Length of pelvis displacements in the medio-lateral direction |
| | 33 | Length of pelvis displacements in the vertical direction |
| | 34 | Length of pelvis displacements in all directions |
| Joint angles and segmental oscillations | | |
| <i>Backward</i> | 35 | Crest oscillations |
| | 36 | Thigh oscillations |
| | 37 | Leg oscillations |
| | 38 | Foot oscillations |
| | 39 | Whole limb oscillations |
| <i>Forward</i> | 40 | Crest oscillations |
| | 41 | Thigh oscillations |
| | 42 | Leg oscillations |
| | 43 | Foot oscillations |
| | 44 | Whole limb oscillations |
| <i>Flexion</i> | 45 | Hip joint angle |
| | 46 | Knee joint angle |
| | 47 | Ankle joint angle |
| <i>Abduction</i> | 48 | Whole limb abduction |
| | 49 | Foot abduction |
| <i>Extension</i> | 50 | Hip joint angle |

| | | |
|---|----|---|
| | 51 | Knee joint angle |
| | 52 | Ankle joint angle |
| <i>Adduction</i> | 53 | Whole limb adduction |
| | 54 | Foot adduction |
| <i>Amplitude</i> | 55 | Crest oscillations |
| | 56 | Thigh oscillations |
| | 57 | Leg oscillations |
| | 58 | Foot oscillations |
| | 59 | Whole limb oscillations |
| | 60 | Hip joint angle |
| | 61 | Knee joint angle |
| | 62 | Ankle joint angle |
| | 63 | Whole limb medio-lateral oscillations |
| | 64 | Foot abduction/adduction |
| Velocity | | |
| <i>Minimum</i> | 65 | Whole limb oscillation velocity |
| | 66 | Hip joint angle velocity |
| | 67 | Knee joint angle velocity |
| | 68 | Ankle joint angle velocity |
| <i>Maximum</i> | 69 | Whole limb oscillation velocity |
| | 70 | Hip joint angle velocity |
| | 71 | Knee joint angle velocity |
| | 72 | Ankle joint angle velocity |
| <i>Amplitude</i> | 73 | Whole limb angle velocity |
| | 74 | Hip joint angle velocity |
| | 75 | Knee joint angle velocity |
| | 76 | Ankle joint angle velocity |
| Inter-limb coordination | | |
| <i>PC analysis</i> | 77 | Degree of linear coupling between joint oscillations |
| <i>FFT</i> | 78 | Temporal coupling between crest and thigh oscillations |
| <i>decomposition</i> | 79 | Temporal coupling between thigh and leg oscillations |
| | 80 | Temporal coupling between leg and foot oscillations |
| | 81 | Correlation between crest and thigh oscillations |
| | 82 | Correlation between thigh and leg oscillations |
| | 83 | Correlation between leg and foot oscillations |
| <i>Crosscorrelation</i> | 84 | Correlation between hip and knee oscillations |
| | 85 | Correlation between knee and ankle oscillations |
| | 86 | Correlation between ankle and MTP oscillations |
| | 87 | Temporal lag between backward positions of crest and thigh oscillations |
| | 88 | Temporal lag between forward positions of crest and thigh oscillations |
| <i>Relative coupling</i> | 89 | Temporal lag between backward positions of thigh and leg oscillations |
| | 90 | Temporal lag between forward positions of the thigh and leg oscillations |
| | 91 | Temporal lag between backward positions of leg and foot oscillations |
| | 92 | Temporal lag between forward positions of leg and foot oscillations |
| <i>Inter-segmental coordination compared to</i> | 93 | Lag of the cross correlation function between hindlimb oscillations |
| | 94 | Maximum R-value of the cross correlation function between hindlimb oscillations |
| | 95 | Lag of the cross correlation function between hip oscillations |
| | 96 | Maximum R-value of the cross correlation function between hip oscillations |
| <i>Able-bodied rats</i> | 97 | Lag of the cross correlation function between knee oscillations |
| | 98 | Maximum R-value of the cross correlation function between knee oscillations |

| | | |
|---------------------|-----|---|
| | 99 | Lag of the cross correlation function between ankle oscillations |
| | 100 | Maximum R-value of the cross correlation function between ankle oscillations |
| | 101 | Lag of the cross correlation function between endpoint oscillations |
| | 102 | Maximum R-value of the cross correlation function between endpoint oscillations |
| | 103 | Phase of the first harmonic of the FFT of the hip elevation angle |
| | 104 | Amplitude of the first harmonic of the FFT of the hip elevation angle |
| | 105 | Phase of the first harmonic of the FFT of the knee elevation angle |
| | 106 | Amplitude of the first harmonic of the FFT of the knee elevation angle |
| | 107 | Phase of the first harmonic of the FFT of the ankle elevation angle |
| | 108 | Amplitude of the first harmonic of the FFT of the ankle elevation angle |
| Left-right | 109 | Phase of the first harmonic of the FFT of the endpoint elevation angle |
| hindlimb | 110 | Amplitude of the first harmonic of the FFT of the endpoint elevation angle |
| coordination | 111 | Phase of the first harmonic of the FFT of the hindlimb elevation angle |
| | 112 | Amplitude of the first harmonic of the FFT of the hindlimb elevation angle |
| | 113 | Lag of the cross correlation function between crest and thigh limb elevation angles |
| Hindlimb | 114 | Lag of the cross correlation function between thigh and hindlimb elevation angles |
| coordination | 115 | Lag of the cross correlation function between hip and thigh elevation angles |
| | 116 | Lag of the cross correlation function between hindlimb and foot elevation angles |
| | 117 | Lag of the cross correlation function between thigh and ankle elevation angles |
| | 118 | Lag of the cross correlation function between ankle and foot elevation angles |

Kinetics

| | | |
|--|-----|------------------------|
| | 119 | Medio-lateral forces |
| | 120 | Anteroposterior forces |
| | 121 | Vertical forces |
| | 122 | Weight-bearing level |

EMG

Timing (relative to cycle duration, paw contact to paw contact)

| | | |
|-------------------------------|-----|--|
| <i>Extensor ipsilateral</i> | 123 | Relative onset of ipsilateral MG EMG burst |
| <i>Flexor ipsilateral</i> | 124 | Relative end of ipsilateral MG EMG burst |
| <i>Extensor contralateral</i> | 125 | Relative onset of ipsilateral TA EMG burst |
| <i>Flexor contralateral</i> | 126 | Relative end of ipsilateral TA EMG burst |
| <i>Extensor ipsilateral</i> | 127 | Relative onset of contralateral MG EMG burst |
| <i>Flexor ipsilateral</i> | 128 | Relative end of contralateral MG EMG burst |
| <i>Extensor contralateral</i> | 129 | Relative onset of contralateral TA EMG burst |
| <i>Flexor contralateral</i> | 130 | Relative end of contralateral TA EMG burst |
| Duration | | |
| <i>Extensor ipsilateral</i> | 131 | Duration of ipsilateral MG EMG burst |
| <i>Flexor ipsilateral</i> | 132 | Duration of ipsilateral TA EMG burst |
| <i>Extensor contralateral</i> | 133 | Duration of contralateral MG EMG burst |

| | | |
|---------------------------------|-----|--|
| <i>Flexor contralateral</i> | 134 | Duration of contralateral TA EMG burst |
|---------------------------------|-----|--|

| | | |
|------------------|--|--|
| Amplitude | | |
|------------------|--|--|

| | | |
|-----------------------------------|-----|--|
| <i>Extensor ipsilateral</i> | 135 | Mean amplitude of ipsilateral MG EMG burst |
| | 136 | Integral of ipsilateral MG EMG burst |
| | 137 | Root mean square of ipsilateral MG EMG burst |
| <i>Flexor ipsilateral</i> | 138 | Mean amplitude of ipsilateral TA EMG burst |
| | 139 | Integral of ipsilateral TA EMG burst |
| | 140 | Root mean square of ipsilateral TA EMG burst |
| <i>Extensor contralateral</i> | 141 | Mean amplitude of contralateral MG EMG burst |
| | 142 | Integral of contralateral MG EMG burst |
| | 143 | Root mean square of contralateral MG EMG burst |
| <i>Flexor contralateral</i> | 144 | Mean amplitude of contralateral TA EMG burst |
| | 145 | Integral of contralateral TA EMG burst |
| | 146 | Root mean square of contralateral TA EMG burst |
| Muscle coactivation | 147 | Co-contraction of flexor and extensor muscle |

SUPPLEMENTARY VIDEOS

Movie S1: Real-time monitoring and control platform. The platform to monitor whole-body kinematics, muscle activity, and ground reaction forces in real-time involves an integrated system that interfaces the reconstructed biomechanical state of the rat with control algorithms. Spatial and temporal features of gait are extracted *online* to trigger feedback and feed-forward adjustments of stimulation parameters in order to maintain step height within a desired range. .

Movie S2: Closed-loop neuromodulation achieves high-fidelity control of leg movements. The experimental procedure promoted locomotion in paralyzed rats. We imposed small changes and large changes in step height, as well as maintenance of stable references. The controller successfully tuned stimulation frequency in order to automatically adjust step height.

Movie S3: Closed-loop neuromodulation prevents rapid fatigue during continuous locomotion. We compared the evolution of the stepping patterns and muscle activity during non-controlled and controlled neuromodulation of spinal circuits. After 9 minutes, rats demonstrated a graded decrease in step height because of fatigue, which was corrected under controlled stimulation conditions.

Movie S4: Closed-loop neuromodulation enables locomotion across staircases. Closed-loop neuromodulation allowed the rats to adjust limb kinematic and ground reaction forces in order to restore locomotion across single and combinations of staircases in paralyzed rats. Automated tuning of EES frequency produced adequate foot trajectory to overcome the staircase. By contrast, non-controlled rats were unable to climb the staircase.