Producing synthetic natural gas from microalgae via supercritical water gasification: A techno-economic sensitivity analysis

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A B S T R A C T

A techno-economic sensitivity analysis of the production of synthetic natural gas (SNG) via catalytic supercritical water gasification (SCWG) of microalgae produced in raceway ponds (RP), tubular-, or flat-panel-airlift photobioreactors (FPA-PBR) has been performed. The aim of combining microalgae production with SCWG is to close material flows with respect to water and nutrients, the so-called SunChem process. The sensitivity analysis is based on an annual production of 86,500 t of microalgae biomass yielding 1.14 PJ of methane per year. The sensitivity analysis showed that with an annual algae productivity of 38.5 t per hectare of RP an energy return on energy invested (EROEI) of 1.84 can be achieved for the self-sufficient base case scenario. An SNG production cost of 194 \( \text{V GJ}/\text{C}^0 \) was obtained for RP. An EROEI of 0.08 was calculated for tubular PBR with a productivity of 75.1 t ha\(^{-1}\) a\(^{-1}\) in the base case scenario and thus was found to be inappropriate for SNG production. EROEI for FPA-PBR with an assumed microalgae productivity of 79 t ha\(^{-1}\) a\(^{-1}\) was found to be 1.01 in the base case scenario and an SNG production cost of 266 GJ\(^{-1}\). With significantly more optimistic assumptions concerning microalgae productivity, energy input and capital requirement with respect to microalgae cultivation, an EROEI of 3.6–5.8 and SNG production costs of 53–90 GJ\(^{-1}\) were found for RP, whereas for FPA-PBR an EROEI of 2.3–3.7 and SNG production costs of 30–103 GJ\(^{-1}\) were obtained.

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1. Introduction

The potential of microalgae as a renewable energy source, as a provider of renewable bulk and high value chemicals for the chemical and pharmaceutical industry, as a source of proteins for animal feedstock and fertilizer has made them the subject of considerable research effort in the past [1,2]. However, the economic viability and energy efficiency of biofuels made from microalgae are presently intensively discussed. The main obstacles to large scale introduction of biofuels from microalgae are the high investment costs and energy input required for microalgae cultivation and harvesting [3,4].

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Yet, published data on the environmental sustainability, economic and energetic viability of biofuels from microalgae focused mainly on biodiesel [3–5]. Biomethane (biogas) from microalgae, on the other hand, has been mostly considered as a waste treatment technology for the organic leftovers from the biodiesel production process [6,7]. The economic and energetic potential of converting the entire microalgal biomass into biomethane has not received much attention. This paper considers thus the production of synthetic natural gas (SNG) via catalytic supercritical water gasification (SCWG) of microalgae with closed material flows in terms of water and nutrients, the so called SunChem process [8,9]. However, due to the immaturity of the technology, there is a significant uncertainty to determine exactly in advance to which extent the different factors can be effectively improved in the future. Consequently, a sensitivity analysis has been performed with an optimistic scenario, where half of the optimization potential is realized and a very optimistic scenario, where the optimization potential is fully exploited, based on the sensitivity analysis parameters.

Catalytic SCWG allows the production of SNG from biomass without prior drying (water content = 50%–90%) at high chemical energy conversion efficiencies of up to 70%–77% [10,11]. Such high energy conversion efficiencies are possible because at supercritical pressure the specific and latent heat demand of water is strongly decreased, thus being a promising biofuel pathway for feedstocks with high water content like microalgae [12]. Furthermore, catalytic supercritical water gasification converts the entire reactive biomass to a product gas, and due to residence times in the order of minutes high biomass conversion rates are possible on a much smaller area than for anaerobic digestion.

In addition, catalytic SCWG allows the potential recovery of nutrients from the microalgal biomass during SNG production. At supercritical water (SCW) conditions, the nutrients precipitate because the fluid exhibits very low solubility for salts. It has been shown that with a reverse flow gravity separator, type 1 and 2 salt mixtures of NaNO3/K2CO3, K2HPO4, Na2CO3/K2SO4, Na3PO4/K2SO4 and single salt solutions such as (NH4)2CO3, NH4Cl, Ca(NO3)2, (NH4)2SO4 and many more could be separated and recovered from aqueous solutions with efficiencies between 80% and 97% [13–15].

The production of chemical fertilizer was singled out by Clarenz et al. [3] and Lardon et al. [16] as a main factor concerning the environmental burden of microalgal fuels with respect to their greenhouse gas emissions, human and marine ecosystem toxicity potential as well as for the emission of acidifying substances. Conversion of microalgae to SNG via catalytic SCWG thus could reduce the consumption of nutrients for algae cultivation.

### 2. Methodology

In view of the presently high production costs and energy input for microalgae cultivation and as such for biofuels derived from microalgae, a techno-economic sensitivity analysis has been done for the production of synthetic natural gas (SNG) via catalytic supercritical water gasification (SCWG) of sweet water microalgae based on three different microalgal production systems: Raceway ponds (RP), tubular-, and flat-panel- airlift photobioreactors (FPA-PBR). This work thus gives a range of SNG production costs and energy return on energy invested (EROEI) from microalgae via catalytic SCWG according to different scenarios of technological improvements. A detailed summary of the variables settings, the sensitivity analysis and all assumptions in this model can be found in the Supporting Information (SI) provided in several additional tables and figures. In particular, the SI describes the technological and economic model as well as the performance metrics, including the equations, used in this work. The data is based on published peer-reviewed values, personal communications from manufacturers and what are regarded to be realistically achievable values. EROEI is defined according to equation (2.1). It should be mentioned that the EROEI includes power production from SNG (see SI).

\[
EROEI = \frac{\text{Usable acquired energy}}{\text{Energy expended}}
\]  

Fig. 1 gives an overview of the flowsheet of the combined microalgal cultivation and catalytic SCWG process. It is assumed that the carbon dioxide is provided from a combustion source such as a coal power plant, cement plant, biogas plant with a combined heat and power plant (CHP) or a petrochemical refinery. The dry flue gas is assumed to be composed of 15% CO2 and 85% N2 [17].

The closed PBR are not actively cooled, as they are cultivated with thermophilic algal species and because we believe that actively cooled PBR’s are not suitable for large-scale algae production due to the large amounts of heat, which need to be removed to keep the broth temperature at 298 K or 308 K (see SI for more details) [18].

A circular plant layout is assumed for the three different microalgal cultivation systems: Raceway ponds (RP), tubular-, or FPA-PBR with the flue gas source, the SCWG plant and the dewatering units in the center as shown in Fig. SI 1. The RP and PBR are positioned around the center and are organized in modules of 100 ha size. They are connected with the control and processing units via flue gas and water pipes.

### 3. Results and discussion

#### 3.1. Analysis of energy consumption: base case

Table 1 shows the results for the base case scenarios calculated on the assumptions given in Table SI 1 – Table SI 3 in the SI. Energy use for flue gas transport is highest for RP, this is not unexpected because the flue gas needs to be transported over the longest distance. For an average transportation distance of 21 km for the case with RP, 113 MJ are required to transport one tonne of CO2 from the source to the cultivation sites and 79–81 MJ t−1 for tubular- and FPA-PBR, respectively. The values obtained are similar to the 80.3 MJ t−1 for a 1000 ha direct CO2 injection system calculated by Kadam [17]. The results show that energy input for flue gas transport is a minor contribution if CO2 is supplied by large diameter low-pressure pipelines (see SI for details).

Energy input to pump the algal slurry to the dewatering location and return the reclaimed water to the cultivation
sites shows strong differences between RP, tubular- and FPA-PBR. Significantly smaller volumes of algal slurry and reclaimed water need to be transported back and forth between the dewatering and cultivation sites for tubular- and FPA-PBR (harvesting concentration of 3.6–8 g L\(^{-1}\)) than with RP. The energy need for RP is thus 4–6 times higher (7421 GJ a\(^{-1}\)) at a biomass harvesting concentration of 0.5 g L\(^{-1}\) as shown in Table 1.

Table 1 – Energy return on energy invested (EROEI) for RP, tubular PBR and FPA-PBR.

<table>
<thead>
<tr>
<th>Process unit</th>
<th>RP + SCWG</th>
<th>RP + SCWG</th>
<th>Tubular PBR + SCWG</th>
<th>Tubular PBR + SCWG</th>
<th>FPA PBR + SCWG</th>
<th>FPA PBR + SCWG</th>
</tr>
</thead>
<tbody>
<tr>
<td>Algae culture and harvesting</td>
<td>TJ a(^{-1})</td>
<td>%</td>
<td>TJ a(^{-1})</td>
<td>%</td>
<td>TJ a(^{-1})</td>
<td>%</td>
</tr>
<tr>
<td>Flue gas transport</td>
<td>8.6</td>
<td>2.5</td>
<td>6.1</td>
<td>0.1</td>
<td>6.0</td>
<td>1.0</td>
</tr>
<tr>
<td>Water circulation pumps</td>
<td>7.4</td>
<td>2.2</td>
<td>2.3</td>
<td>0.0</td>
<td>1.3</td>
<td>0.2</td>
</tr>
<tr>
<td>Dewatering</td>
<td>51.3</td>
<td>15.1</td>
<td>8.0</td>
<td>0.1</td>
<td>4.6</td>
<td>0.7</td>
</tr>
<tr>
<td>Air blowers/paddle wheels</td>
<td>213</td>
<td>62.7</td>
<td>7996</td>
<td>99.1</td>
<td>545</td>
<td>88.5</td>
</tr>
<tr>
<td>Algae conversion</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Feed pump</td>
<td>14.1</td>
<td>4.2</td>
<td>14.1</td>
<td>0.2</td>
<td>14.1</td>
<td>2.3</td>
</tr>
<tr>
<td>Gas separation</td>
<td>44.4</td>
<td>13.1</td>
<td>44.4</td>
<td>0.6</td>
<td>44.4</td>
<td>7.2</td>
</tr>
<tr>
<td>Ultrafiltration</td>
<td>0.6</td>
<td>0.2</td>
<td>0.6</td>
<td>0.0</td>
<td>0.6</td>
<td>0.1</td>
</tr>
<tr>
<td>Total energy consumption</td>
<td>339</td>
<td>100.0</td>
<td>8071</td>
<td>100.0</td>
<td>616</td>
<td>100.0</td>
</tr>
<tr>
<td>((E_{\text{required}}))</td>
<td>1895</td>
<td>1895</td>
<td>1895</td>
<td>1895</td>
<td>1895</td>
<td></td>
</tr>
<tr>
<td>Total energy of biomass ((E_{\text{algae}}))</td>
<td>1135</td>
<td>1135</td>
<td>1135</td>
<td>1135</td>
<td>1135</td>
<td></td>
</tr>
<tr>
<td>Bio-SNG ((E_{\text{SNG}}))</td>
<td>%</td>
<td>%</td>
<td>%</td>
<td>%</td>
<td>%</td>
<td></td>
</tr>
<tr>
<td>Energy efficiency</td>
<td>59.9</td>
<td>59.9</td>
<td>59.9</td>
<td>59.9</td>
<td>59.9</td>
<td>1.01</td>
</tr>
<tr>
<td>EROI</td>
<td>1.84</td>
<td>0.08</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
Typically the algal slurry is dewatered to a feed concentration of 20% total solids (TS) for catalytic SCWG (Table SI 3). In the case of RP, the energy input for dewatering accounts for a large part of the total process energy on the order of 15% due to the low initial algal biomass concentration. Accordingly, the energy input for dewatering the algal slurry from tubular or FPA-PBR is modest and only accounts for a small fraction of the total process energy.

Power consumption for air blowers and paddle wheels, in order to assure proper mixing of the culture medium and gas transfer, are very low per reactor volume (m³) for the RP compared to the other two systems. Nonetheless the large water volume required due to the low volumetric biomass productivity of RP partially offsets the low energy input and thus accounts for 63% of the total energy consumption of RP. However, as can be seen in Table 1, the energy input for CO₂ mass transfer and mixing in tubular and FPA-PBR is significantly higher. In both cases the energy input for CO₂ mass transfer and mixing accounts for 89%–99% of the energy required to cultivate the microalgae. Consequently the air blowers are the main reason for the unfavorable EROEI for the closed PBR systems. Especially the large power needs for mixing in tubular PBR of 2500 W m⁻³ (99% of the total process energy) renders this production system apparently uninteresting for biofuel production [19]. However, recent calculations from Norsker et al. [20] suggest much lower power inputs for tubular PBR on the order of <100 W m⁻³, which would make this cultivation system a net energy producer.

The energy efficiency for the conversion of algal biomass into methane through catalytic SCWG depends on the TS concentration of the feedstock and on its elemental composition. Because it is assumed in the base case that the algal slurry is dewatered to the same TS concentration and composition for all three cultivation systems, energy input as well as energy output for the catalytic SCWG process are equal. A gross energy efficiency of 59.9% is obtained for the conversion of algal biomass into SNG (detailed calculations are given in the SI). This value is slightly lower than predicted by state of the art models for SNG production from microalgae by SCWG which can be as high as 70% [10], hence showing the conservative approach of our model assumptions with respect to catalytic SCWG. The dry product gas composition at 0 °C and 0.1 MPa after the SCWG reactor consists mainly of CH₄ (51.8%) and CO₂ (44%). Some H₂ (4.1%), traces of CO (7.8 10⁻²%) and C₂H₆ (31.4 10⁻²%) are present in the product gas as well. The specific methane yield is calculated to be in the base case 0.35 kg kg⁻¹ TS of algal biomass, which is a bit lower than the above mentioned production costs for large scale algal production of 0.41 $ kg⁻¹. However, as is shown later, these values can only be achieved for highly optimized cultures. In fact, Williams and Laurens [1] calculated production costs for large scale algal production of 0.41 $ kg⁻¹. This partially offsets the advantage given by the low investment in the case of both closed photobioreactors.

In summary, the EROEI is >1 for the RP and FPA-PBR but highly unfavorable for the tubular PBR (EROEI = 0.08). It is necessary to take into account that the energy required to cultivate the microalgae is electric power. Therefore, the EROEI is significantly lower than one would expect from Table 1 if only the energy consumed during the production and conversion of the algal biomass was considered. The EROEI takes into account that the energy required to cultivate the microalgae is electric power. Therefore, the EROEI is significantly lower than one would expect from Table 1 if only the energy consumed during the production and conversion of the algal biomass was considered. The EROEI takes into account that the energy required to cultivate the microalgae is electric power. Therefore, the EROEI is significantly lower than one would expect from Table 1 if only the energy consumed during the production and conversion of the algal biomass was considered. The EROEI takes into account that the energy required to cultivate the microalgae is electric power. Therefore, the EROEI is significantly lower than one would expect from Table 1 if only the energy consumed during the production and conversion of the algal biomass was considered. The EROEI takes into account that the energy required to cultivate the microalgae is electric power. Therefore, the EROEI is significantly lower than one would expect from Table 1 if only the energy consumed during the production and conversion of the algal biomass was considered.
scenarios as well as for the RP are essentially composed of the biomass production part, whereas the actual fraction of capital investment for the catalytic SCWG of the algal biomass is very small. These results show that the economic bottleneck clearly comes from the algal biomass production part, as more than 94% of the required investment goes into the biomass production for all three scenarios.

3.3. Base case: sensitivity analysis

3.3.1. Energy sensitivity analysis

The parameters studied in this work and the ranges of variation are given in Table SI 6 in the SI. The tubular PBR was not further investigated because it became obvious during the analysis of the base case that this system is inefficient with respect to net energy production and thus not suitable for SNG production from microalgae with the present assumptions.

Figs. 2 and 3 show the results from the sensitivity analysis of the two remaining viable options with respect to the EROEI: RP and FPA-PBR. The intercept of all lines corresponds to the base case, and any point away from the intercept represents an increase or decrease of EROEI. The steeper the slope of the curve, the higher the EROEI sensitivity towards the parameter.

As can be seen in Figs. 2 and 3, both systems are quite sensitive to the following parameters: air blowers, biomass productivity and SCWG feed concentration. In contrast, the amount of CO₂ converted to algal biomass (CO₂ uptake), has almost no impact. Indeed, whether 25% (base case ±0%) or 90% (+360%) of the emitted CO₂ in the flue gas is converted to biomass is irrelevant as there is no energetic penalty for increasing the cultivation area. About 100 km² of cultivation area are required near a CO₂ source for such a scenario where 90% of the emitted CO₂ is converted into biomass (producing >310,000 t of algal biomass per year), which may represent a significant limiting factor for such an installation.

![Fig. 2 – Sensitivity analysis RP scenario: EROEI. Sensitivity parameters are shown in the legend.](image)
Present research efforts in microalgae cultivation are directed towards lowering energy input and increasing the productivity at the highest harvesting concentration possible [21]. However, it needs to be taken into account that an increase of biomass productivity by 50% or even by 100% would mean an annual production of 58–77 t ha\(^{-1}\) for RP and 119–158 t ha\(^{-1}\) for FPA-PBR. Consequently this would correspond to a photosynthetic efficiency between 2.6% and 3.5% for RP and 5.4%–7.2% for FPA-PBR (based on 5040 MJ m\(^{-2}\) solar irradiance for Switzerland) which is close to the maximum theoretical amount of 9% of the incoming solar irradiation that can be converted into algal biomass [23]. Such high productivities have never been reached in year-round outdoor cultivations, but only under laboratory conditions. From an energetic point of view, it would therefore be easier to focus on lowering the energy input for microalgae cultivation instead of increasing the productivity as both parameters improve the EROEI by a similar level.

With an energy input of 0.29 MJ per cubic meter of algal slurry processed for the belt filters and 3.6 MJ m\(^{-3}\) for the centrifuge (Table SI 1), the energy input for dewatering 1 kg of algal biomass to 20% TS is as low as 0.59 MJ kg\(^{-1}\) for RP and 0.15 MJ kg\(^{-1}\) for FPA-PBR, assuming 100% biomass recovery. As the belt filters preconcentrate the algal slurry to a concentration of 9.5% TS for the centrifuge, the difference in energy input to recover 1 kg TS of microalgae, is due to the belt filters. Indeed, this explains the small impact of the energy input for dewatering or the harvesting concentration if they are continuously varied in the sensitivity analysis, the base case containing 0.29 MJ m\(^{-3}\) of processed algal slurry for the belt filters. Lardon et al. [16] assumed an electricity input of 1.44 MJ kg\(^{-1}\) microalgae for belt filters which is 2.5 times higher than the values proposed by Mohn [24]. A more conservative assumption for the energy consumption for the belt filters would thus strongly affect the EROEI of the overall process. For example, a similar electricity input for the belt filters as proposed by Lardon et al. [16] would reduce the EROEI for the RP base case by 18% to 1.51. It is energetically favorable to dewater the incoming algal slurry as much as possible before the gasification step as shown in Figs. 2 and 3. Low feed concentrations for the SCWG plant, for example 5% TS (−75%), means saving energy during the dewatering step, but consequently mostly water is pumped through the SCWG plant and heated up to supercritical water conditions, instead of biomass. As this step requires much more energy than can be saved during the dewatering step, the EROEI in both cases drops quickly below one. Thus, it should be the aim to dewater the algal slurry up to 30% TS, as long as the resulting algal slurry remains pumpable.

3.3.2. Production costs sensitivity analysis

Table SI 7 in the SI shows the parameters used for the economic sensitivity analysis to calculate the price of one energy unit of SNG expressed in Euro per Gigajoule (€ GJ\(^{-1}\)). The intervals were chosen in such a way to reflect possible future improvements. Especially the large decrease in construction costs up to −90% shall take into account future cost reductions. This value corresponds to construction costs of only 230,000 € ha\(^{-1}\) for a fully installed PBR unit (including harvesting and storage), whereas in the base case the costs are 7 times higher for 1 ha of land covered with PBR.

Fig. 4 shows the results of the sensitivity analysis for the RP. The parameters with the highest saving potential are the harvesting concentration of the algal biomass, the concentration of the feed into the SCWG plant after the dewatering and the biomass productivity. The effect of harvesting at high biomass concentrations allows reducing significantly the investment costs for the dewatering equipment. However, the effect levels off at 128 € GJ\(^{-1}\), and a harvesting concentration of >2 g L\(^{-1}\) in RP will not reduce further the dewatering costs significantly. If only the costs for dewatering are considered, the costs to obtain 1 kg of dry algal biomass by dewatering the wet algal slurry decreases from 0.67 € kg\(^{-1}\) TS to 0.17 € kg\(^{-1}\) TS (without considering labor and maintenance). This result points to the necessity of cultivating microalgae in such a way that they can be harvested easily, for example, by cultivating microalgae species with a natural tendency to float, or focusing on macroalgae instead of microalgae. An increase of productivity is not shown in Figs. 2 and 3. Low feed concentrations for the SCWG plant, for example 5% TS (−75%), means saving energy during the dewatering step, but consequently mostly water is pumped through the SCWG plant and heated up to supercritical water conditions, instead of biomass. As this step requires much more energy than can be saved during the dewatering step, the EROEI in both cases drops quickly below one. Thus, it should be the aim to dewater the algal slurry up to 30% TS, as long as the resulting algal slurry remains pumpable.
required under such conditions. However, flocculation is not considered as a viable long term option for the SunChem process. For instance, the need of large amounts of chemicals does not fit into the closed loop aspect of the SunChem process, where all materials shall be as much as possible recycled.

Dewatering the harvested biomass to a slurry with 30% TS of algal biomass instead of 20% TS reduces the production costs to 167 € GJ⁻¹ instead of 194 € GJ⁻¹, i.e. a reduction by −14%. This further increase of the dry matter content by 50% for the hydrothermal gasification step is probably the most easy to achieve.

If the productivity of RP can be increased by 100% to 77 t ha⁻¹ a⁻¹, a 22% reduction in production costs compared to the base case may be achieved (152 € GJ⁻¹). This is due to the effect that a smaller production surface is required in order to achieve the same annual biomass productivity and thus smaller investment costs for the RP are necessary. Furthermore, labor costs decrease as well because a smaller surface has to be maintained. However, it clearly needs to be stated that such a high productivity in RP, due to poor mixing of the microalgae and the light exposure regime, is questionable and has to the authors’ knowledge not yet been shown for year-round outdoor cultivation [4].

The production costs only show little sensitivity towards the remaining parameters. Interestingly, whether the nutrients N and P are free (would correspond to 100% nutrient recycling efficiency from the SCWG process) or a carbon tax of 36 € per tonne of CO₂ can be generated by displacing fossil natural gas, the SNG production costs are not significantly lowered. Nevertheless, it must not be forgotten that recycling nutrients strongly reduces the environmental impact of the SunChem process [3].

FPA-PBR show a different cost structure compared to the RP, as shown in Fig. 5. Even though the biomass productivity as well as the dry matter content of the algal slurry fed into the SCWG plant plays an important role, clearly the most sensitive parameter with respect to production costs is the high investment cost for FPA-PBR. A reduction of 90% in construction costs for fully installed PBR (230,000 € ha⁻¹) leads to a decrease in production cost of 66% and to a production cost of 91 € GJ⁻¹. However, such a reduction in construction costs is challenging. Accordingly to a recent study, construction costs of 800,000 € ha⁻¹ were proposed for an FPA-PBR (including harvesting and storage of biomass) [25].

### 3.4 Economic and energetic optimization potential

The economic sensitivity analysis presented in the previous section showed that even large improvements of one single parameter with respect to algal biomass production, SCWG and construction costs are not sufficient to obtain an economic process with a positive energy balance. The lowest SNG production costs obtained in the sensitivity analysis by changing one parameter were 128 € GJ⁻¹ for the RP and 91 € GJ⁻¹ for the FPA-PBR. This is still 4–7 times higher than the targeted renewable energy price of 20 € GJ⁻¹ [26]. Moreover, the highest EROEI for RP was 2.7 and 1.8 for FPA-PBR by doubling the biomass productivity. In short, EROEI and production costs can be improved significantly further by improving multiple parameters simultaneously.
optimistic scenario would only divide the production costs by less than two ($3 \text{ € GJ}^{-1}$) and thus still be significantly higher than present energy prices.

Surprisingly, the production costs obtained in the very optimistic scenario for the FPA-PBR are the lowest of all scenarios with only specific production costs of $30 \text{ € GJ}^{-1}$ and thus reversed the trend shown in all other scenarios. This behavior is due to two reasons: raceway ponds, due to their lower biomass productivity, require a larger surface area for cultivation than FPA-PBR and therefore implicitly also need more personnel, based on the assumption that 7 persons are required for engineering and maintenance per 100 ha [25]. The labor costs thus are almost twice as big in the case of the very optimistic scenario for RP compared to the FPA-PBR and account for 43% of the total production costs (see Table SI 5). Clearly, labor costs need to be taken into account, as they make up 30–45% of the production costs in the case of the raceway ponds and 10–40% for the FPA-PBR, depending on the scenario. Therefore, not only higher productivities or reduced material costs play a role, but also the automation of the algal production is very important and needs to be considered in the future, something that has largely been overlooked up to now. Alternatively, locations for algal biomass production with low labor costs need to be considered.

The second reason is due to the limited harvesting concentration of 2 g L$^{-1}$ for RP, which means high investment costs for dewatering equipment.

Interestingly, up to this point, the production costs related to the SCWG plant played only a marginal role. For example, the contribution to the production costs was in the base case 3.7% for RP and 2.7% for FPA-PBR (see Table SI 5). This is not anymore the case in the very optimistic scenario, where 14.6% of the production costs are due to the SCWG plant for FPA-PBR and 8.4% for RP (including gas upgrading).

Finally, a large number of claims concerning microalgae and biofuel production costs have been made over the last years by some algal biofuel start-up companies. Interestingly, most of the claims concerning the very low production costs could not be reconstructed in this work as well as in other publications [1,2,4,28]. Some of these reports [29–31] give no details on the assumed labor costs behind their calculations. Holtermann et al. [31] assumed maintenance and operating costs based on 2% of the investment sum, which is about 7–9 times lower than what was obtained in this work under any scenario. The separately estimated maintenance and labor costs and plant overheads are shown in Table SI 4. These values are based on the estimations from Norsker et al. and Grima et al. [25,28] and lead to the significantly higher operation and maintenance costs which were used in this study. Another misleading assumption is the actual obtained outdoor biomass productivity, which in some cases are unrealistically high. Unfortunately it is not possible to verify these data published from start-up companies due to their non-disclosure policy. Whether the data are obtained from outdoor culture experiments or simply inaccurate extrapolations of literature data or from laboratory experiments remains unanswered.

4. Conclusions

The present work showed that the economical and energetic bottleneck for the production of SNG from algal biomass is not the actual conversion of the wet biomass by catalytic hydrothermal gasification, but the necessity to grow microalgae in artificial culture systems (RP or PBR). More than 95% of the required investment costs and between 40 and 55% of the production costs are related to the algal biomass production in the base case scenarios. Under very optimistic assumptions with respect to algal biomass production in the case of the RP and FPA-PBR scenarios more than 70% of the investment costs and about 26% of the production costs are due to the algal biomass production part.

However, the assumed investment costs as well as the algal productivities are not easily achievable, and involve a complete change in algal biomass production technology, including novel harvesting technologies, novel reactor materials and designs and algal species with a high productivity as well as a natural tendency to agglomerate rather than to produce high lipid contents. Nevertheless, the calculated production costs are still too high compared with the present price for natural gas.

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Appendix A. Supplementary data

Supplementary data related to this article can be found at http://dx.doi.org/10.1016/j.biombioe.2012.12.038.
REFERENCES


