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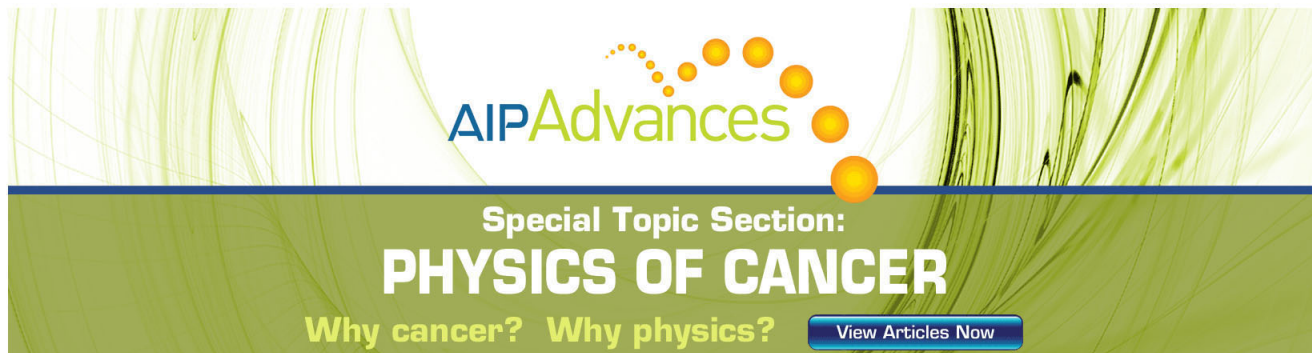
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Small-signal amplifier based on single-layer MoS₂

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In this letter we demonstrate the operation of an analog small-signal amplifier based on single-layer MoS₂, a semiconducting analogue of graphene. Our device consists of two transistors integrated on the same piece of single-layer MoS₂. The high intrinsic band gap of 1.8 eV allows MoS₂-based amplifiers to operate with a room temperature gain of 4. The amplifier operation is demonstrated for the frequencies of input signal up to 2 kHz preserving the gain higher than 1. Our work shows that MoS₂ can effectively amplify signals and that it could be used for advanced analog circuits based on two-dimensional materials. © 2012 American Institute of Physics. [<http://dx.doi.org/10.1063/1.4738986>]

The limits of further miniaturization of silicon nanoelectronic devices lead to an emerging development of novel nanomaterials. It is anticipated that silicon complementary metal-oxide semiconductor (CMOS) technology will reach the scaling limit in the near future. Electronic materials, such as semiconductor nanowires,¹ carbon nanotubes,² III-V compound semiconductors,³ are proposed as promising candidates to replace silicon in electronic devices. On the other side, two-dimensional materials, such as graphene and transition-metal chalcogenides, are attractive for novel nanoelectronic devices because, compared to working with one-dimensional materials, it is relatively easy to tailor them in desired shape and fabricate very complex structures from them. Being just few angstroms thick, 2D materials are very attractive for new generation transistors. Scaling theory predicts that short-channel effects, such as threshold voltage roll-off, drain-induced barrier lowering, and impaired drain current saturation, in field-effect transistors should be much less pronounced in this case.⁴ Graphene,⁵ an atomically thin two-dimensional sheet of graphite, is very promising because of its extraordinary properties, such as high carrier mobility up to 230 000 cm²/Vs (Ref. 6) and two-dimensional geometry that is at the ultimate limit in vertical device scaling. In its pristine form, graphene does not have a bandgap that is of crucial importance for realization of field-effect transistors (FETs) with satisfactory on/off ratios. We have recently shown⁷ that field-effect transistors based on monolayer MoS₂ have room temperature mobility comparable to that of the best graphene nanoribbons fabricated to date⁸ and strained thin silicon films,⁹ with current on/off ratio higher than 10⁸.

Single-layer MoS₂, 6.5 Å thick, is a 2D direct gap semiconductor that can be exfoliated from bulk crystal using scotch tape micromechanical cleavage,¹⁰ lithium intercalation,¹¹ or liquid exfoliation methods.¹² Its energy bandgap of 1.8 eV (Ref. 13) makes it very suitable for nanoelectronic applications, such as field-effect transistors,⁷ and devices based on them, such as digital logic gates¹⁴ and analog small-signal amplifiers. Single-layer MoS₂ is also 30 times stronger than steel¹⁵ which makes it suitable for use in flexi-

ble electronics. Additionally, by decreasing the number of layers in MoS₂ crystal stack down to monolayer, an indirect bandgap of 1.2 eV converts to a direct one of 1.8 eV, giving an opportunity for engineering new optoelectronic behaviors and gives promise for new nanophotonic applications.¹⁶

Here, we demonstrate the realization of integrated voltage amplifier based on 2D semiconducting material MoS₂ with voltage gain G higher than 1, making it suitable for incorporation in analog circuits where amplification of small AC signals is necessary. Thanks to its very high input impedances, such amplifiers may be essential when dealing with the high-impedance signal sources in new nanoelectronic devices.

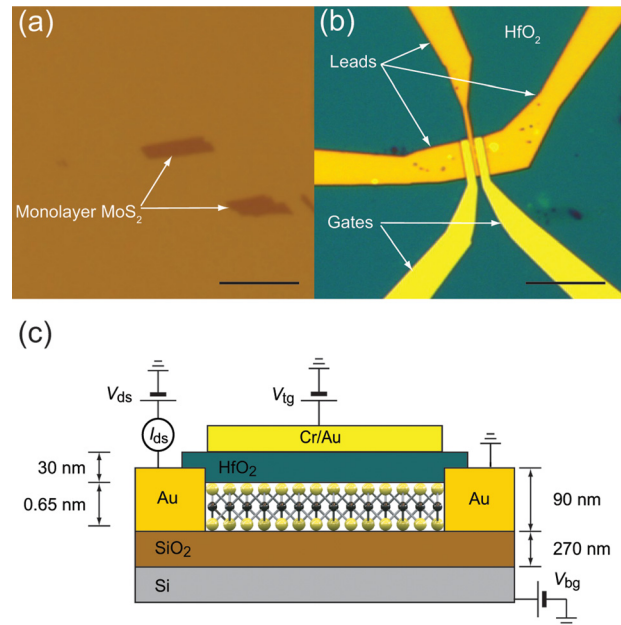


FIG. 1. Fabrication of single-layer MoS₂ amplifiers. (a) Optical image of monolayer MoS₂ flakes deposited on top of a silicon chip with 270 nm thick SiO₂ layer. (b) Optical image of two field-effect transistors connected in series, fabricated on the upper flake shown in (a). (c) Cross-sectional view of a field-effect transistor based on single-layer MoS₂. Gold leads are used for the source and drain electrodes. The silicon substrate was used as a back-gate with the 270 nm SiO₂ layer used as a dielectric. Top-gates were fabricated with Cr/Au leads and 30-nm-thick HfO₂ dielectric. Scale bars in (a) and (b) are 10 μm.

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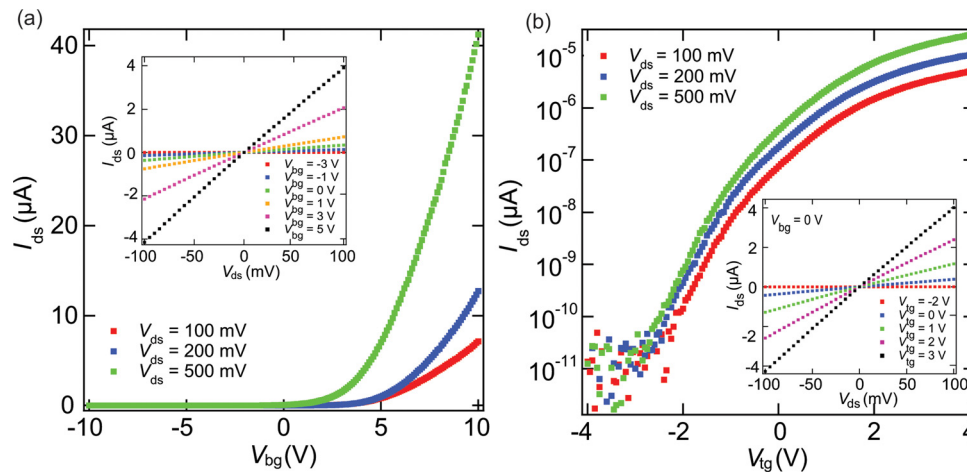


FIG. 2. Electrical characterization of the field-effect transistors based on monolayer MoS₂. (a) I_{ds} - V_{bg} curves acquired for different drain-source biases, indicating presence of n-type channel in our FET. Back-gate voltage is applied to the substrate and top-gate is disconnected. Extracted field-effect mobility from two-contact measurement is $\sim 380 \text{ cm}^2/\text{Vs}$. Inset: I_{ds} - V_{ds} curves for V_{bg} ranging from -3 to 5 V. (b) Transfer characteristic of our FET for different source-drain biases. The device can be turned-off by changing the top-gate voltage from 2 to -2 V. The current on/off ratio is $> 2 \times 10^6$ and subthreshold swing is $\sim 500 \text{ mV}/\text{dec}$. Inset: I_{ds} - V_{ds} curves recorded for different V_{tg} , with linear dependence clearly indicating ohmic gold contacts. Back-gate electrode is grounded.

We start the fabrication of our transistors with scotch-tape micromechanical exfoliation⁵ of single-layer MoS₂ on top of the degenerately doped silicon substrate covered with 270 nm thick SiO₂, as shown in Fig. 1(a). This oxide thickness has been shown to be the optimal one for optical detection of single-layer MoS₂.¹⁷ The resulting single-layer MoS₂ is highly crystalline.¹⁸ Electrical leads for the source and drain are fabricated using electron-beam lithography, followed by evaporation of 90-nm -thick Au layer and standard metal lift-off procedure in acetone. In order to decrease contact resistance and remove resist residue, devices are annealed in Ar/H₂ atmosphere at 200°C for 2 h .¹⁹ After that, devices are covered with 30-nm -thick layer of HfO₂ deposited by atomic layer deposition (ALD). ALD is performed in a Beneq system using a reaction of H₂O with tetrakis(ethylmethylamido)hafnium at 200°C . HfO₂ has a dielectric constant of ~ 19 and acts as a top-gate dielectric. Finally, another electron-beam step is performed for top gate electrodes and followed by Cr/Au ($10/50 \text{ nm}$) metallization. The typical structure of our devices, in this particular case, composed of two transistors connected in series is shown in Fig. 1(b). We have previously demonstrated that different devices realized in the same geometry can perform digital logic operations.¹⁴ Cross-sectional view of a field-effect transistor based on single-layer MoS₂ is shown on Fig. 1(c).

Before connecting them in the amplifier circuit, we perform basic electrical characterization of our MoS₂ transistors. All electrical measurements are carried out using National Instruments Digital Acquisition cards, a home-built shielded probe station, and an Agilent E5270B parameter analyzer. In Fig. 2 are shown electrical characteristics of one of our transistors. The second transistor used for the realization of an integrated amplifier presented in this letter has very similar electrical characteristics, a prerequisite for operation in an electrical circuit. All measurements are performed in the air at room temperature. First, we applied drain-source bias V_{ds} to a pair of gold leads and back-gate voltage V_{bg} to the silicon substrate which acts as a back-gate electrode, as it is highly p-doped. These gating characteristics are presented in Fig. 2(a),

showing a typical behavior of FETs with an n-type channel. Using the expression $\mu = [dI_{ds}/dV_{bg}] \times [L/(WCV_{ds})]$, where $L = 1.6 \mu\text{m}$ is the channel length, $W = 4.2 \mu\text{m}$ is the channel width, and $C = 1.3 \times 10^{-4} \text{ F m}^{-2}$ is the back-gate capacitance per unit area ($C = \frac{\epsilon_0 \epsilon_r}{d}$; $\epsilon_0 = 8.85 \times 10^{-12} \frac{\text{C}}{\text{m}}$; $\epsilon_r = 3.9$; $d = 270 \text{ nm}$), we extracted field-effect mobility of $\sim 380 \text{ cm}^2/\text{Vs}$. This is still a lower limit of mobility as it is a two-contact measurement and contact resistance is not excluded. Linear

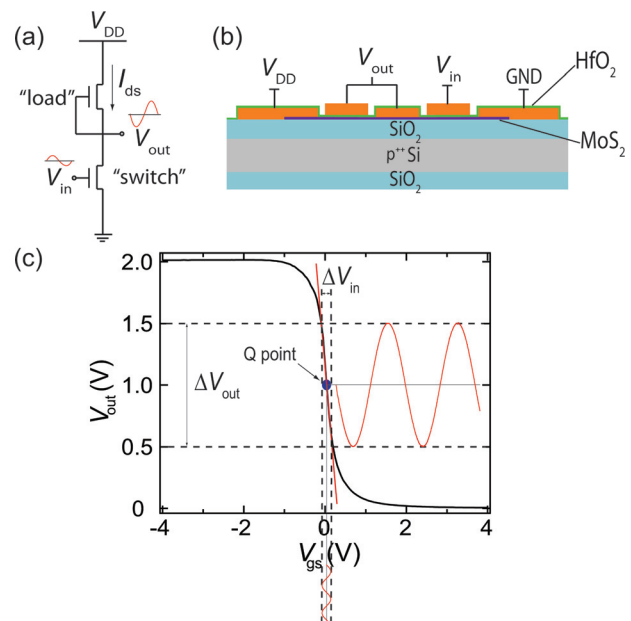


FIG. 3. Transfer characteristic of the integrated MoS₂ amplifier. (a) Schematic drawing of integrated amplifier in common-source configuration. The lower transistor acts as a “switch” and upper as a “load.” (b) Vertical cross-section of the amplifier device from Fig. 1(b) with appropriate wire connections. (c) Transfer characteristic of the integrated amplifier realized with two transistors on the same MoS₂ flake. The “switch” transistor is first biased at a certain DC gate bias to establish a desired drain current, shown as the “Q”-point (quiescent point). At that point the “load” transistor has a certain constant resistance and acts as an active resistor. A small AC signal of amplitude $\Delta V_{in}/2$ is then superimposed on the gate bias of the “switch” transistor, causing the output voltage to oscillate synchronously with a phase difference of π .

dependence of drain-source current I_{ds} on bias voltage V_{ds} clearly indicates the ohmic character of our gold contacts (Fig. 2(a) inset). The two-contact on-resistance is $25\text{ k}\Omega$ for $V_{bg} = 5\text{ V}$ and drain-source bias $V_{ds} = 100\text{ mV}$.

Local gate control of charge density in MoS_2 channel of our transistor is shown in Fig. 2(b). This is achieved via a Cr/Au top gate where the role of top-gate dielectric is played by a 30-nm-thick HfO_2 ALD layer. During these measurements, the back-gate is kept grounded. For drain-source bias $V_{ds} = 500\text{ mV}$, we recorded a maximal on-current of $25\text{ }\mu\text{A}$ ($5.94\text{ }\mu\text{A }\mu\text{m}^{-1}$) and an off-current smaller than 5 pA ($1.18\text{ pA }\mu\text{m}^{-1}$), resulting in a current on/off ratio of $\sim 2 \times 10^6$ in the $\pm 4\text{ V}$ top-gate voltage range. Subthreshold swing is $\sim 500\text{ mV/dec}$, reaching 150 mV/dec for some of our devices. In the inset of Fig. 2(b) we present the dependence of drain-source current I_{ds} on drain source bias V_{ds} for different top-gate voltages, indicating efficient local-gate control of the channel resistance.

After basic characterization of the transistors we connect them in the amplifier circuit, as shown in Fig. 3(a). In this letter, we demonstrate an integrated common-source analog amplifier that basically has a function of amplifying small AC signal with negative gain $|G| > 1$. We have already demonstrated that a different device with the same layout could

operate as a digital circuit.¹⁴ This circuit consists of two transistors connected in series, where one acts as a “switch” (lower one in Fig. 3(a)) and the other one acts as an active “load” (upper one in Fig. 3(a)). The gate of one of the transistors (“switch” transistor) acts as input, whereas the gate of the other (“load” transistor) acts as the central lead and acts as the output (Fig. 3(b)). Power supply of the amplifier V_{DD} is set to be 2 V . The DC transfer characteristic of the amplifier based on the transistor from Fig. 2 acting as a “load” is shown in Fig. 3(c). When a small AC signal V_{in-AC} is superimposed on the DC bias V_{gs} at the input, $V_{in} = V_{gs} + V_{in-AC}$, then under the right circumstances the transistor circuit can act as a linear amplifier. The transistor is first biased at a certain DC gate voltage to establish a desired current in the circuit, shown as the Q-point in Fig. 3(c). A small sinusoidal AC signal V_{in-AC} of amplitude $\Delta V_{in}/2$ is then superimposed on the gate bias on the input, causing the output voltage V_{out} to oscillate synchronously with a phase difference of 180° with respect to V_{in-AC} . The steepest region of the $V_{out}-V_{gs}$ curve can be approximated by a straight line (red line in the Fig. 3(c)) where the slope represents the voltage gain G of the amplifier. In this case the gain of our amplifier is $|G| > 4$. It is important to note that for practical applications, a gain higher than 1 is desired.

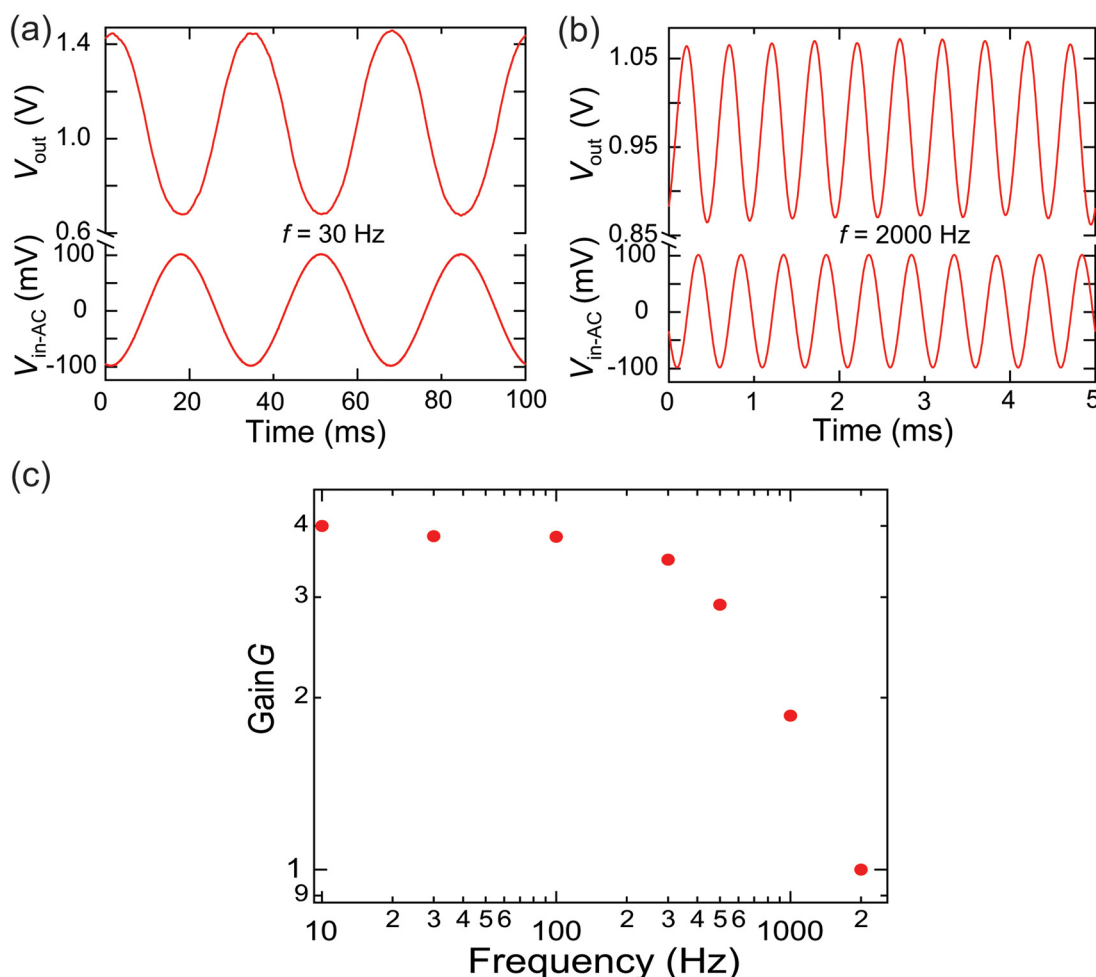


FIG. 4. Demonstration of the small-signal amplifier operation. On the input terminal of the amplifier, a sinusoidal signal V_{in-AC} of amplitude $\Delta V_{in} = 100\text{ mV}$ and frequencies of (a) 30 Hz and (b) 2000 Hz is applied with DC bias of $V_{gs} = 0\text{ V}$, resulting in an amplified sinusoidal signal on the output. The output signal is shifted in phase for 180° with respect to the input signal, in agreement with the standard characteristic of common-source amplifiers. (c) Voltage gain dependence on frequency of the small input signal. Voltage gain $|G| = \Delta V_{out}/\Delta V_{in}$ up to 100 Hz frequency of the input signal is ~ 4 and decreases with increasing frequency.

To allow for maximum output voltage swing, the Q-point should be positioned approximately in the middle of the steepest region of the transfer characteristic in Fig. 3(c). We achieve this by applying a DC bias of $V_{gs} = 0$ V to the top gate of our “switch” transistor and superposing AC signals V_{in-AC} of different frequencies on this gate bias. We have applied small AC signal of 100 mV amplitude with frequency ranging from 30 to 2000 Hz shown in Figs. 4(a) and 4(b), respectively. It is important to notice that the AC signal is amplified and shifted in phase for 180° , in agreement with the standard characteristic of common-source amplifiers. As shown in Fig. 4(c) we performed measurements up to 2 kHz preserving the voltage gain higher than 1. For small frequencies (30 Hz) we can see that the gain $|G| = \Delta V_{out}/\Delta V_{in}$ is larger than 4. By increasing the frequency, the gain is reduced, reaching 1 at 2000 Hz. This is due to the influence of high parasitic capacitances and fringing fields that can be decreased by further circuit engineering, and by improving the device transconductance.

We have fabricated single-transistor amplifier as well, where the role of “load” plays a resistor of $30\text{ M}\Omega$ (see supplementary material²⁰). The device consists of one transistor fabricated on monolayer MoS_2 flake connected in series with an off-chip load resistor. For some of our devices by using different load resistors and bias voltages V_{DD} we were able to extract voltage gain G larger than 10.

In conclusion, we have demonstrated an integrated small-signal analog amplifier based on single-layer MoS_2 field-effect transistors. The amplifier is built using top gated MoS_2 transistors connected in series, which, with appropriate wiring, form an amplifier circuit with negative gain. Our amplifier exhibits a small-signal voltage gain higher than 4 and reaching 10 in the single-transistor configuration, surpassing graphene-based two-dimensional amplifiers.²¹ Operation of amplifiers with frequencies up to 2 kHz has been shown, with gain higher than 1 and no signal distortion. The frequency range can be further extended by decreasing parasitic capacitances of contacts, using exclusively on-chip wiring to connect the transistor gates and improving transistor transconductances. With a possibility of large scale production by solution-based processing or large-scale growth of MoS_2 thin films²² and the high mechanical strength of single-layer MoS_2 ,¹⁵ our result could be very important for the realization of low cost and flexible small-signal amplifiers of new generation with higher integration densities.

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