

# Kinetic Modeling of Batch Slurry Reactions

Paul J. Gemperline<sup>1</sup>, Mary Ellen McNalley<sup>2</sup>, Ron Hoffman<sup>2</sup>, Chun Hsieh<sup>1</sup>, David Joiner<sup>1</sup>, Julien Billeter<sup>1</sup>

(1) East Carolina University, (2) DuPont Crop Protection

June 27, 2012

XIII Chemometrics in Analytical Chemistry
Budapest, Hungary



## Overall project goal – develop monitoring technique for batch processes involving slurries

- Extend kinetic modeling approach to a prototypical slurry reaction at DuPont: sulfonylurea coupling reaction for monitoring purposes
- Make optical measurements in light-scattering medium
- Modify kinetic models to include:
  - Dissolution of starting material A & flow-in of reagent B
  - Nucleation and crystallization of product, P
- Develop empirical models for dissolution, nucleation and crystallization
- Kinetic models with reagent flow-in impose strict mass balance



## Isothermal model with flow-in reagents

$$r_{1} = k_{1}C_{SA}C_{AA}$$

$$r_{2} = k_{2}C_{I}$$

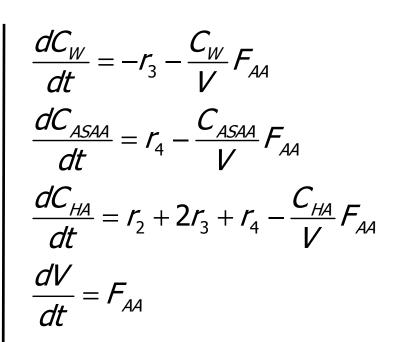
$$r_{3} = k_{3}C_{W}C_{AA}$$

$$r_{4} = k_{4}C_{ASA}C_{AA}$$

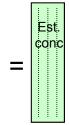
$$\frac{dC_{AA}}{dt} = -r_1 - r_3 - r_4 + \frac{C_{AAin} - C_{AA}}{V} F_{AA}$$

$$\frac{dC_I}{dt} = r_1 - r_2 - \frac{C_I}{V} F_{AA}$$

$$\frac{dC_{SA}}{dt} = -r_1 - \frac{C_{SA}}{V} F_{AA}$$







X Est. pure spectra



- A dynamic system of crystalline material suspended in a liquid medium
- Common Examples
  - Production of pharmaceuticals
  - Production of fine chemicals
  - Biological absorption of pharmaceuticals
- Dynamic processes
  - Dissolution of starting materials
  - Nucleation and crystal growth of products

### Crystal products

- Often desire specific properties
  - Size distribution, lattice form, etc.
- Relative rates determine properties
- Factors governing process rates
  - Temperature
  - Rate of stirring
  - Crystal surface area
  - Attrition
  - Agglomeration



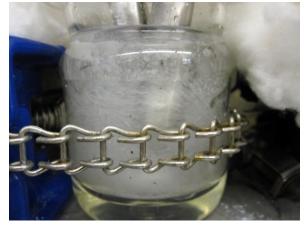
## **Challenges – Optical Methods in Slurries**

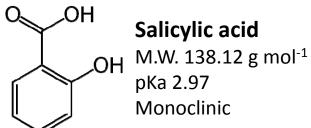
- Linear response is needed for kinetic modeling and self-modeling curve resolution
- Reflectance measurements include both light scattering and light absorption signals
  - Mathematical resolution of the two is needed to estimate solid fraction and dissolved fraction
  - Effective path length is dependent on
    - Number density of light scattering particles
    - Particle size distribution
    - Wavelength
- ATR measurements for light absorption (dissolved fraction)

# Project 1: modeling of dissolution of salicylic acid

$$r = k(c_{sat} - c)^n$$

- □ Develop a kinetic model for the dissolution of salicylic acid in a solvent mixture (52% ethanol, 48% water), based on a power law equation
  - ☐ simpler system, easily controlled
  - help gain understanding about kinetic of dissolution and crystallization in general
  - Precisely controlled conditions will facilitate model validation
- $\Box$  Optimize the rate constant (k) and the exponent (n) of the power law equation

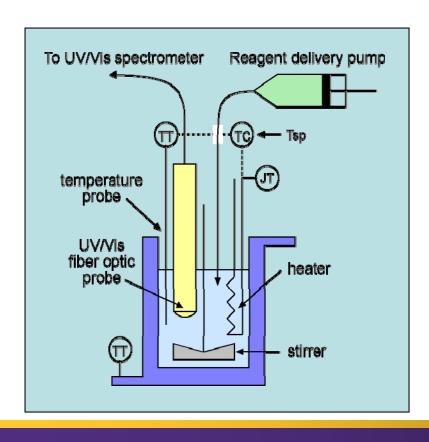






# Laboratory scale batch reactors

**Batch Titration Reactor** 

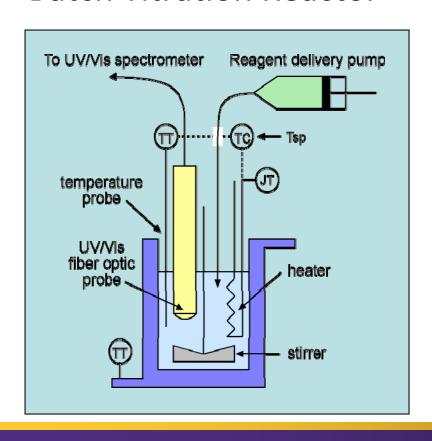






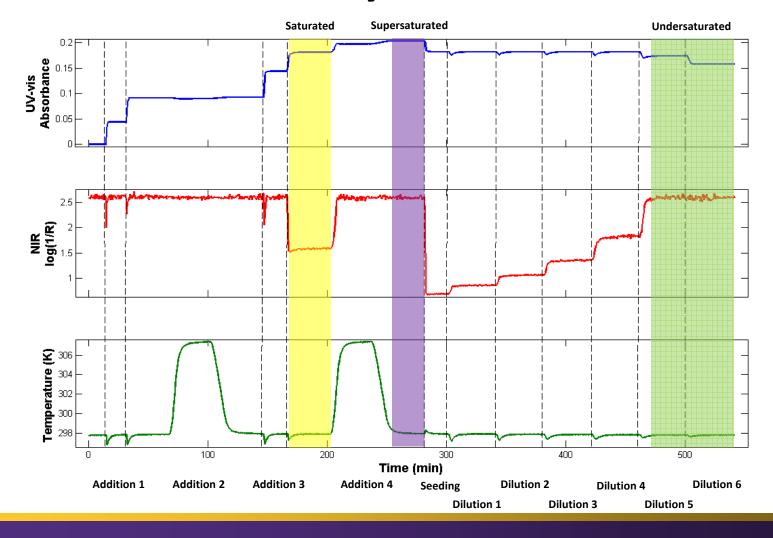
# Laboratory scale batch reactors

**Batch Titration Reactor** 





## Dissolution of salicylic acid





## Simplifying Assumptions

Crystallization Rate

Dissolution Rate

high theory model

$$r_c = \frac{\Phi_s M W_s k_c}{3d_s \Phi_v} \eta_r (c - c_{sat})^g \qquad r_d = \frac{2M W_s k_d}{d_s} (c_{sat} - c)$$

$$r_d = \frac{2MW_s k_d}{d_s} (c_{sat} - c)$$

low theory model

$$r_c = k_c (c - c_{sat})^g$$

$$r_d = m \cdot k_d (c_{sat} - c)^n$$

### **Assumptions:**

Well-mixed slurries, the length of crystals, solid density, effectiveness factor, molecular weight of the solid, surface factor and volumetric shape factor do not change significantly in these experiments.



## Model batch (08-29-10)

 Hessian

 1.0000
 -0.9383
 -1.0000
 0.6118
 0.1929
 0.1540

 -0.9383
 1.0000
 0.9384
 -0.5082
 -0.2022
 -0.1508

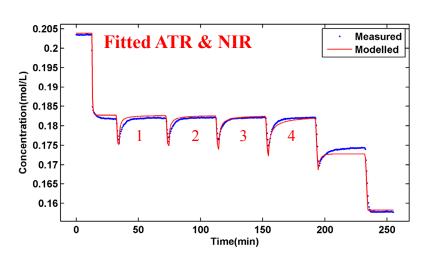
 -1.0000
 0.9384
 1.0000
 -0.6116
 -0.1928
 -0.1540

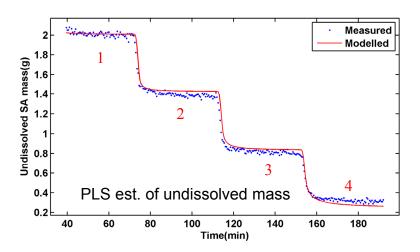
 0.6118
 -0.5082
 -0.6116
 1.0000
 0.7244
 0.0860

 0.1929
 -0.2022
 -0.1928
 0.7244
 1.0000
 -0.0514

 0.1540
 -0.1508
 -0.1540
 0.0860
 -0.0514
 1.0000

UV-vis range used:: 270 – 360 nm, NIR range used: 1100 nm





### **Initial Conditions:**

Dissolution rate constant (kd) =  $30.00 L^{n-1}/(mol^{n-1}min)$ 

Crystallization rate constant (kc) =  $15.00 L^{n-1}/(mol^{n-1}min)$ 

Order parameter (n) = 1.800

Order parameter (g) = 1.700

Total SA mass added (mt) = 3.1882 g

Concentration (c0) = 1.0176 (mol/L)

Saturation limit (csat) = 0.9075

Initial volume (v0) = 22.7 mL

Correction factor (cf) = 15

### **Optimized Parameters:**

Dissolution rate constant (kd) =  $22.16 L^{n-1}/(mol^{n-1}min)$ 

Crystallization rate constant (kc) =  $9.115 L^{n-1}/(mol^{n-1}min)$ 

Order parameter (n) = 2.034

Order parameter (g) = 1.194

Saturation limit (csat) = 1.010 (mol/L)

Correction factor (cf) = 14.27

Sum of Square (SSQ) = 0.5221



## **Experiment 2**

- Reaction of Salicylic Acid to form Acetylsalicylic Acid (Aspirin)
  - Simple, well understood reaction to test modeling ability
- Process includes:
  - Dissolution
  - 4 Primary Reactions
  - Crystallization



### **Reaction Mechanisms**

### **Catalyzed Reaction**

$$SA + AA \xrightarrow{k_1} ASA + HA$$

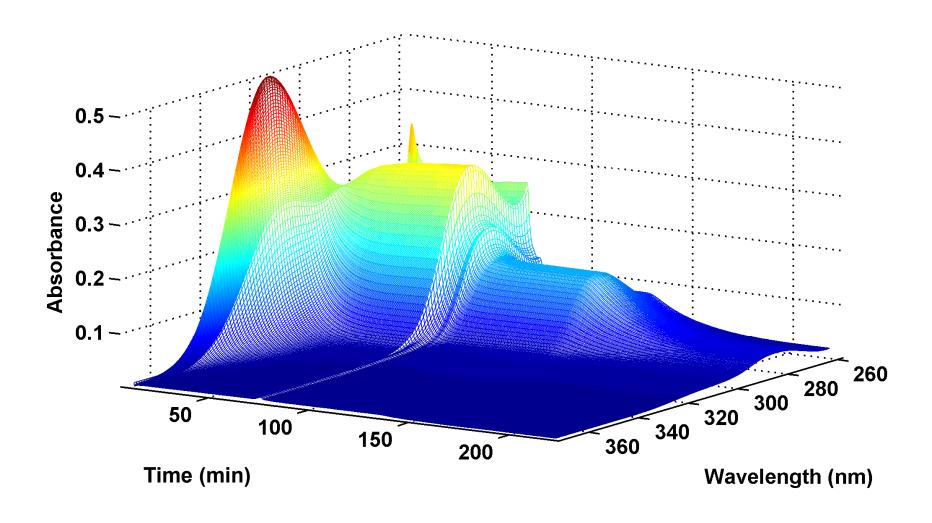
$$ASA + AA \xrightarrow{k_2} ASAA + HA$$

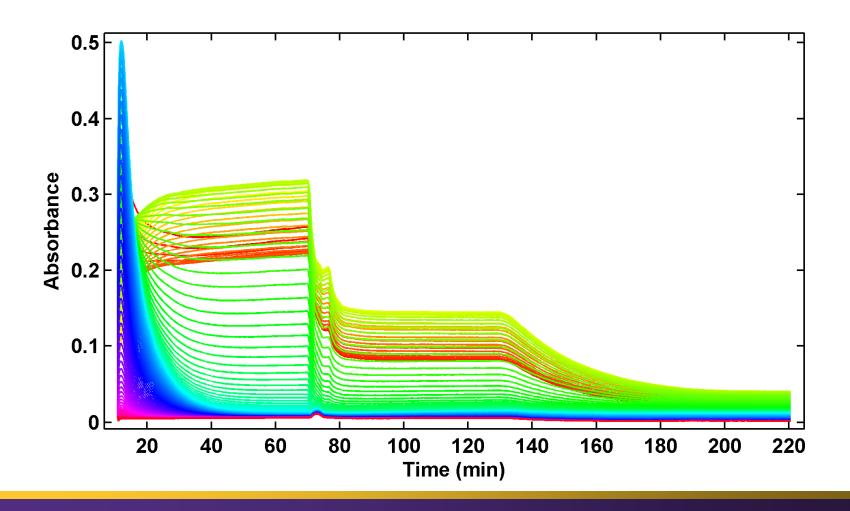
### **Water Addition**

$$ASAA + H_2O \xrightarrow{k_3} ASA + HA$$

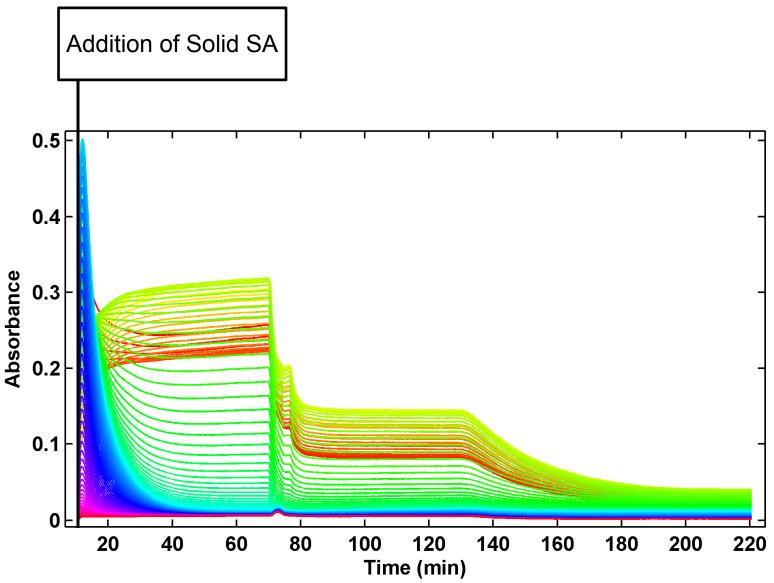
$$AA + H_2O \xrightarrow{k_4} 2HA$$



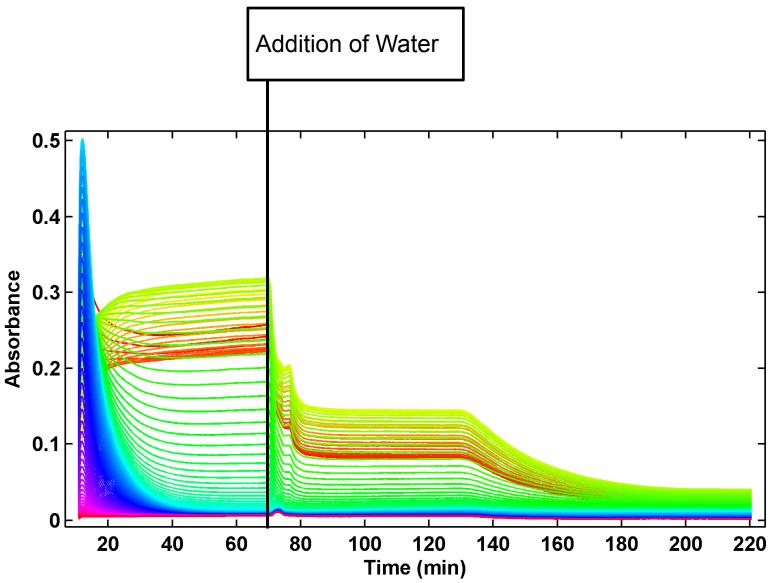


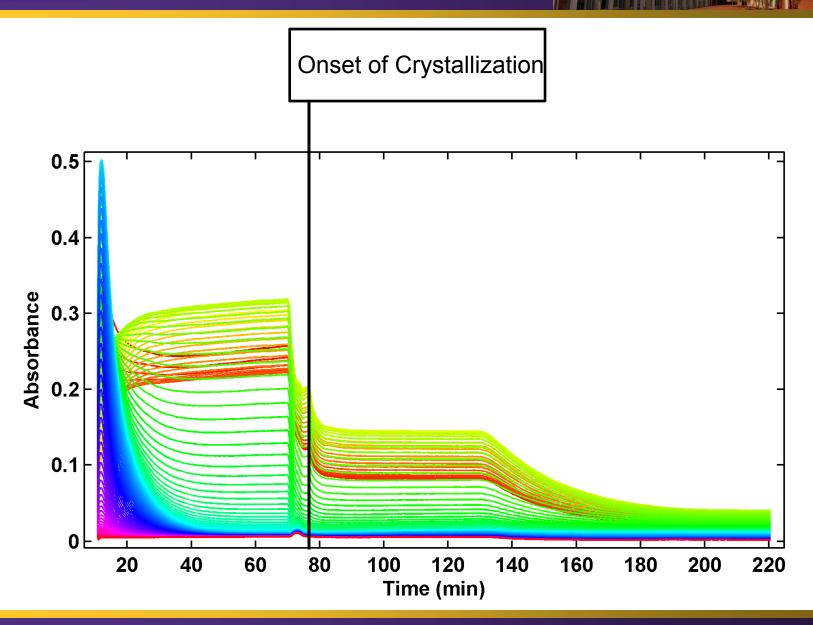


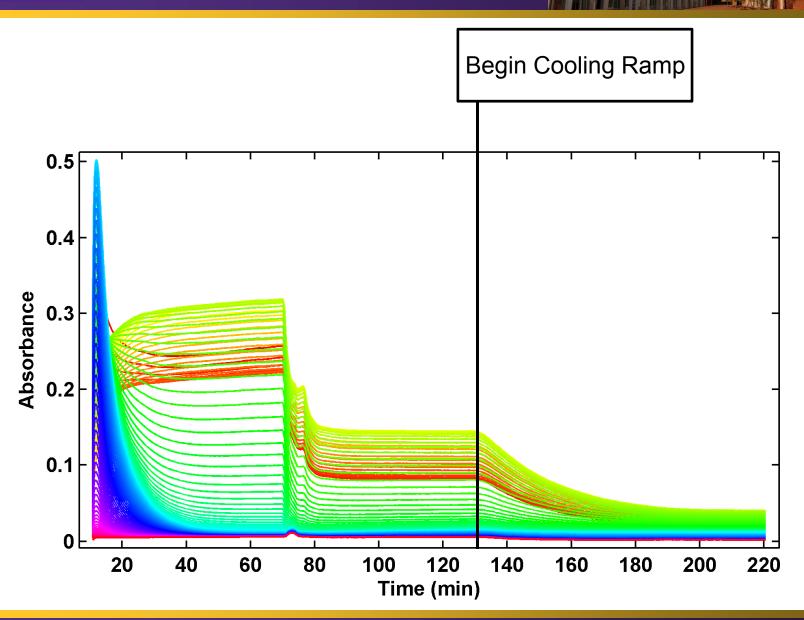


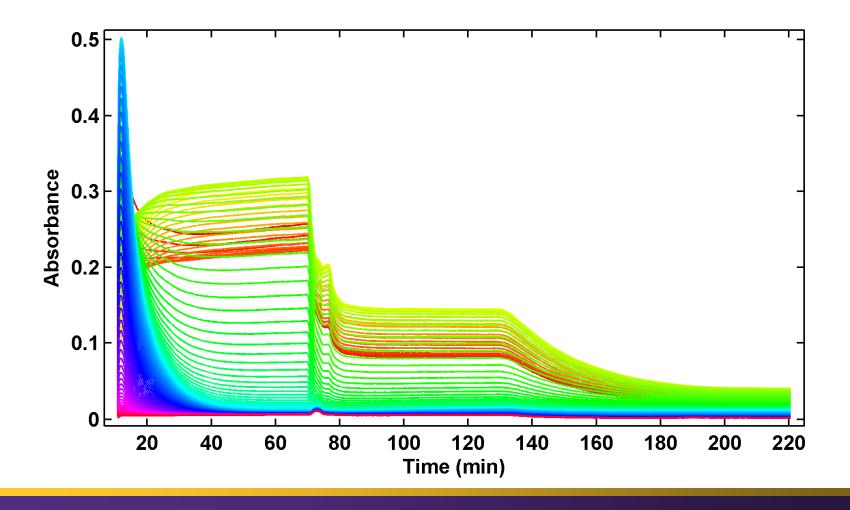










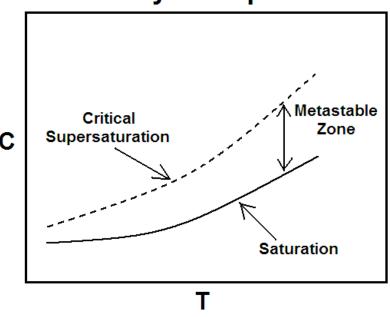




## **Saturation and Supersaturation**

- Considered relative to equilibrium solubility
- Super-saturation
  - "Driving force" of nucleation and crystal growth
  - Metastable
  - Generated by
    - Cooling
    - Anti-solvent addition
    - Solvent evaporation

### **Metastability of Supersaturation**





## **Differential Equations**

$$\frac{d[SA]_{solid}}{dt} = -r_d$$

$$\frac{d[ASAA]}{dt} = r_2 - \frac{dV}{dt} \frac{[ASAA]}{V}$$

$$\frac{d[SA]}{dt} = r_d - r_1 - \frac{dV}{dt} \frac{[SA]}{V}$$

$$\frac{d[ASA]}{dt} = r_1 - r_2 + r_3 - r_c - \frac{dV}{dt} \frac{[ASA]}{V}$$

$$\frac{d[AA]}{dt} = -r_1 - r_2 - r_4 - \frac{dV}{dt} \frac{[AA]}{V}$$

$$\frac{d[AA]}{dt} = -r_1 - r_2 - r_4 - \frac{dV}{dt} \frac{[AA]}{V} \qquad \frac{d[H_2O]}{dt} = -r_3 - r_4 + f \frac{[H_2O]_{in}}{V} - \frac{dV}{dt} \frac{[H_2O]}{V}$$

$$\frac{d[HA]}{dt} = r_1 + r_2 + r_3 + r_4 - \frac{dV}{dt} \frac{[HA]}{V} \quad \frac{d[ASA]_{\text{solid}}}{dt} = r_c$$

$$\frac{d[ASA]_{solid}}{dt} = r_c$$



## **Differential Equations**

$$\frac{d[SA]_{solid}}{dt} = -r_d$$

$$\frac{d[ASAA]}{dt} = r_2 - \frac{dV}{dt} \frac{[ASAA]}{V}$$

$$\frac{d[SA]}{dt} = r_d - r_1 - \frac{dV}{dt} \frac{[SA]}{V}$$

$$\frac{d[ASA]}{dt} = r_1 - r_2 + r_3 - r_c - \frac{dV}{dt} \frac{[ASA]}{V}$$

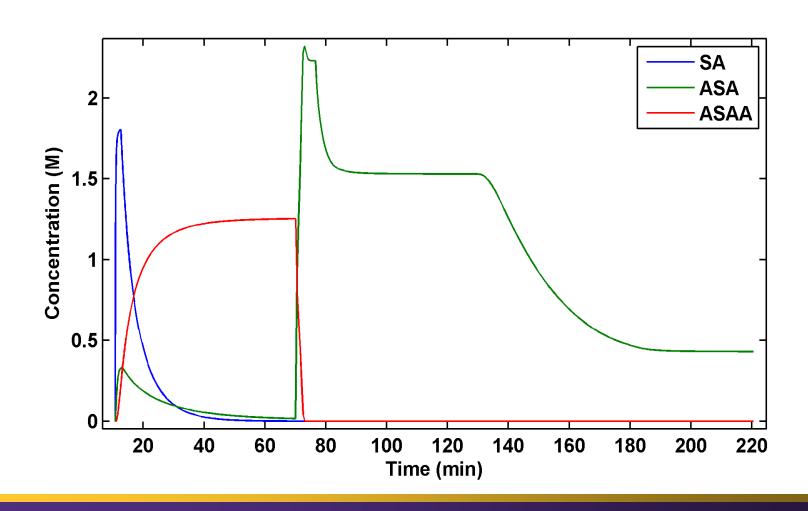
$$\frac{d[AA]}{dt} = -r_1 - r_2 - r_4 - \frac{dV}{dt} \frac{[AA]}{V}$$

$$\frac{d[AA]}{dt} = -r_1 - r_2 - r_4 - \frac{dV}{dt} \frac{[AA]}{V} \qquad \frac{d[H_2O]}{dt} = -r_3 - r_4 + f \frac{[H_2O]_{in}}{V} - \frac{dV}{dt} \frac{[H_2O]}{V}$$

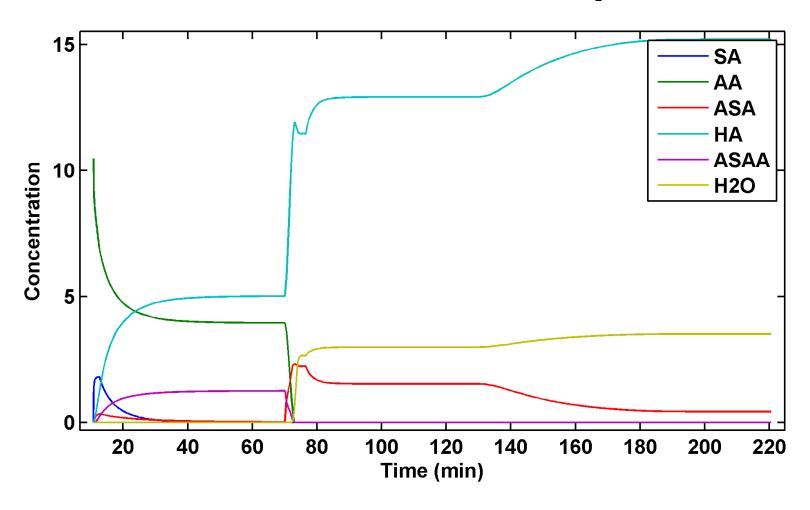
$$\frac{d[HA]}{dt} = r_1 + r_2 + r_3 + r_4 - \frac{dV}{dt} \frac{[HA]}{V} \quad \frac{d[ASA]_{\text{solid}}}{dt} = r_c$$

$$\frac{d[ASA]_{solid}}{dt} = r_c$$

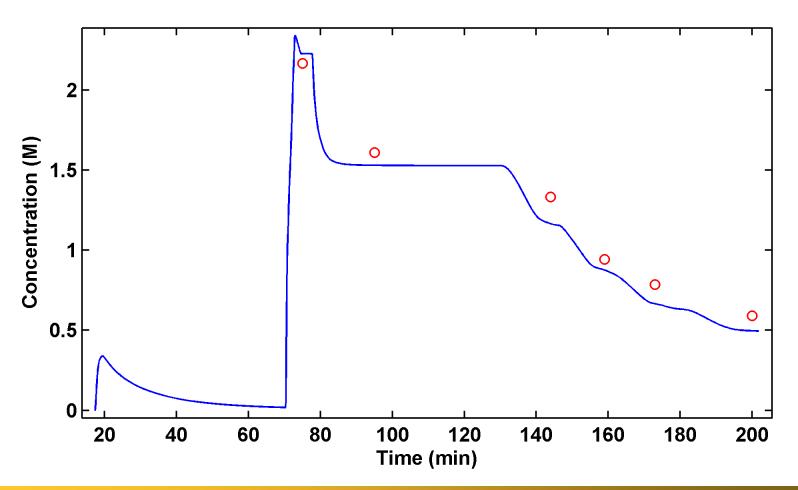
## **Concentration Profile of Active Species**



## **Concentration Profiles of All Species**



# Validation of ASA Concentration Profiles by HPLC – Preliminary results





# Project 3: modeling of sulfonylurea coupling reaction

- ☐ Develop a combined kinetic model for the reaction, dissolution and crystallization for the slurry-based sulfonylurea coupling reaction.
- ☐ Use NIR diffuse reflectance spectroscopy<sup>3</sup> and kinetic model for monitoring purpose, and to perform endpoint and fault detections.
- ☐ Use High Performance Liquid Chromatography (HPLC) samples taken from the reaction mixture to validate kinetic models





## **Sulfonyl Urea Coupling Reaction**

**CMBSI** 

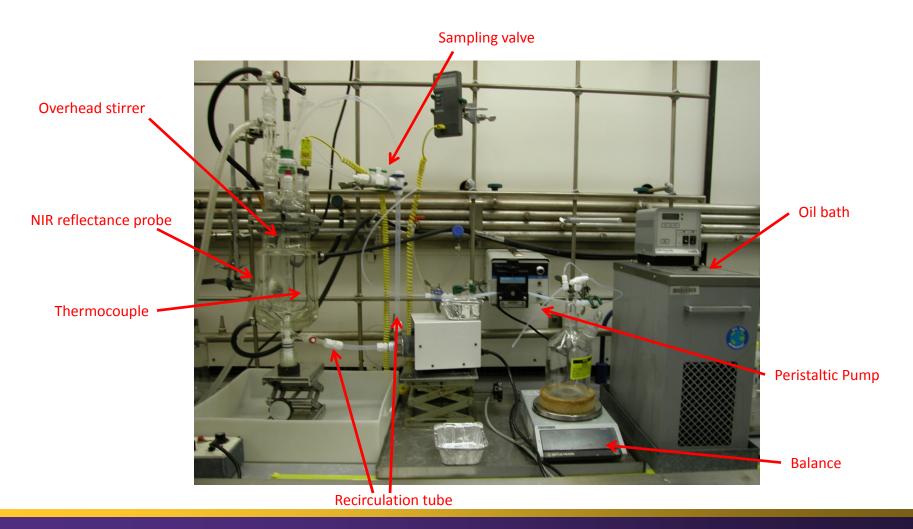
benzoic acid 2-[(Isocyanato)sulfonyl]methyl ester

A4098

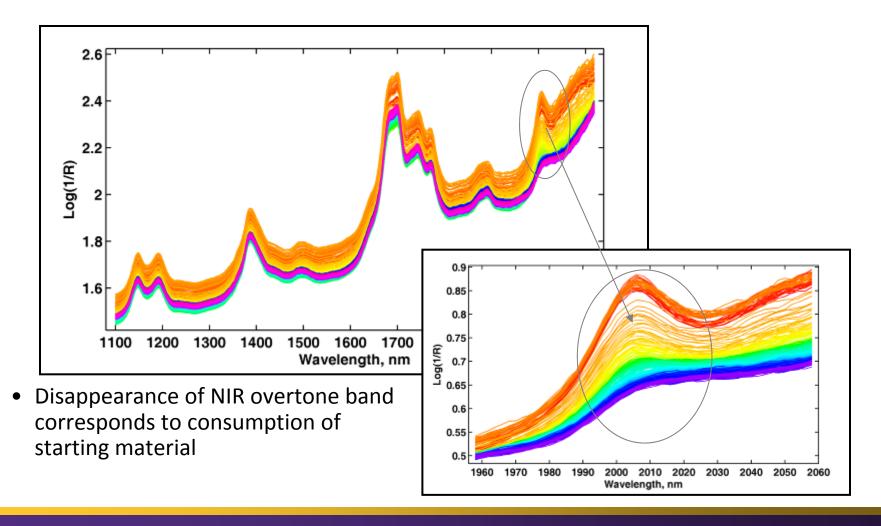
2-amino-4-methoxy-6-methyl-1,3,5triazine

metsulfuron methyl

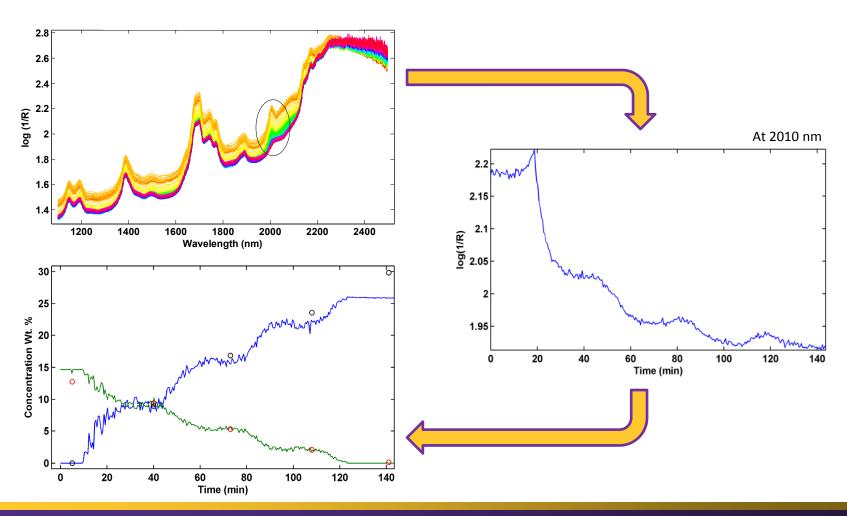
## **Apparatus setup at DuPont**



## Sample batch slurry system



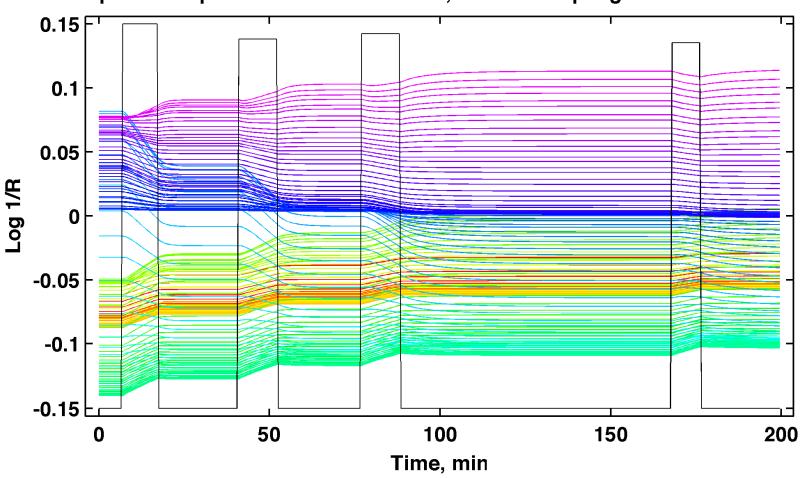






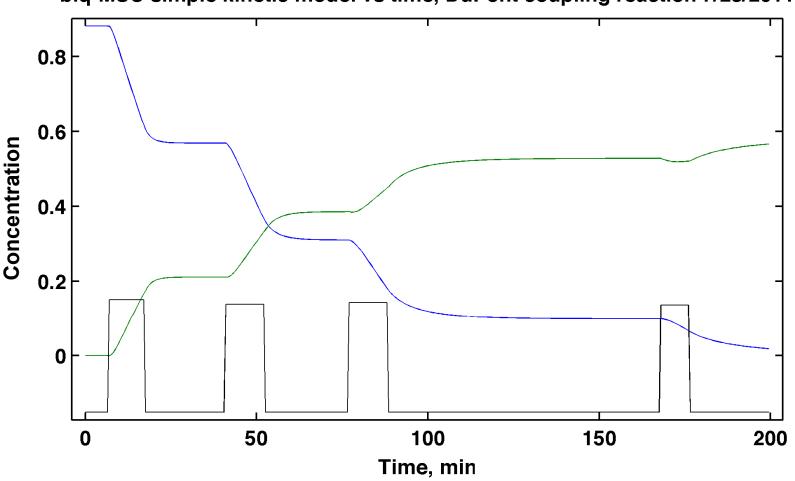
## **Modeling the Coupling Reaction**

blq-MSC simple kinetic model vs time, DuPont coupling reaction 7/28/2011



## **Coupling Reaction - Kinetic Fitting Results**

blq-MSC simple kinetic model vs time, DuPont coupling reaction 7/28/2011





### Acknowledgements

This research was supported by the National Science Foundation (NSF) under Grant Number CHE-0750287 for Grant Opportunities for Academic Liaison with Industry (GOALI)

This research was also sponsored by E.I. DuPont de Nemours and Co., Inc., Crop Protection Products and Engineering Technologies

### **GOALI**

Principal Investigators (PIs)

Dr. Mary Ellen McNally (Dupont)

Dr. Ron Hoffman (Dupont)

Dr. Paul Gemperline (ECU)

Dr. Julien Billeter

Chun Hsieh

**Chad Adkins** 

Ethan Chiappisi

Kristian Scott

Dr. Liguo Song (UT)

Dr. David S. Cho

Dr. Frank Chambers (OSU)

Consultant

Dr. Kelsey Cook (NSF)