

Process integration aspects in the design of biofuel processes

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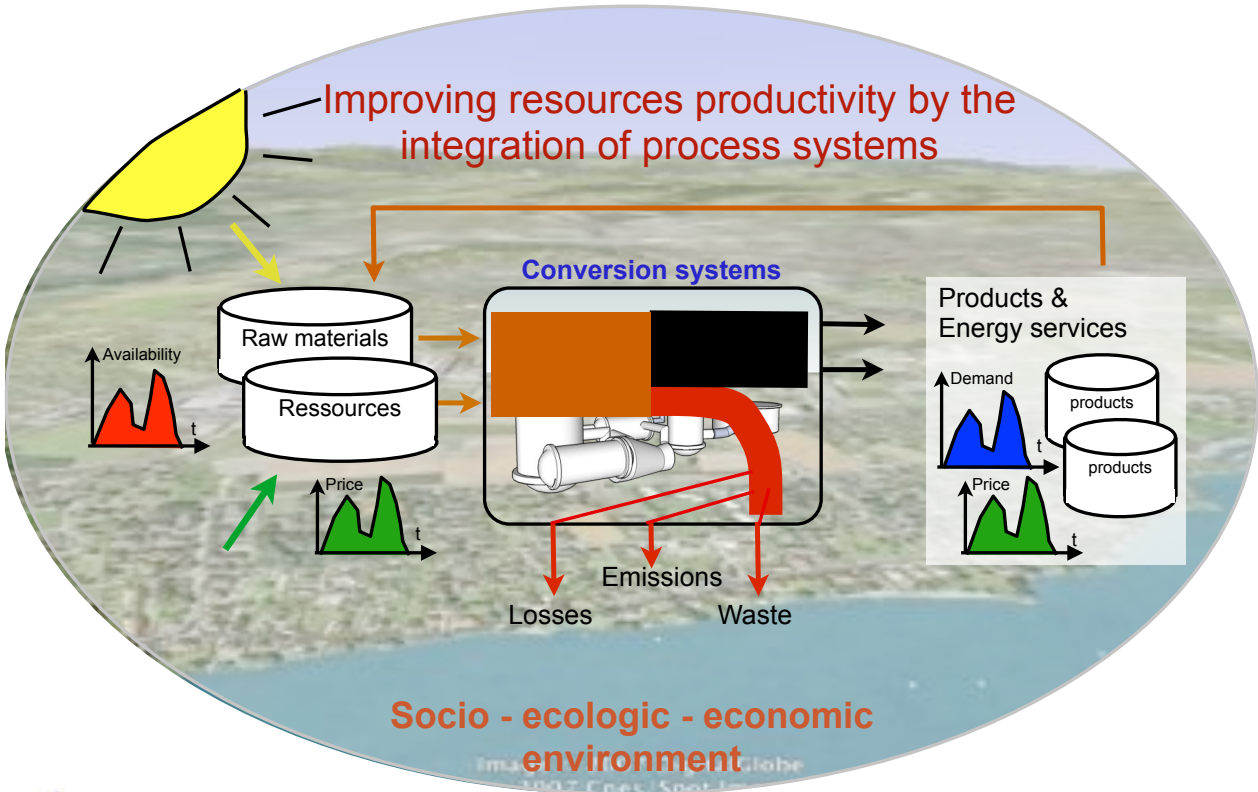
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<http://leni.epfl.ch/lenisystem>

Goals of my talk

1. Motivations
2. Process integration
3. Process system design method
4. Integrating Sustainability in design
5. Multi-objective optimization
6. System analysis
7. Computer aided design framework

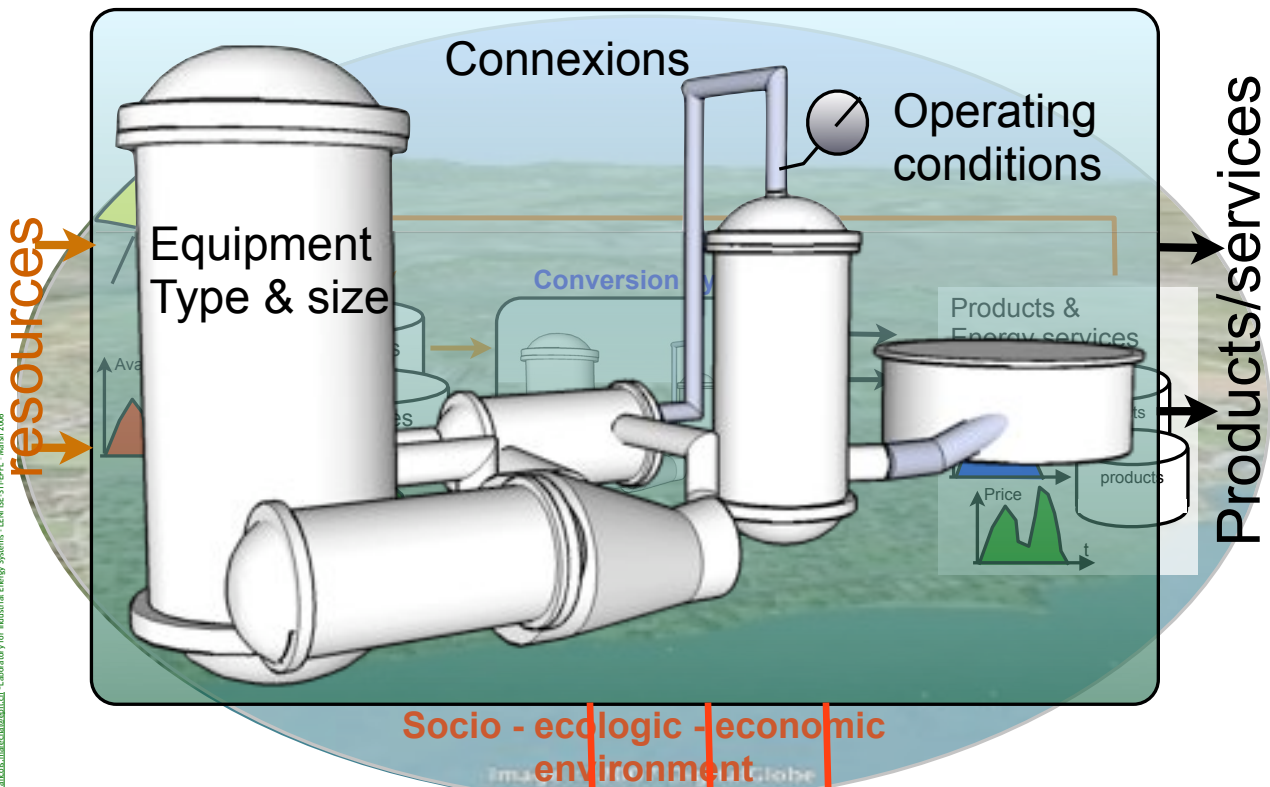
Energy Conversion Systems



fraunhofer.energiesystems_lab, laboratory for industrial Energy Systems - LENI GE-ST/EPT - March 2006



Energy system analysis and design



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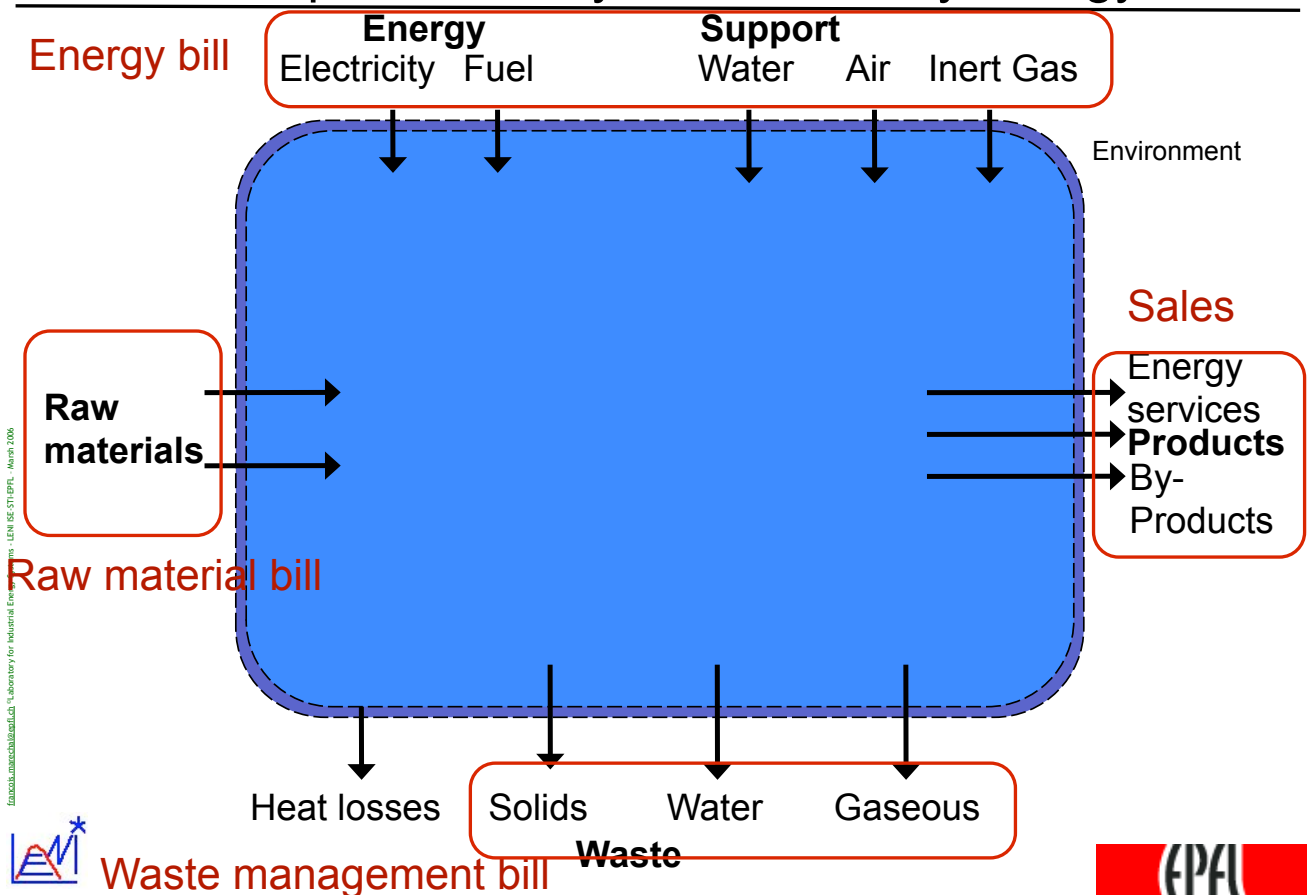
Process integration

Process integration is the engineering action of assembling process equipments to form a process system

- Understanding the interactions between the process units
 - Mass flows
 - Heat exchange
 - Coproduction
 - Waste management
- Adopt a system (holistic) vision
- Reach the "optimal" design
 - the one that makes sense for the engineer

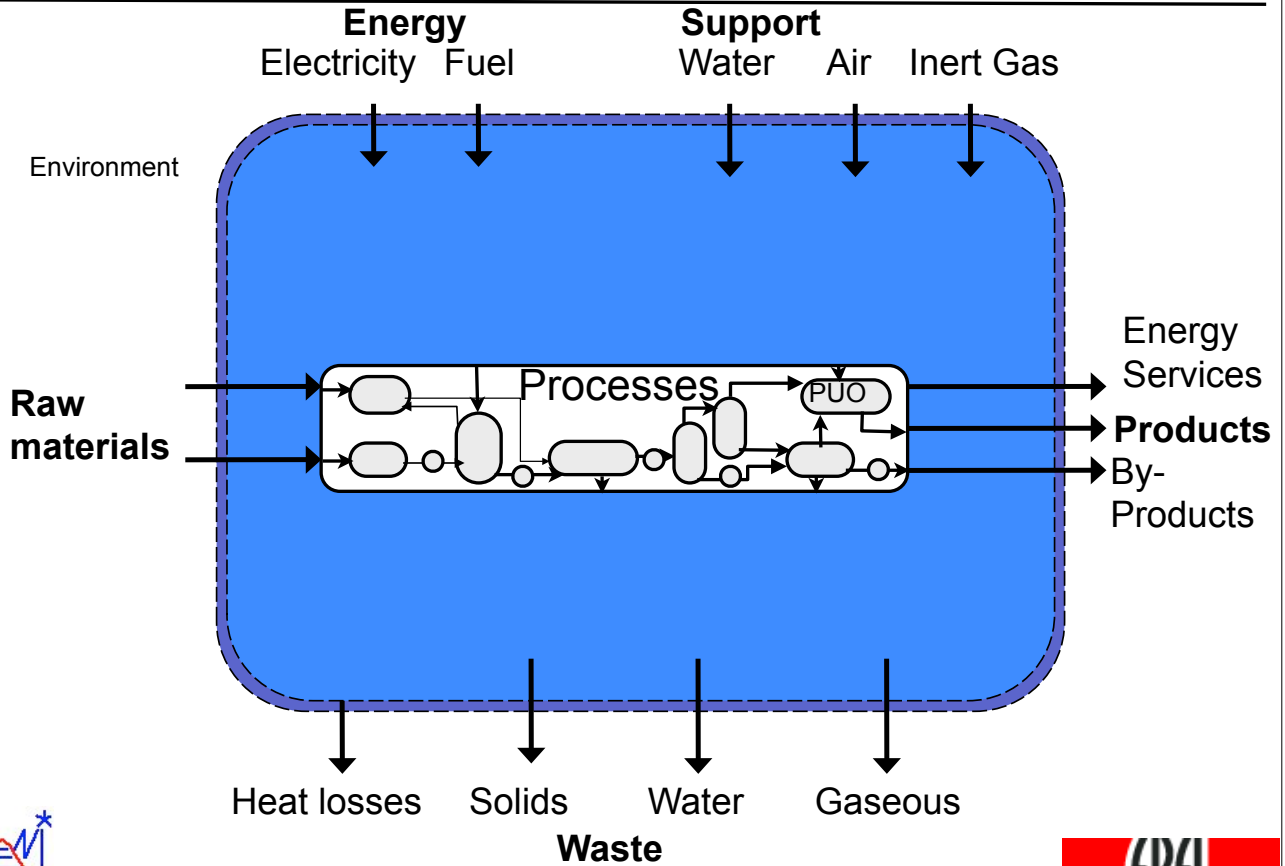
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Industrial processes system driven by energy



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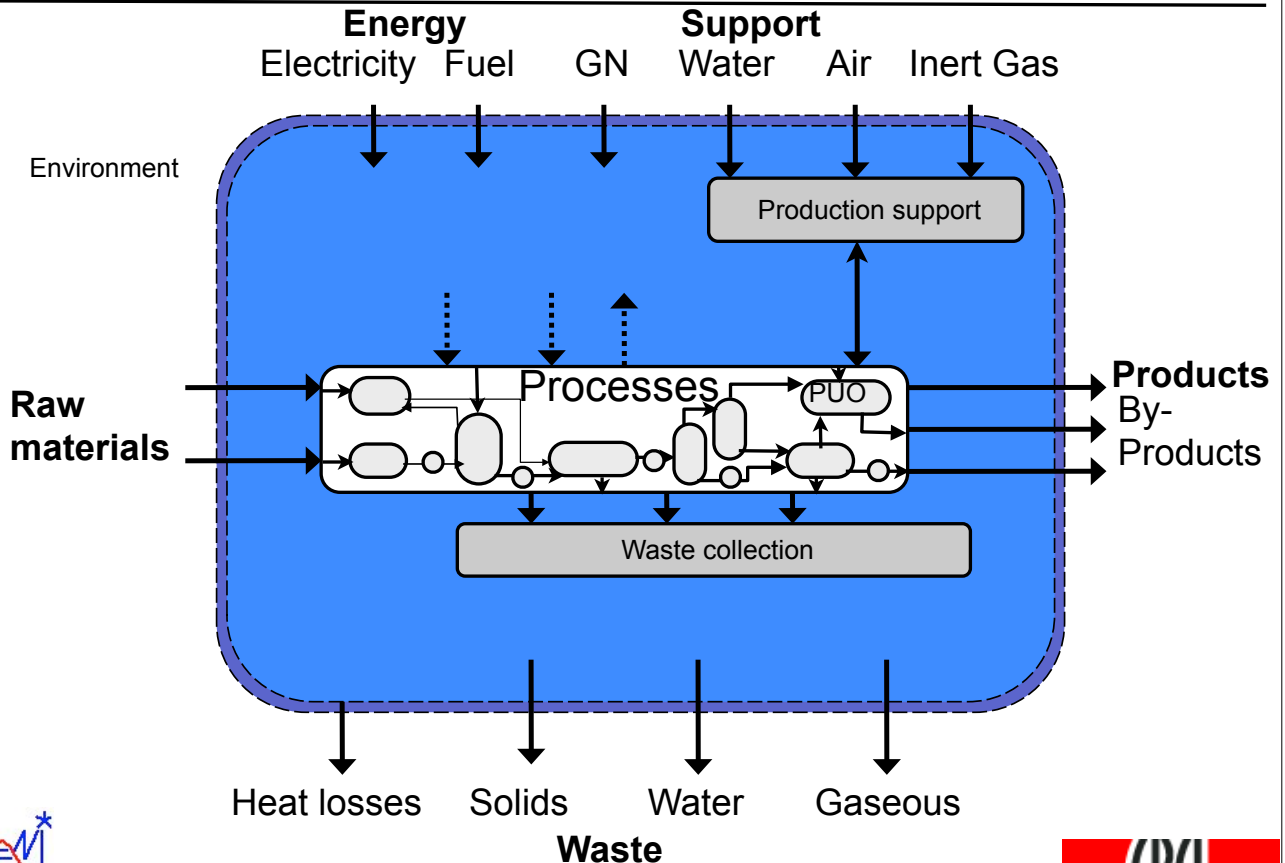
1. Reduce : analyse process requirement



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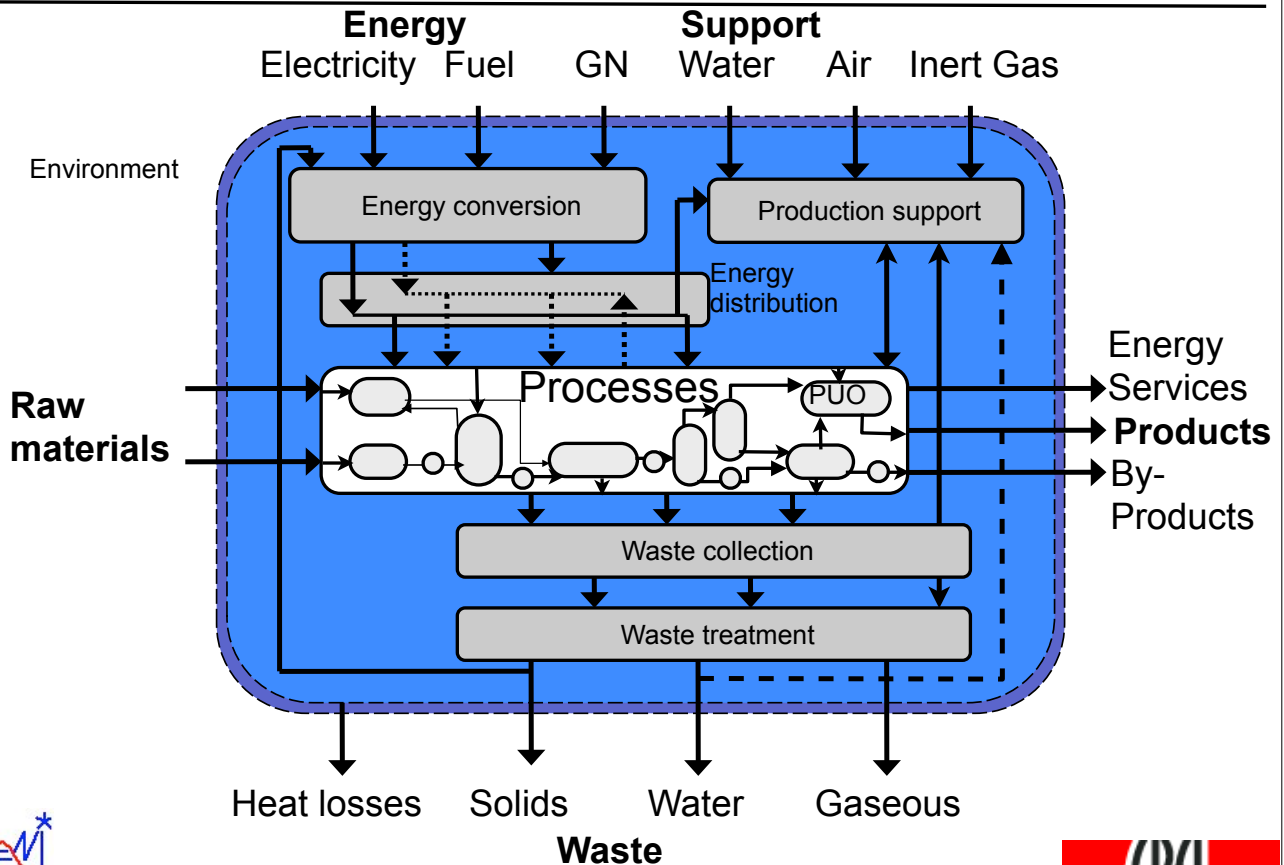
2. Recycling : heat and mass recovery



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3. Reuse : Optimal conversion and waste treatment



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3 R approach for process integration

1. Reduce

- Analyse processing requirements
- Analyse process units requirements
- System boundaries

Exergy analysis

Simulation/
optimisation

Pinchlight.epfl.ch

2. Recycle

- Mass recovery (production support)
- Heat recovery

Heat transfer & mass
requirement

Pinch analysis

3. Reuse

- Combined heat and power
- Heat pumping
- Waste conversion/valorisation
- Extend System boundaries

Optimization

Large scale
system
integration

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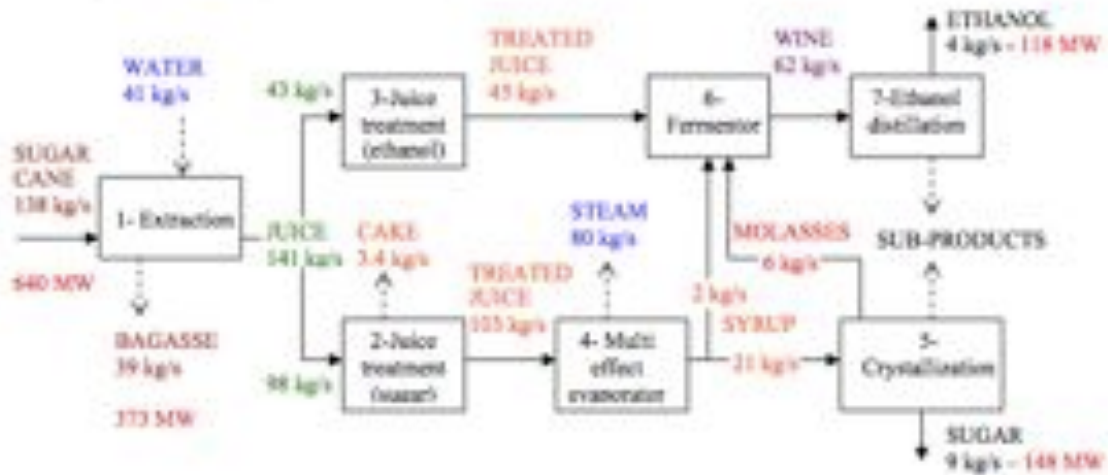


Example sugar-ethanol process

► Present consumption 138 MW of heat

- optimize the process operation
- Simulation of the process

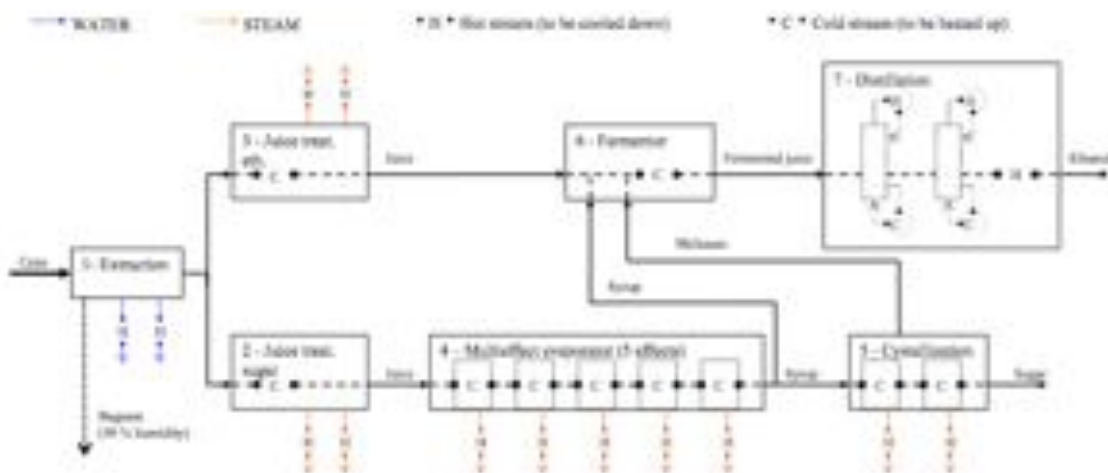
According to the data of the process found in a previous study by Ensinas A.V. et al. :



Morandin, Matteo, Andrea Toffolo, Andrea Lazzaretto, François Maréchal, Adriano V. Ensinas, and Silvia a. Nebra. "Synthesis and parameter optimization of a combined sugar and ethanol production process integrated with a CHP system." *Energy* 36, no. 6 (December 8, 2010): 3675-3690.

Process heat integration

► Define the hot streams and cold streams



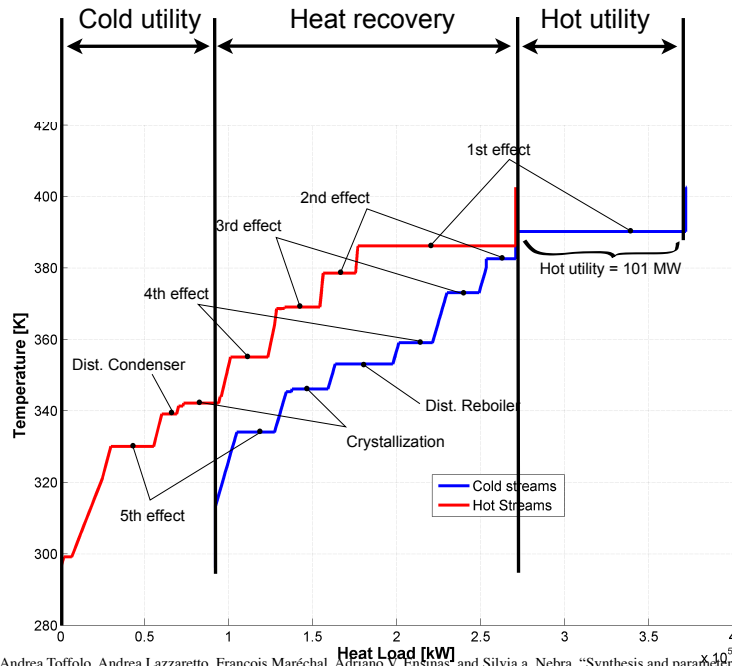
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Maximum heat recovery in the system

► Process composite curves

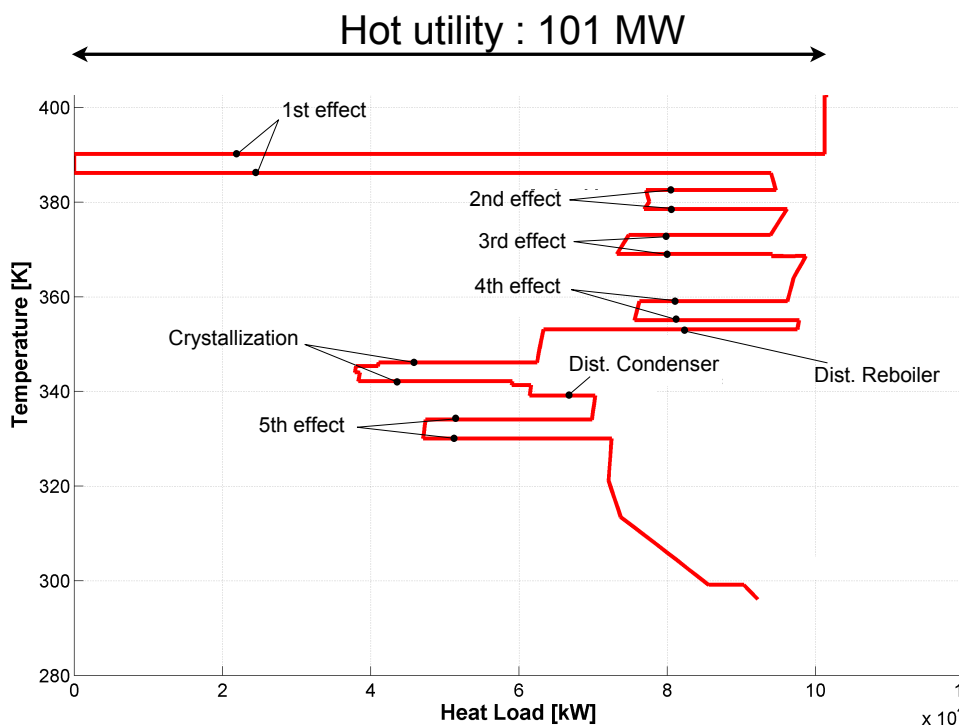
► Heat : 138 MW -> 101 MW (73%)

Ethanol 4.19 kg/s (118 MW), sugar 9.21 kg/s (148 MW)



Morandin, Matteo, Andrea Toffolo, Andrea Lazzaretto, François Maréchal, Adriano V. Ensinas, and Silvia a. Nebra. "Synthesis and parameter optimization of a combined sugar and ethanol production process integrated with a CHP system." *Energy* 36, no. 6 (December 8, 2010): 3675-3690.

Enthalpy temperature profile of the heat requirement

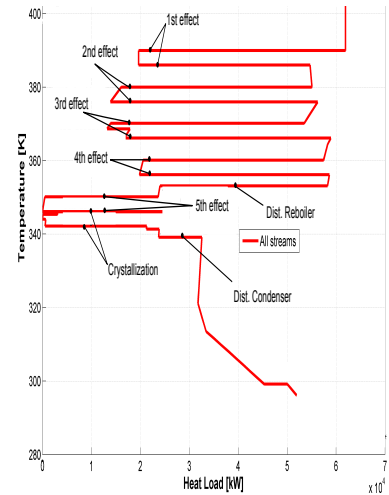
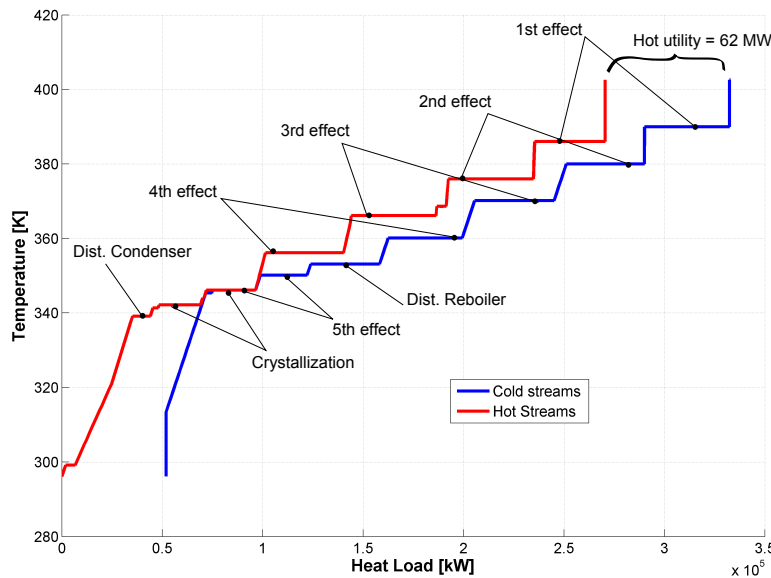


Ethanol 4.19 kg/s (118 MW), sugar 9.21 kg/s (148 MW)

Optimize the operating conditions of the process

► Changing the pressures of the evaporation

- Heat : 138 MW -> 101 MW (73%) -> 62 MW (45%)
- Ethanol 4.19 kg/s (118 MW), sugar 9.21 kg/s (148 MW)



Morandin, Matteo, Andrea Toffolo, Andrea Lazzaretto, François Maréchal, Adriano V. Ensinas, and Silvia a. Nebra. "Synthesis and parameter optimization of a combined sugar and ethanol production process integrated with a CHP system." *Energy* 36, no. 6 (December 8, 2010): 3675-3690.



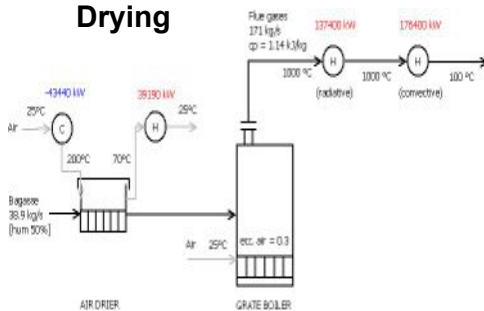
Optimizing the energy conversion

► Bagasse conversion (373 MW_{HHV} available)

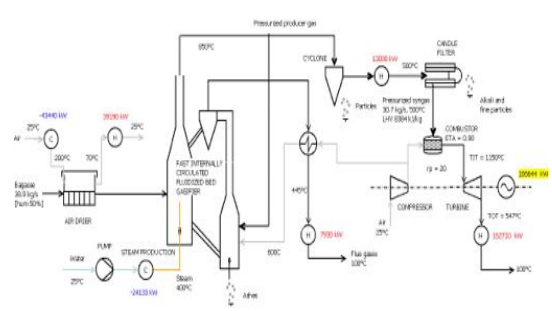
- Full potential ?

Combustion

Drying

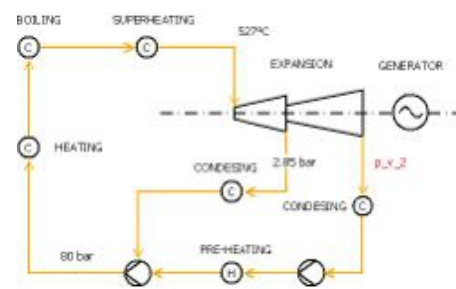


IGCC



Steam Cycle

Pressures to be optimized



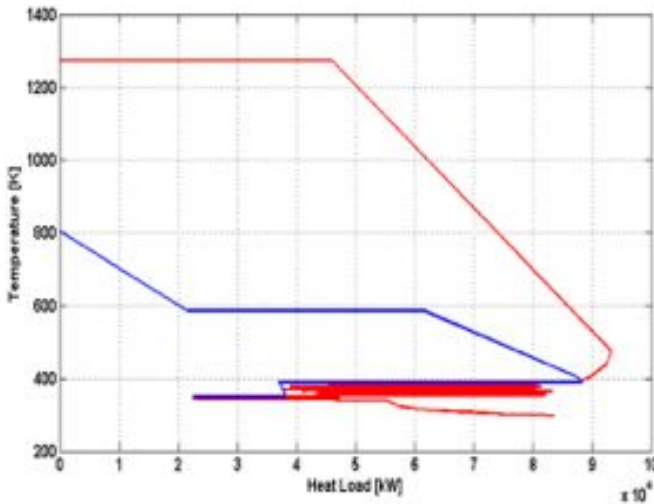
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Result : combustion + CHP

► 30% of bagasse used

► Marginal electricity production efficiency = 82 %



Case 1 results – CHP system 1
(30.2% bagasse combustion)

Rankine cycle net power =	22562 kW
HP turbine section power =	21593 kW
LP turbine section power =	1281 kW
Process power requirement =	15165 kW
Total site net power =	7397 kW
	(14.79 kWh/t _{case})
Cold utility requirement =	61416 kW
Bagasse input power =	89830 kW
Total site net thermal efficiency =	8.23 %

Ethanol 4.19 kg/s (118 MW), sugar 9.21 kg/s (148 MW)

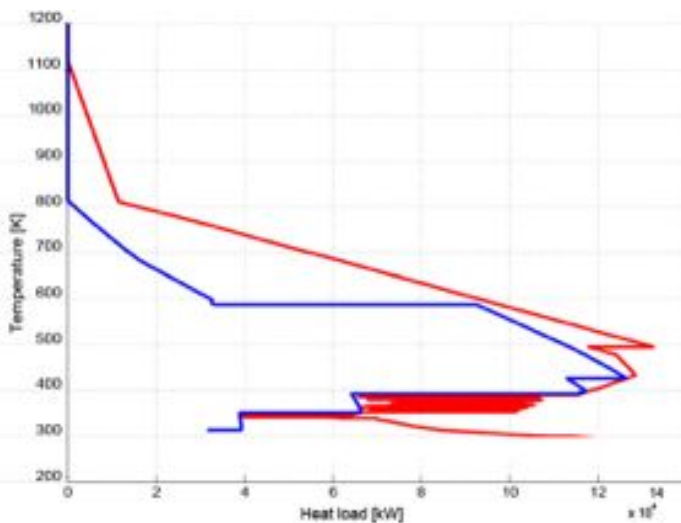
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Optimized system

► Total power produced : 137.8 MWe

► Marginal electricity production efficiency = 59 %



Case 1 results – advanced CHP system
(combined cycle + heat pump across crystallization temperature level)

Gas turbine net power =	106644 kW
Rankine cycle net power =	31196 kW
Process power requirement =	15165 kW
Total site net power =	122675 kW
	(245.35 kWh/t _{case})
Cold utility requirement =	87995 kW
Bagasse input power =	297450 kW
Total site net thermal efficiency =	41.24 %
Steam cycle pressures:	
p_{high} = 101 bar; p_{cstv1} = 5.32 bar; p_{cstv2} = 1.92 bar	
p_{cstv3} = 0.47 bar; p_{out} = 0.1 bar;	

Ethanol 4.19 kg/s (118 MW), sugar 9.21 kg/s (148 MW)

Morandin, Matteo, Andrea Toffolo, Andrea Lazzaretto, François Maréchal, Adriano V. Ensinas, and Silvia a. Nebra. "Synthesis and parameter optimization of a combined sugar and ethanol production process integrated with a CHP system." *Energy* 36, no. 6 (December 8, 2010): 3675-3690.



Process integration comparing solutions

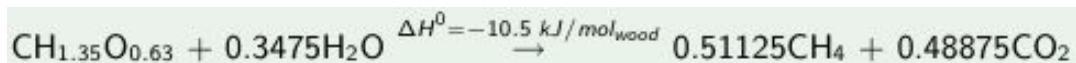
	Bagasse (MW)	Electricity (MW)	Marginal eff.
Combustion	89.8	22.6	82 %
CHP full	297.4	99	42 %
IGCC full + CHP + RMV	297.4	137.8	58.7 %

Ethanol 4.19 kg/s (118 MW), sugar 9.21 kg/s (148 MW)



Process system design : a larger perspective

- A Simple problem ?
Produce Synthetic Natural Gas from Wood

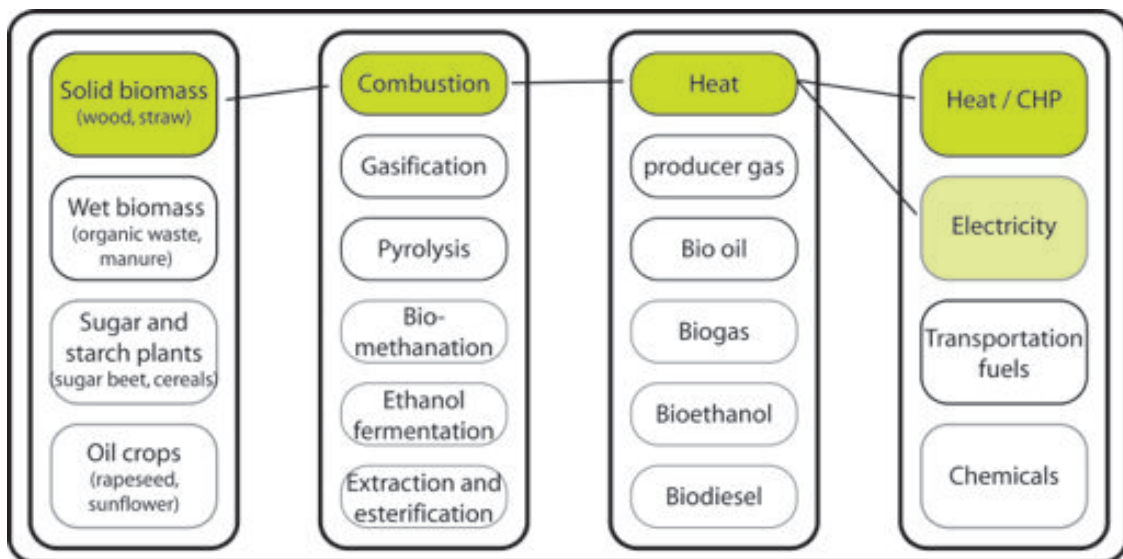


What are the options ?

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Biomass conversion Combustion

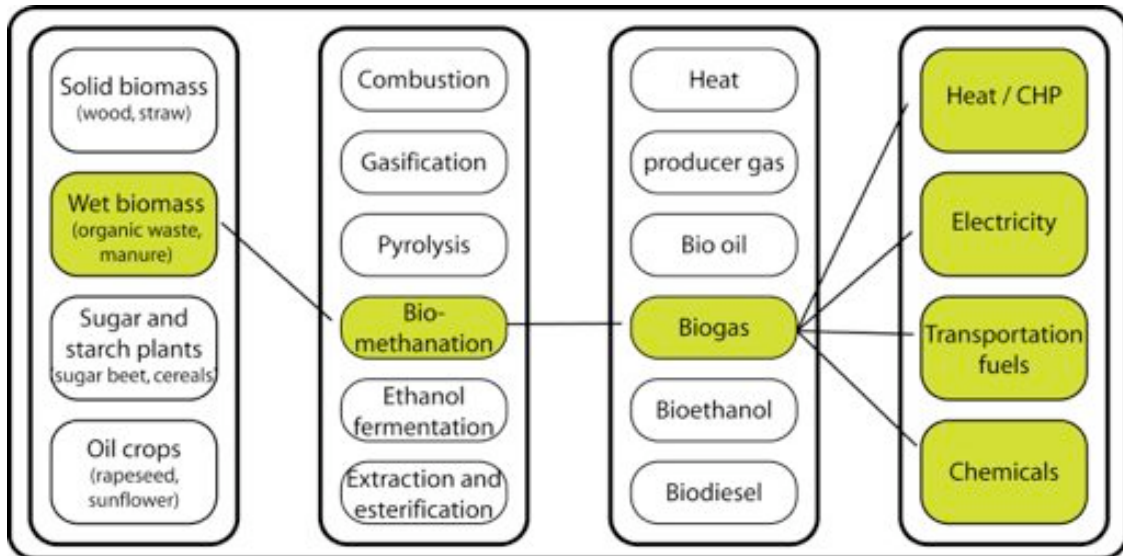


adapted from Chemical Engineering 10 (2006)



Biomass conversion

Biomethanation

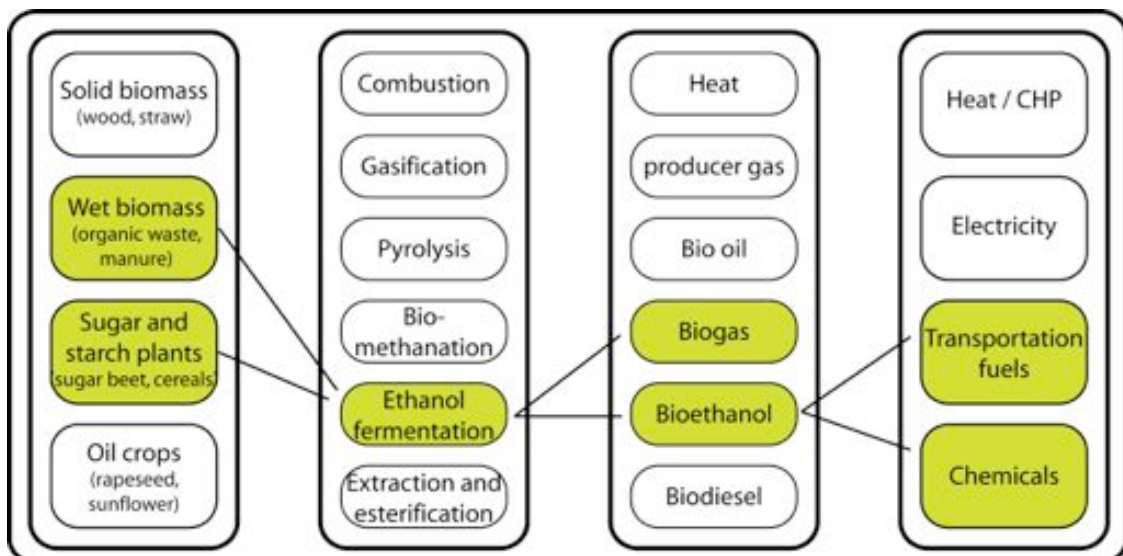


adapted from Chemical Engineering 10 (2006)



Biomass conversion

Ethanol fermentation

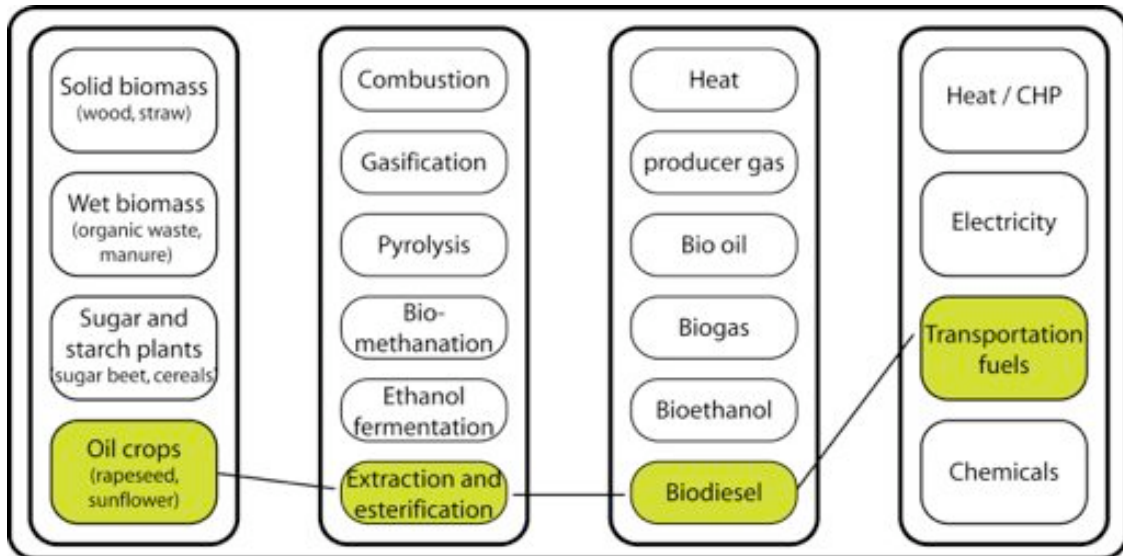


adapted from Chemical Engineering 10 (2006)



Biomass conversion

Transesterification

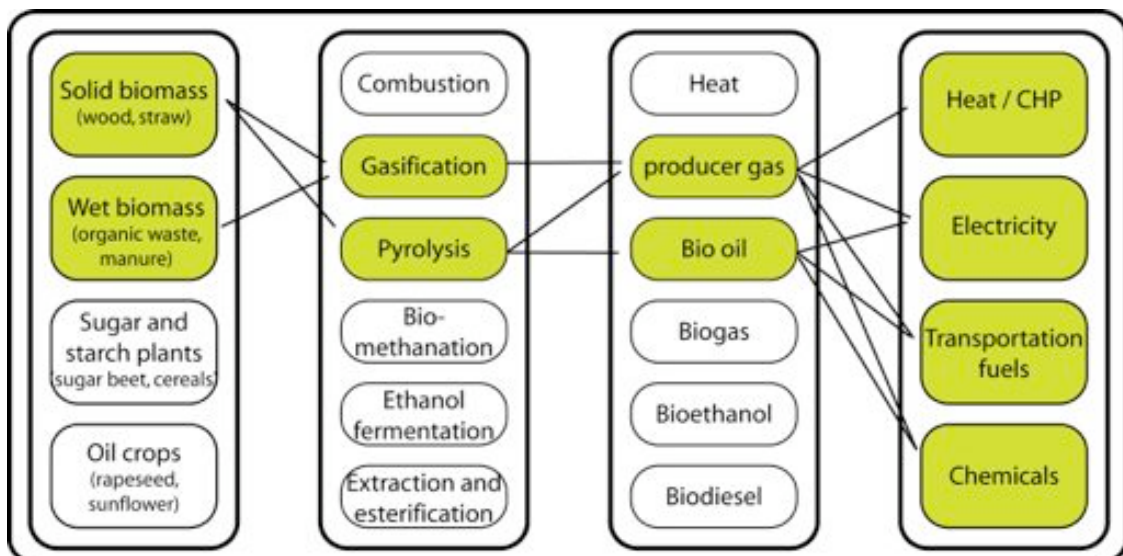


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Biomass conversion

Thermochemical routes



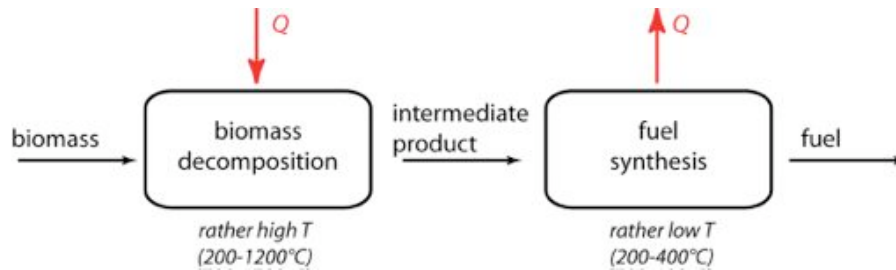
adapted from Chemical Engineering 10 (2006)



Thermochemical biomass conversion

Principle of conventional thermochemical routes

Thermochemical biomass to fuel reforming proceeds typically in two (or more) reaction steps:



- gasification
 - pyrolysis
- non-condensable/
condensable
substances
(H₂, CO, CO₂, H₂O,
CH₄, C_xH_y,
char, tars)
- methanation
 - FT synthesis
 - DME synthesis
 - methanol synthesis

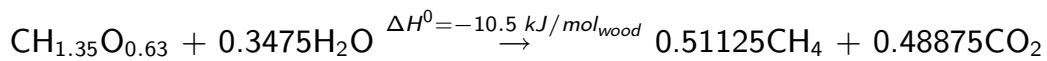
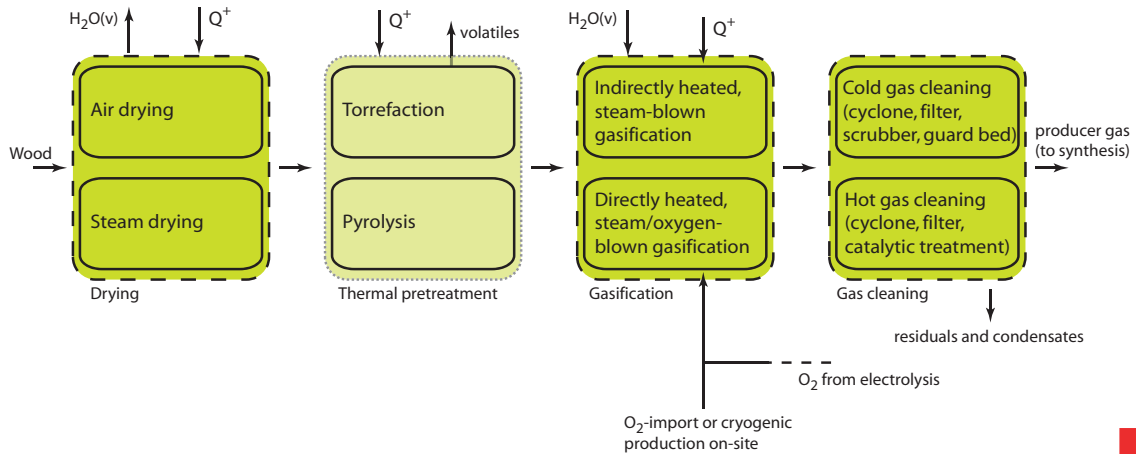


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What are the processing options ?

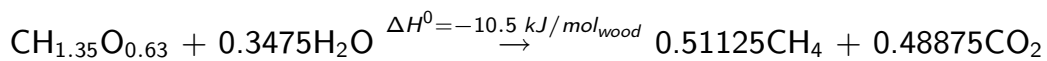
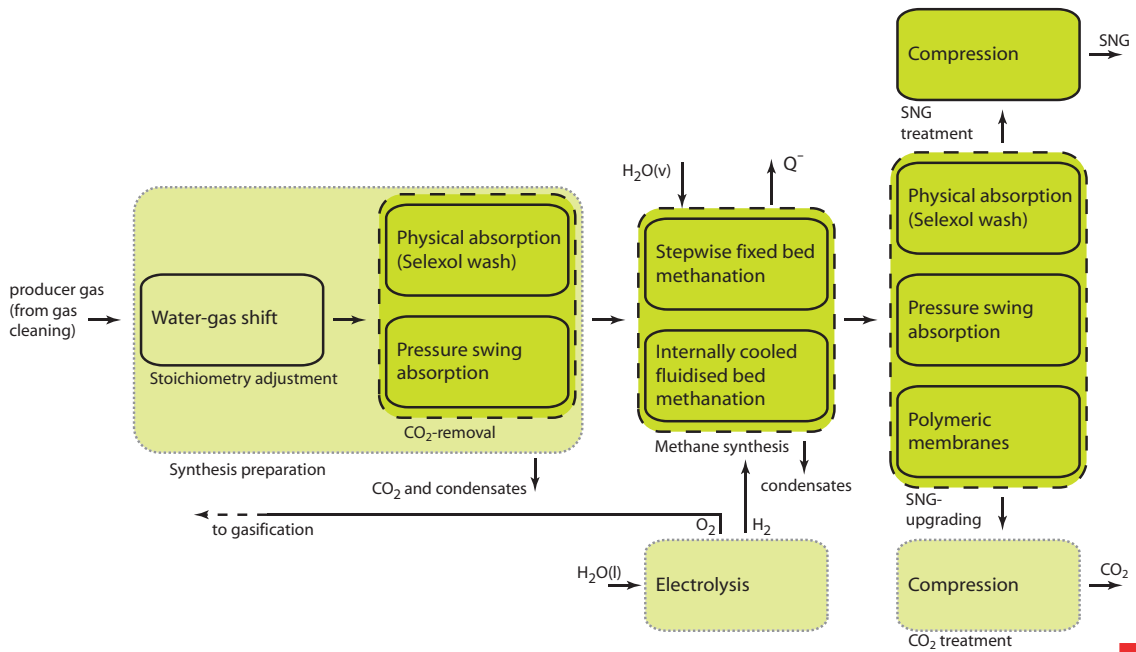
Block flow superstructure

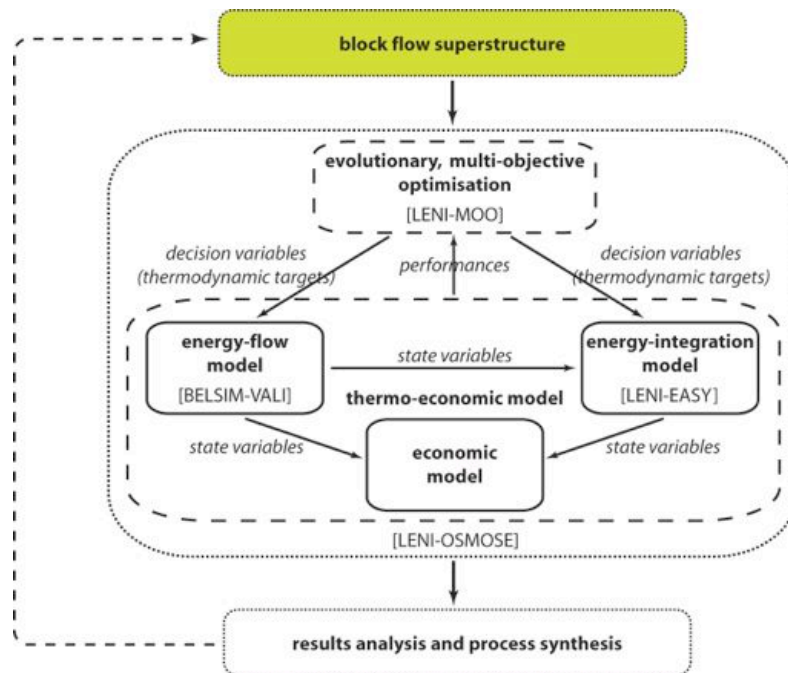
Conventional route (gasification & methanation): decomposition



Block flow superstructure

Conventional route (gasification & methanation): synthesis





Process unit models?

Simple models but not too simple ...

Levels of detail

Developed for the design

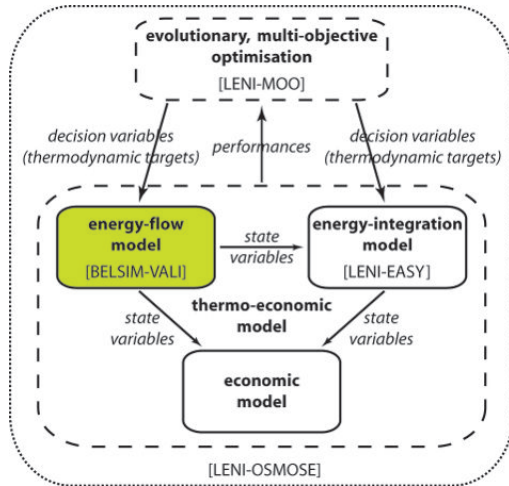
i.e allow for thermo-economic evaluations

- Flowsheet calculation
- Unit size optimization
- Cost estimation
- Environmental impact assessment

Flowsheet generation (1)

Energy-flow model

Calculation of the thermodynamic transformations in the process units



use of

- conservation principles
- model equations

to determine

- power requirements
- heat transfer requirements
 - T-h profile of hot and cold streams

Interconnections ?

Mass interactions -> flow superstructure

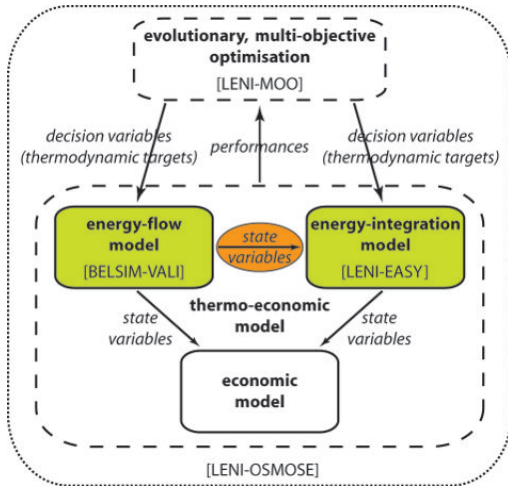
Heat interactions -> Heat cascade

Energy balance -> energy conversion integration

Flowsheet generation (1)

Energy-flow model

Calculation of the thermodynamic transformations in the process units



use of

- conservation principles
- model equations

to determine

- power requirements
- heat transfer requirements
 - T-h profile of hot and cold streams



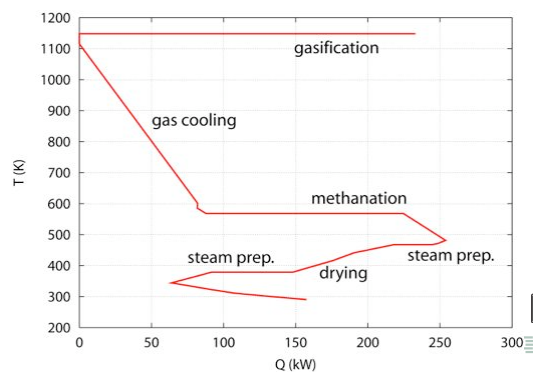
Flowsheet generation (2)

Energy-integration model

How to satisfy the MER?



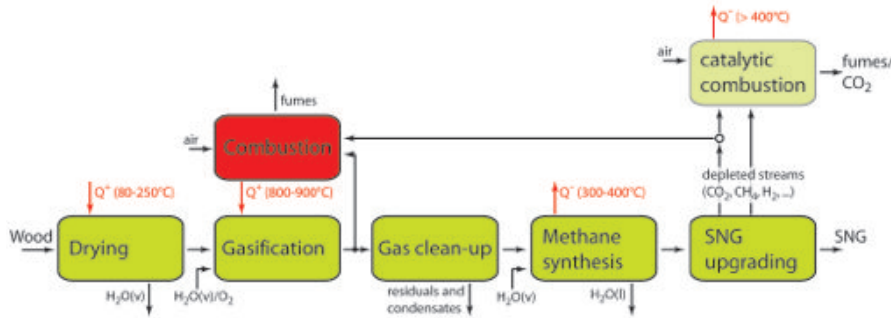
- MER of crude production



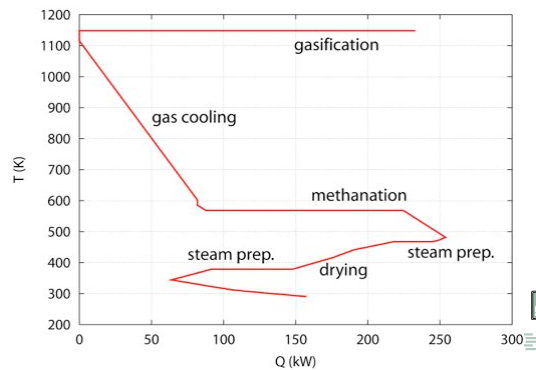
Flowsheet generation (2)

Energy-integration model

How to satisfy the MER?



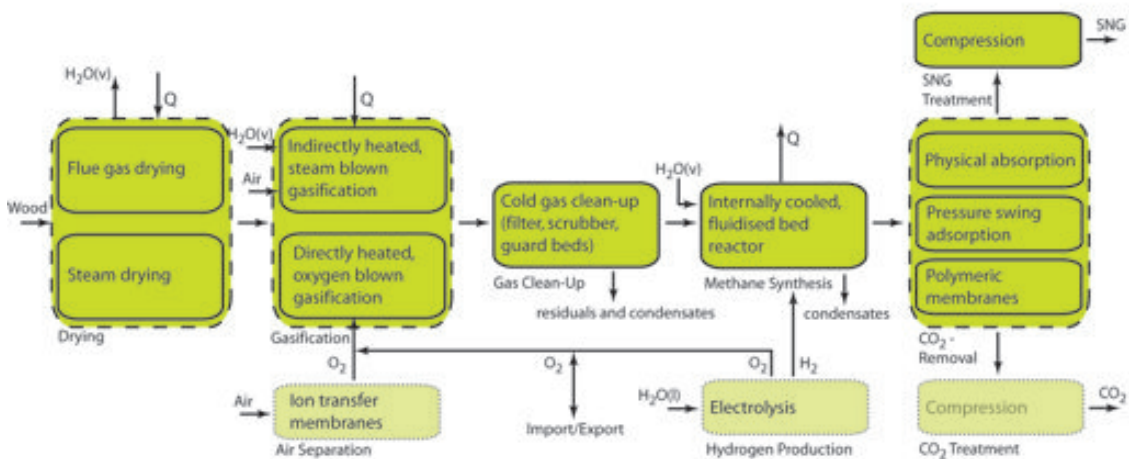
- MER of crude production
- hot utility: combustion
- fuel choice?
 - waste streams
 - intermediate products



Flowsheet generation (2)

Energy-integration model

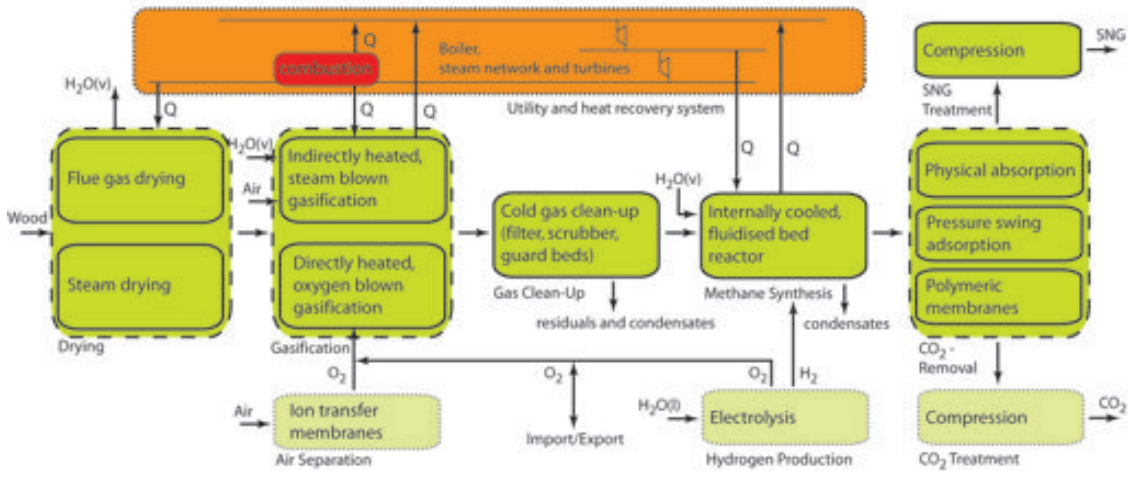
Integrating heat recovery technologies in the superstructure



Flowsheet generation (2)

Energy-integration model

Integrating heat recovery technologies in the superstructure



Flowsheet generation (2)

Energy-integration model

Math. problem formulation: MILP programming...

$$\min_{\dot{R}_r, y_s, f_s} \sum_{s=1}^{n_s} \dot{L}_s = \sum_{s=1}^{n_s} (f_s \cdot (\sum_{f=1}^{n_{fuel,s}} \dot{m}_{f,s} \Delta k_f^0 + \dot{w}_s^+ - \sum_{r=1}^{n_r} (\dot{e}_{q,s,r}^-) \Delta T_{min} - \dot{w}_s^-))$$

subject to:

- 1 Existence of subsystem s :

$$f_{min_s} y_s \leq f_s \leq f_{max_s} y_s$$

$$y_s \in \{0, 1\}, \forall s = 1, \dots, n_s$$

- 2 Heat balance of the temperature intervals r :

$$\sum_{s=1}^{n_s} f_s \dot{q}_{s,r}^- + \dot{R}_{r+1} - \dot{R}_r = 0$$

$$\dot{R}_r \geq 0 \quad \forall r = 1, \dots, n_r$$

- 3 Overall heat balance:

$$\dot{R}_1 = 0, \quad \dot{R}_{n_r+1} = 0$$

Flowsheet generation (2)

Energy-integration model

Math. problem formulation: MILP programming...

$$\min_{\dot{R}_r, y_s, f_s} \sum_{s=1}^{n_s} \dot{L}_s = \sum_{s=1}^{n_s} \left(f_s \cdot \left(\sum_{f=1}^{n_{fuel,s}} \dot{m}_{f,s} \Delta k_f^0 + \dot{w}_s^+ - \sum_{r=1}^{n_r} (\dot{e}_{q,s,r}^-) \Delta T_{min} - \dot{w}_s^- \right) \right)$$

subject to:

- 4** Electricity consumption:

$$\sum_{s=1}^{n_s} f_s \dot{w}_s^- + \epsilon_d \dot{W}^+ - \dot{W}_c \geq 0 \quad \dot{W}^+ \geq 0$$

- 5** Electricity exportation:

$$\sum_{s=1}^{n_s} f_s \dot{w}_s^- + \epsilon_d \dot{W}^+ - \frac{\dot{W}^-}{\epsilon_g} - \dot{W}_c = 0 \quad \dot{W}^+ \geq 0, \dot{W}^- \geq 0$$

- 6** Superstructure model:

$$A f = b$$



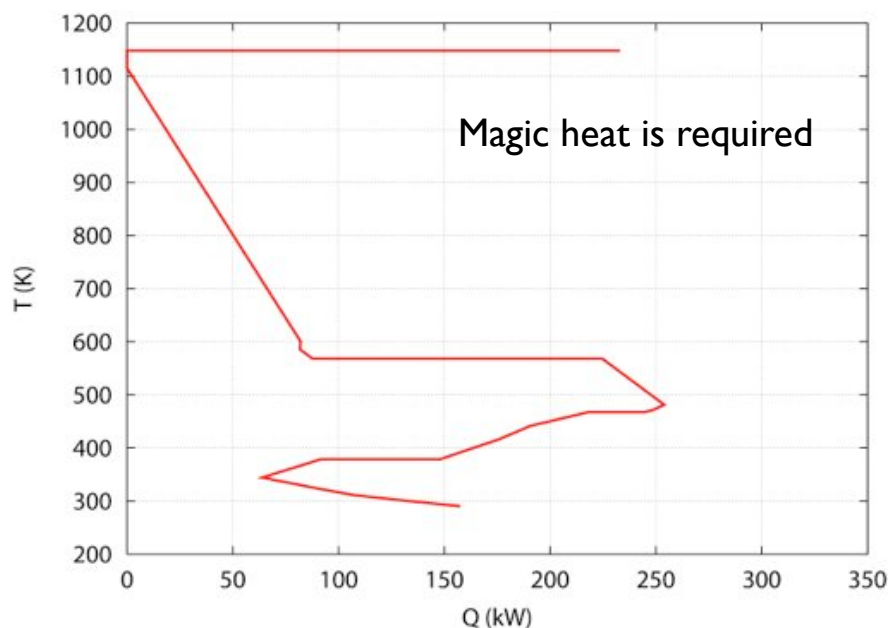
$$A : (n_s \times n_s), f, b : (n_s \times 1)$$

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Flowsheet generation (2)

Energy-integration model

MILP resolution: from MER ...

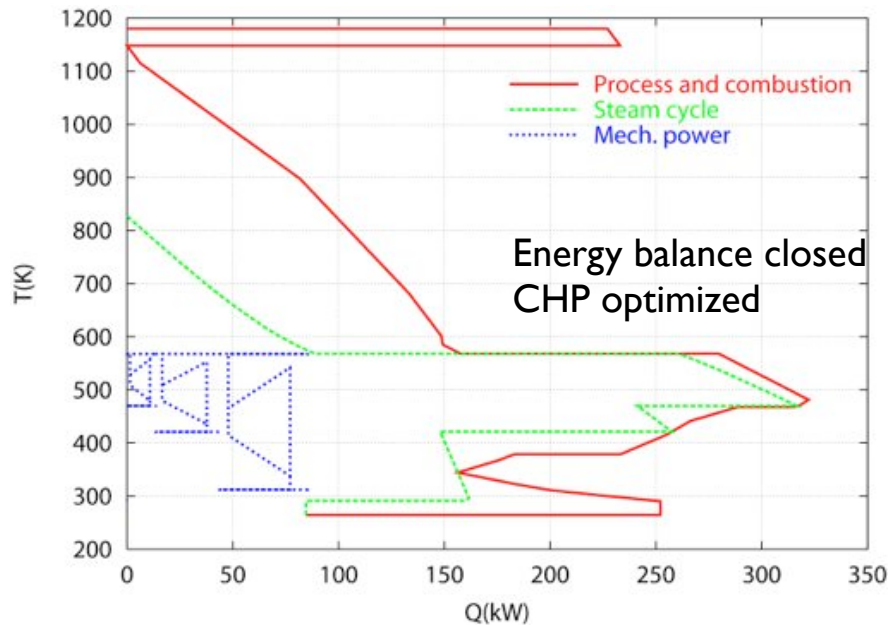


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Flowsheet generation (2)

Energy-integration model

MILP resolution: ... to an integrated solution



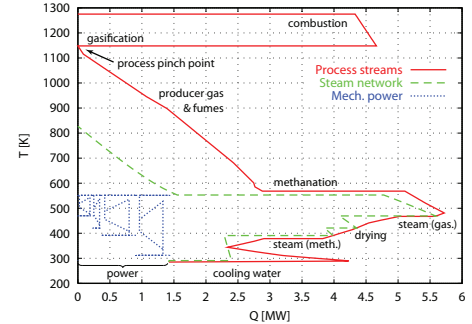
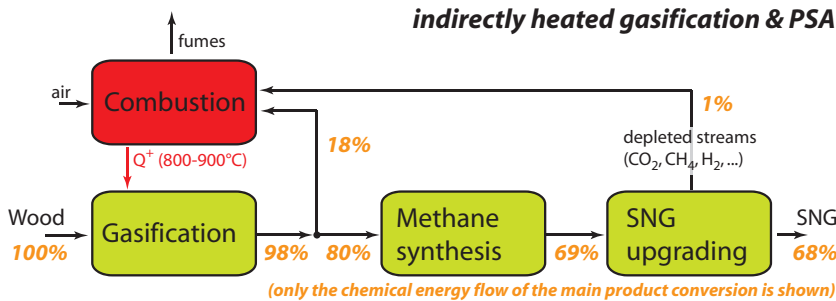
Process performances ?

Thermodynamic performances
System balanced

Process performance

conventional SNG

Some (non-optimised) scenarios for conventional SNG production:



input: 20 MW_{th,wood}

		(base)	FICFB (torr)	FICFB (pM)	FICFB (pM, SA)	CFB (pGM)	CFB (pGM, hot)
Consumption	Wood	100%	100%	100%	100%	100%	100%
	Biodiesel	1.8%	1.6%	1.8%	1.8%	0.1%	-
	Electricity	-	0.5%	-	-	0.9%	-
Production	SNG	67.7%	72.1%	67.5%	67.8%	74.0%	74.0%
	Electricity	2.9%	-	2.6%	3.3%	-	1.6%
Overall efficiency		69.4%	70.7%	68.8%	69.8%	73.2%	75.6%



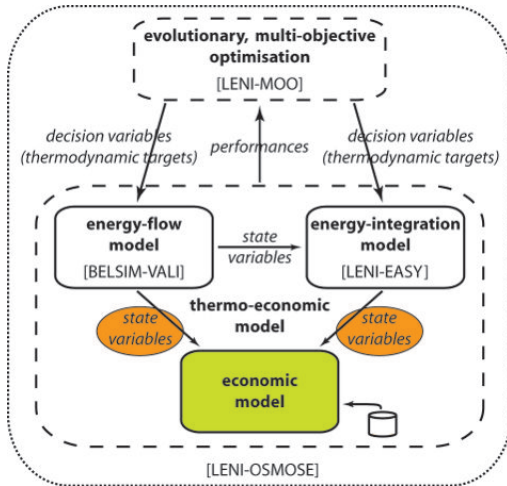
Process system design

Process performances ?

- Economics :
- Investment
 - Design equipments
 - Sizes
 - Cost estimations
- Incomes

Equipment sizing and costing

Meeting the thermodynamic design target for the flowsheet



Rate the equipment with

- design heuristics
- pilot plant data

Assessment of investment cost considering the specific operating conditions

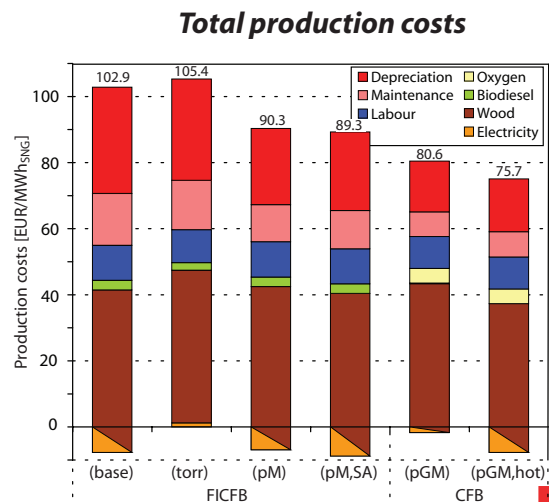
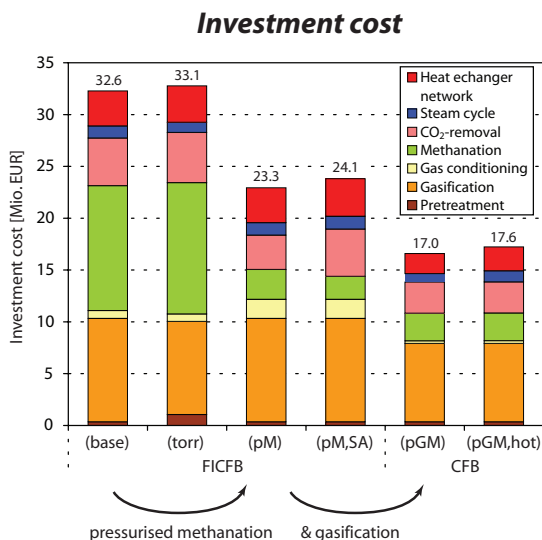
$$C_{GR} = f(T, p, size(T, p, \dots))$$

(1) EPFL
ÉCOLE POLYTECHNIQUE
FÉDÉRALE DE LAUSANNE



Process performance conventional SNG

Some (non-optimised) scenarios for conventional SNG production:



EPFL
ÉCOLE POLYTECHNIQUE
FÉDÉRALE DE LAUSANNE

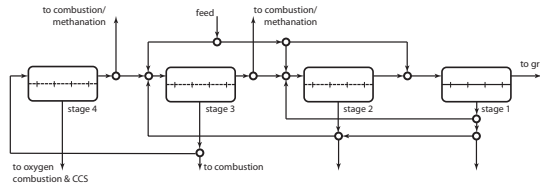


Technology integration example

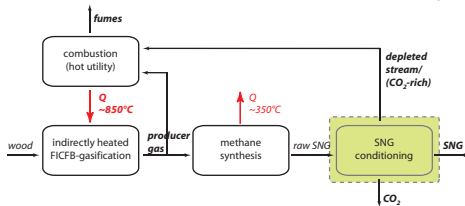
Gas upgrading by membrane

Membrane system upgrading superstructure

CH₄/CO₂ separation

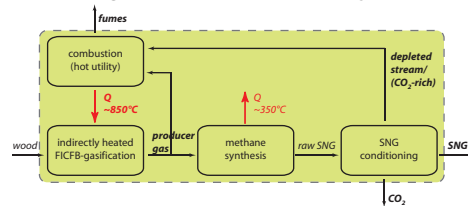


"isolated": separation only



- Maximise SNG recovery
- Permeate stream is lost

"integrated": total system



- Permeate stream valorised
- Overall system performance



Technology integration example

Gas upgrading by membrane

Results : Isolated vs integrated design

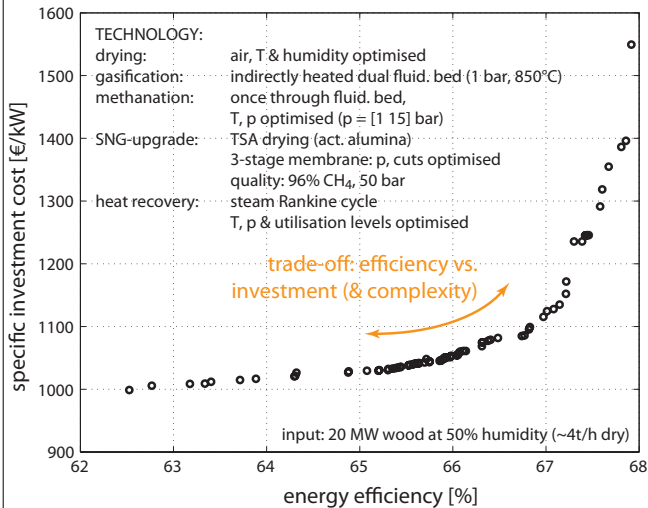
system		isolated	integrated	overshoot
		3-stage CC	3-stage, 1 rec	
r_{SNG}^{sep}	%	93.2	84.1	+ 10.8%
e_{spec}^{sep}	kW _{el} /MW _{th,in}	76.9	55.9	+ 37.6%
$\tilde{c}_{CO_2,p}$	%	86.6	79.9	+ 8.4%
$\tilde{c}_{H_2,p}$	%	10.3	9.4	+ 9.6%
$\tilde{c}_{CH_4,p}$	%	3.0	10.4	- 71.2%
A	m ²	4675	2928	+ 59.7%
C_I^{sep}	M€	5.7	4.1	+ 39.0%
ϵ^{sep}	%	86.6	80.7	+ 8.8%
ϵ_{cg}	%	69.0	63.5	+ 8.7%
ϵ	%	66.0	66.2	- 0.3%
C_I	M€	30.7	29.9	+ 2.7%
C_P	€/MWh	105.6	102.9	+ 2.6%



Thermo-economic optimisation

Trade-offs: efficiency and scale vs. investment

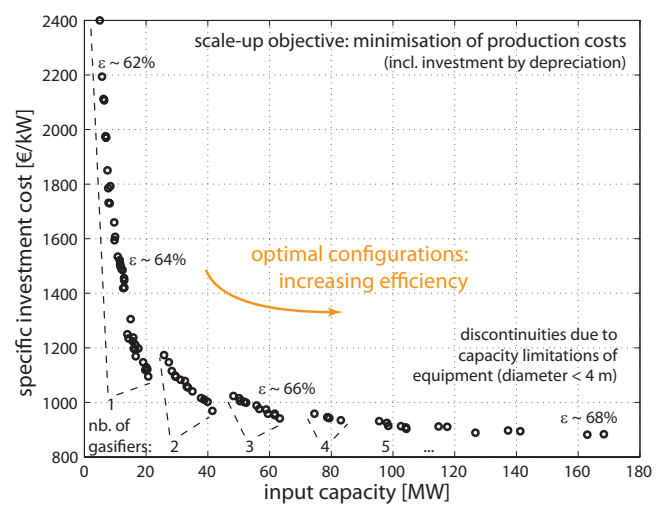
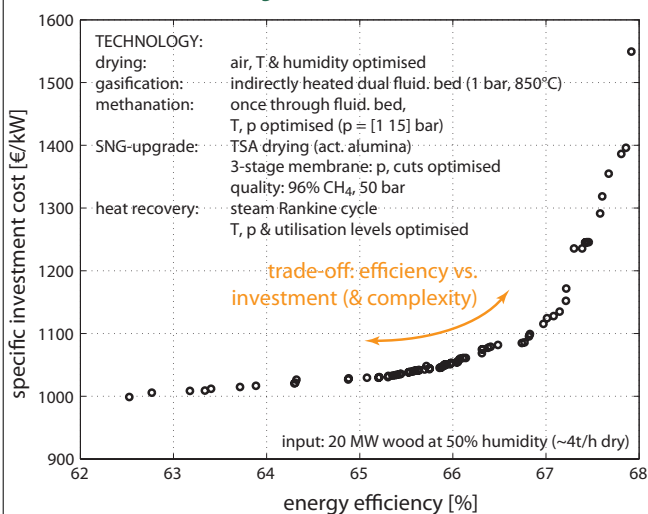
Efficiency vs. investment:



Thermo-economic optimisation

Trade-offs: efficiency and scale vs. investment

Efficiency vs. investment and optimal scale-up:

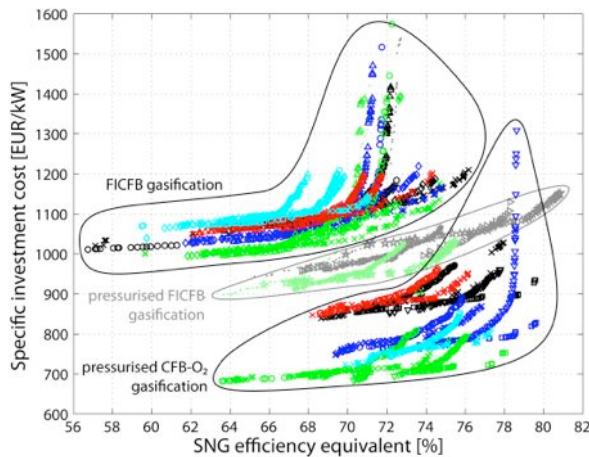


Some results

Comparing technologies and processes

comprehensive way of comparing design options in an uncertain world

Thermo-economic Pareto front (cost vs efficiency):



Gasification:

- FICFB
 - air drying
 - △ + torrefaction
 - × steam drying
 - ◇ + torrefaction
- pressurised FICFB
 - air drying
 - air drying, gas turbine
 - ▷ steam drying, gas turbine
 - ★ + hot gas cleaning
- CFB-O₂
 - air drying
 - ▽ + hot gas cleaning
 - × steam drying
 - + hot gas cleaning

Separation:

- PSA
 - downstream
 - upstream of methanation
- Phys. abs.
 - downstream
 - upstream of methanation
- Membranes
 - downstream of methanation

→ *The best solution is the pressurised directly heated gasifier*



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LENI Systems

Sustainability and process integration

- Process integration of supply chains
 - What is the size of the process wrt to biomass availability ?
 - How to minimize the environmental impact ?

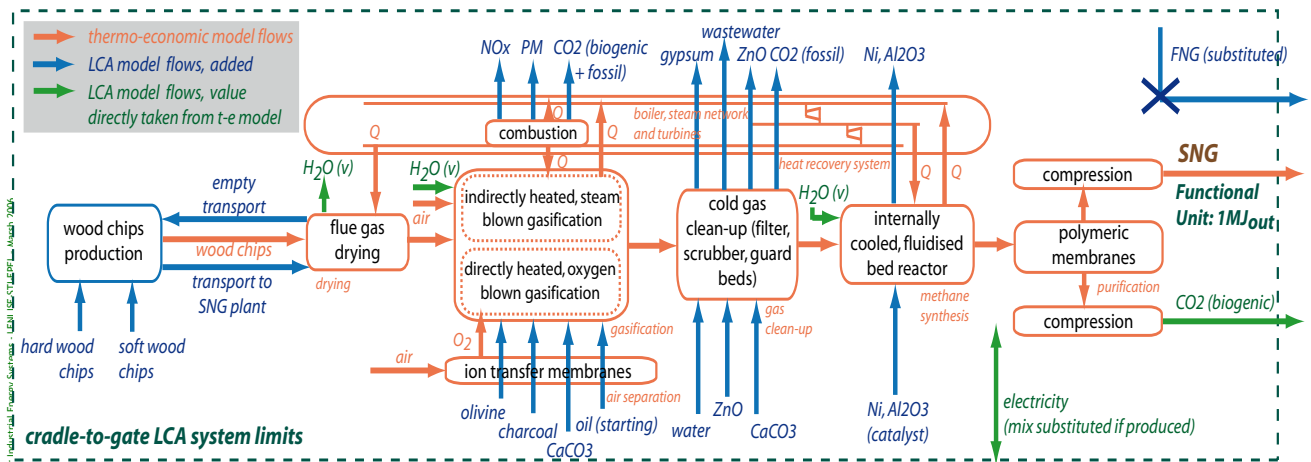
François Maréchal@epfl.ch, "Laboratory for Industrial Energy Systems - LENI (E-517) EPFL - March 2006"



Environmental Process performance indicators

Identification of Life Cycle Inventory elements

- Process superstructure, extended with LCI



➔ use of ecoinvent emission database (1) for each LCI element, to take into account off-site emissions

(1) <http://www.ecoinvent.org>



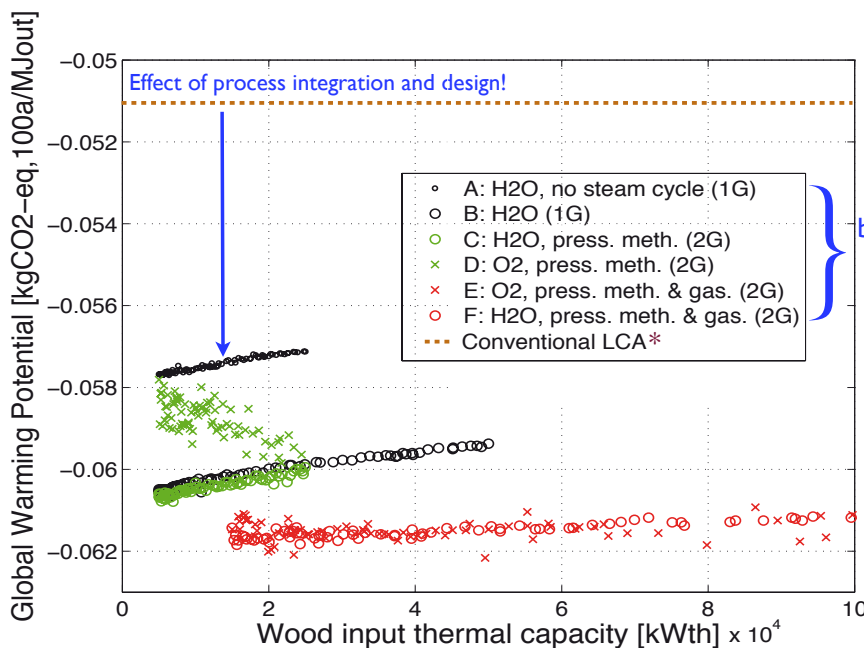
Gerber, L. et al., 2010 Comp & Chem Eng., 1405-1410



Integration of LCIA in the methodology

Perspective: plant scale-up vs. biomass logistics

The biomass Logistics has an influence on the plant impact



* LCI data taken from Felder et al, and adapted to system limits

biomass logistics impact model

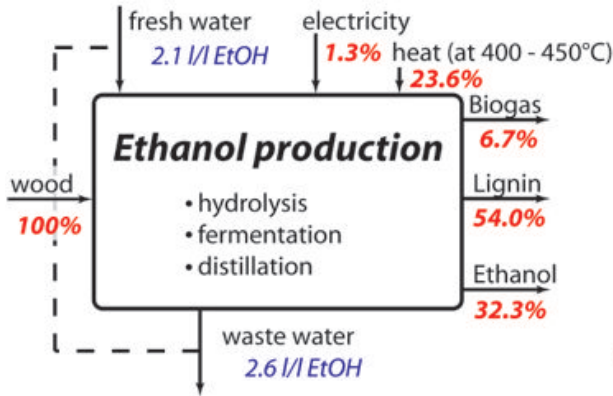
➔ Optimal plant size with respect to biomass logistics



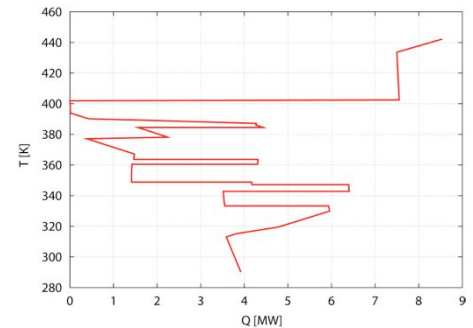
Site integration: process couplings

EtOH & SNG

Ethanol production from lignocellulosic biomass:



values based on LHV



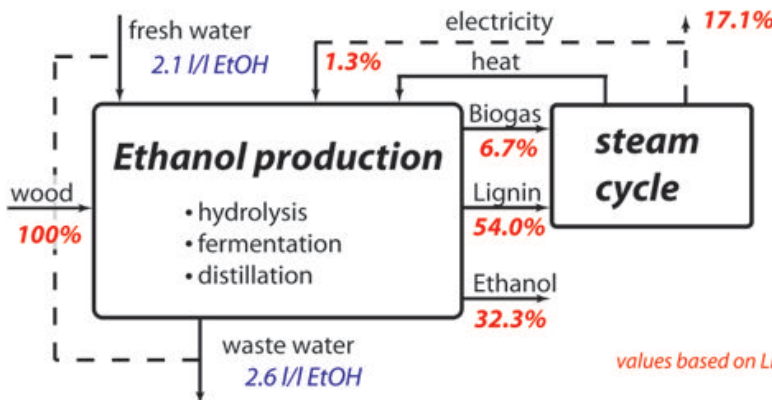
input: 58 MW_{th,wood}



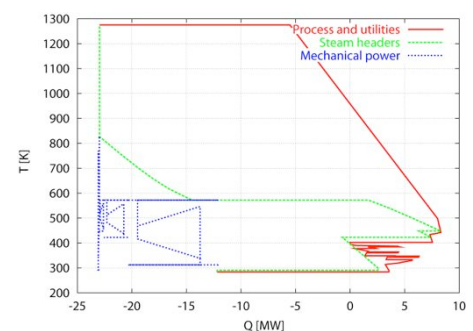
Site integration: process couplings

EtOH & SNG

Ethanol production from lignocellulosic biomass:



values based on LHV



input: 58 MW_{th,wood}

		steam cycle
Input	wood	100 %
	ethanol	32.3 %
Output	SNG	-
	electricity	17.1 %
chem. efficiency ($\Delta\eta_{NGCC}=55\%$)		62.3 %
total efficiency		49.4 %

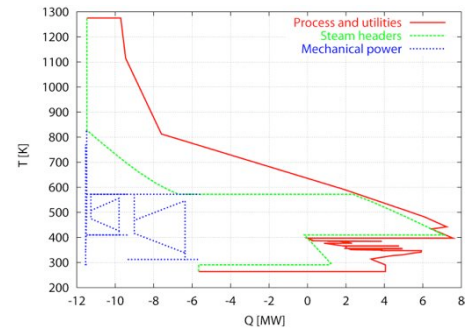
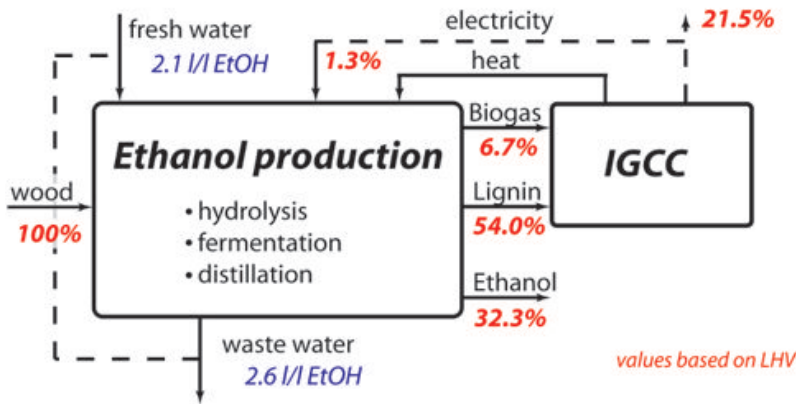
Energy balance for different process integration options (without seed train, non-optimised).



Site integration: process couplings

EtOH & SNG

Ethanol production from lignocellulosic biomass:



input: $58 \text{ MW}_{th,wood}$

		steam cycle	IGCC
Input	wood	100 %	100 %
	ethanol	32.3 %	32.3 %
Output	SNG	-	-
	electricity	17.1 %	21.5 %
chem. efficiency ($\Delta\eta_{NGCC}=55\%$)		62.3 %	70.0 %
total efficiency		49.4 %	53.8 %

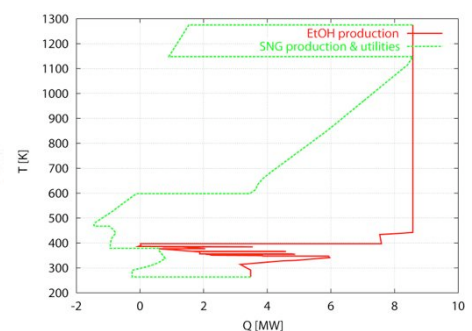
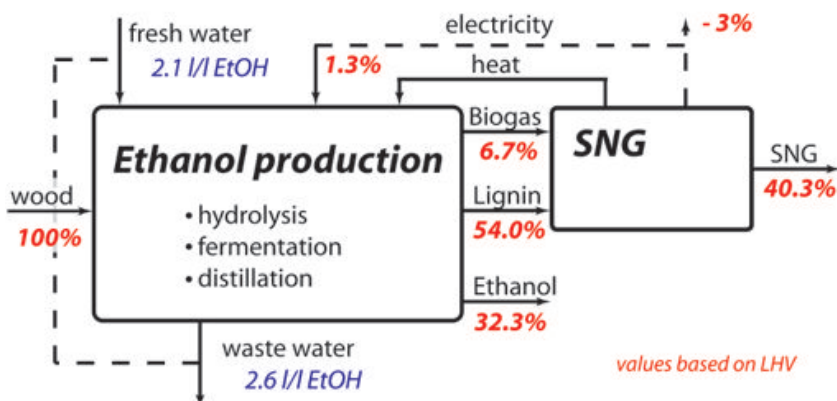
Energy balance for different process integration options (without seed train, non-optimised).



Site integration: process couplings

EtOH & SNG

Ethanol production from lignocellulosic biomass:



input: $58 \text{ MW}_{th,wood}$

		steam cycle	IGCC	SNG
Input	wood	100 %	100 %	100 %
	ethanol	32.3 %	32.3 %	32.3 %
Output	SNG	-	-	40.3 %
	electricity	17.1 %	21.5 %	-3.0 %
chem. efficiency ($\Delta\eta_{NGCC}=55\%$)		62.3 %	70.0 %	67.3 %
total efficiency		49.4 %	53.8 %	70.5 %

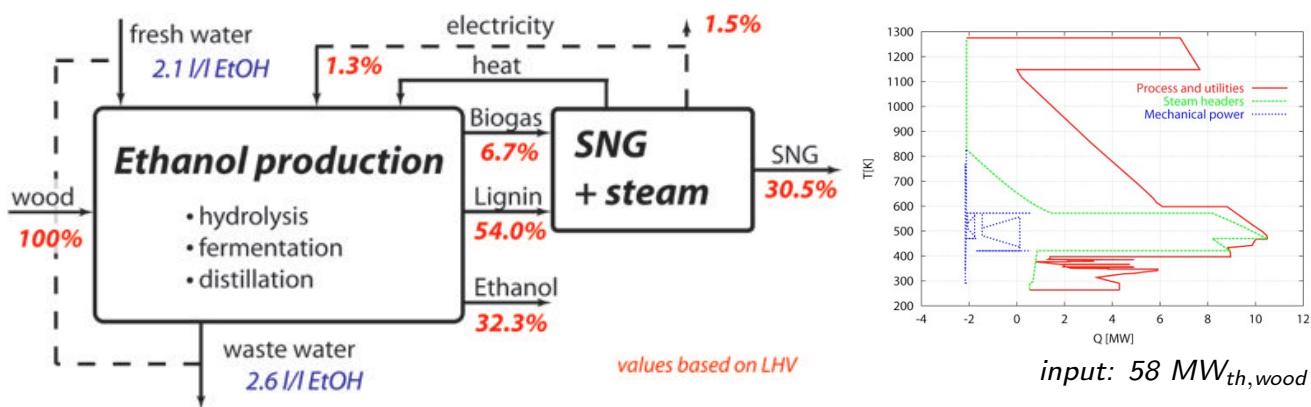
Energy balance for different process integration options (without seed train, non-optimised).



Site integration: process couplings

EtOH & SNG

Ethanol production from lignocellulosic biomass:



		steam cycle	IGCC	SNG	+ steam
Input	wood	100 %	100 %	100 %	100 %
	ethanol	32.3 %	32.3 %	32.3 %	32.2 %
Output	SNG	-	-	40.3 %	30.5 %
	electricity	17.1 %	21.5 %	-3.0 %	1.5 %
chem. efficiency ($\Delta\eta_{NGCC}=55\%$)		62.3 %	70.0 %	67.3 %	65.3 %
total efficiency		49.4 %	53.8 %	70.5 %	64.2 %

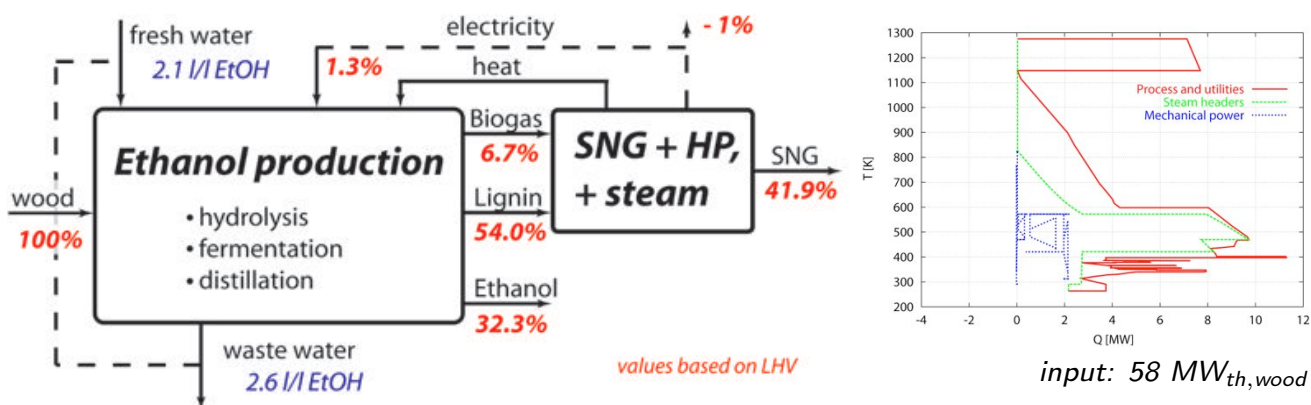
Energy balance for different process integration options (without seed train, non-optimised).



Site integration: process couplings

EtOH & SNG

Ethanol production from lignocellulosic biomass:



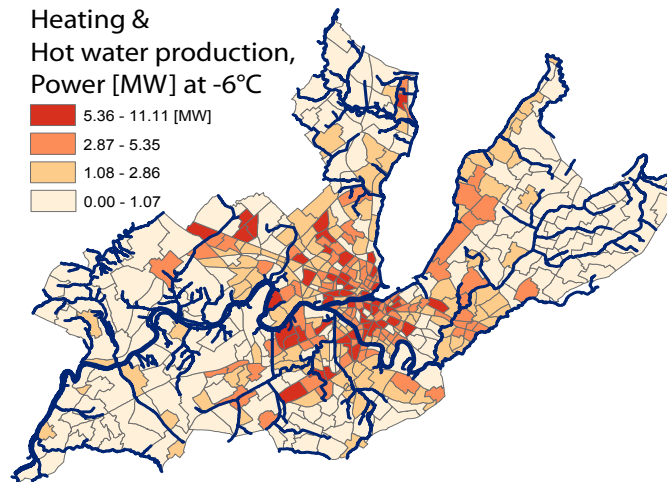
		steam cycle	IGCC	SNG	+ steam	+ HP
Input	wood	100 %	100 %	100 %	100 %	100 %
	ethanol	32.3 %	32.3 %	32.3 %	32.2 %	32.2 %
Output	SNG	-	-	40.3 %	30.5 %	41.9 %
	electricity	17.1 %	21.5 %	-3.0 %	1.5 %	-1.0 %
chem. efficiency ($\Delta\eta_{NGCC}=55\%$)		62.3 %	70.0 %	67.3 %	65.3 %	72.3 %
total efficiency		49.4 %	53.8 %	70.5 %	64.2 %	73.1 %

Energy balance for different process integration options (without seed train, non-optimised).



6. Overall System analysis

Extending system boundaries
Locate the plant for CHP



Heating requirement in the Canton of Geneva

Francis.Marchetti@epfl.ch - Laboratory for Industrial Energy Systems - LENI (EPFL-EPFL) - March 2006



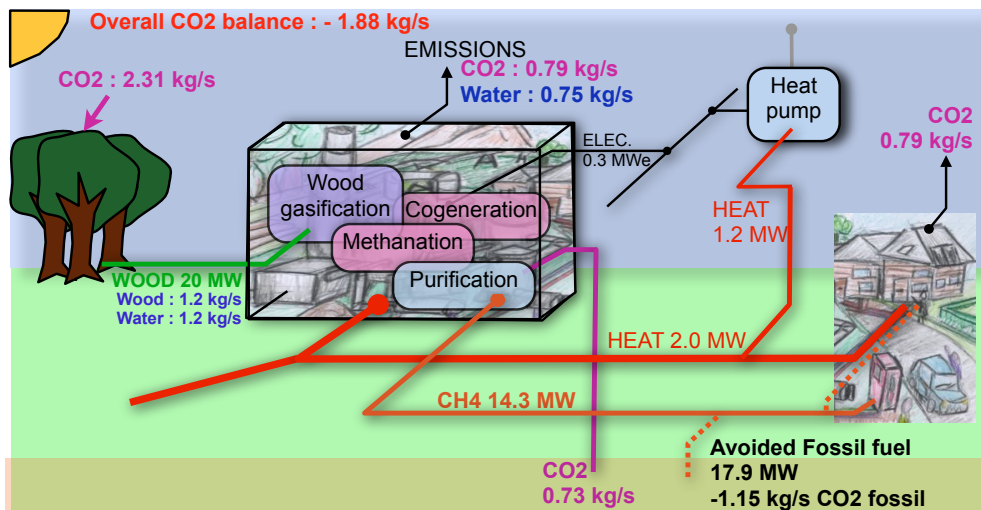
Girardin, et al., Energy, (2010)

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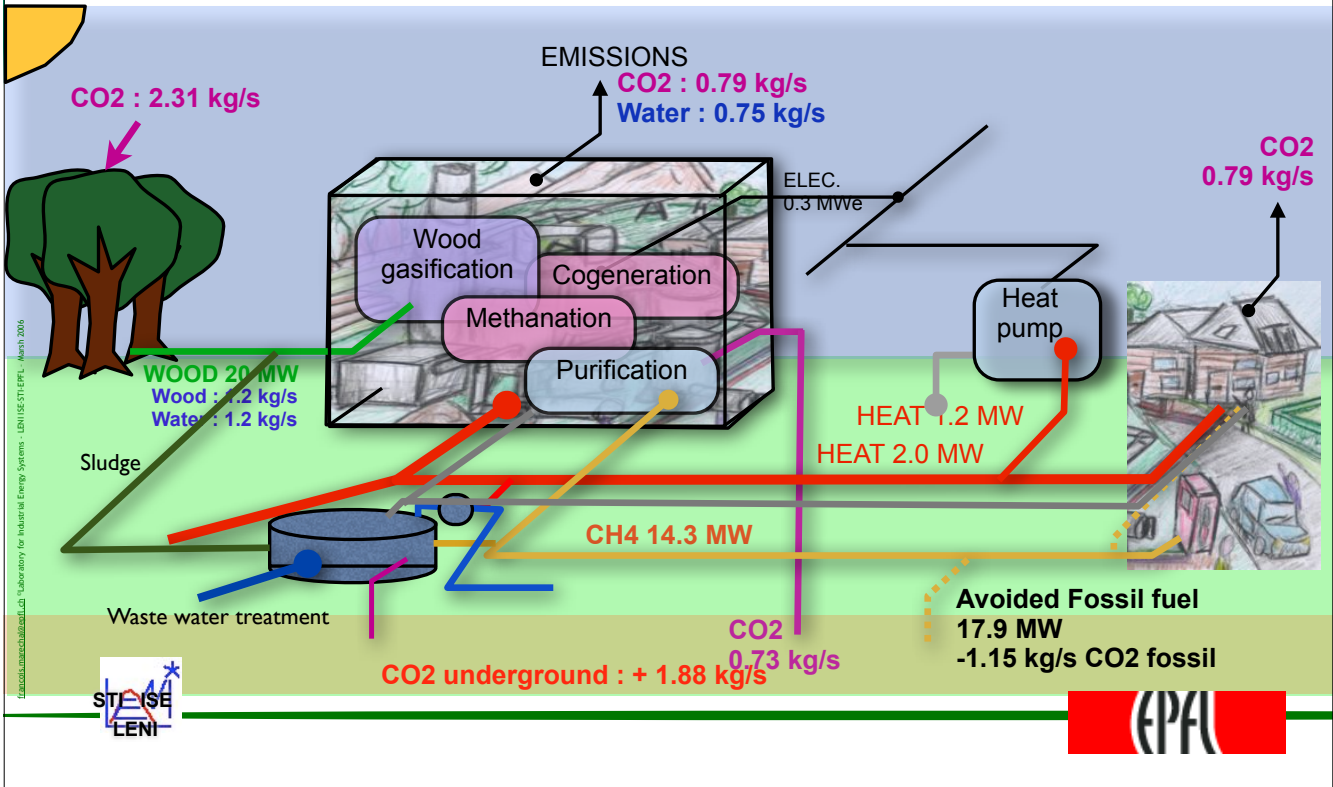


The System vision of the bio SNG plant

1 Swiss family of 4 person with hybrid SNG car and SIA standard house require 2 Ha of forest and ... sucks CO₂ from the environment.



Towards Industrial ecology



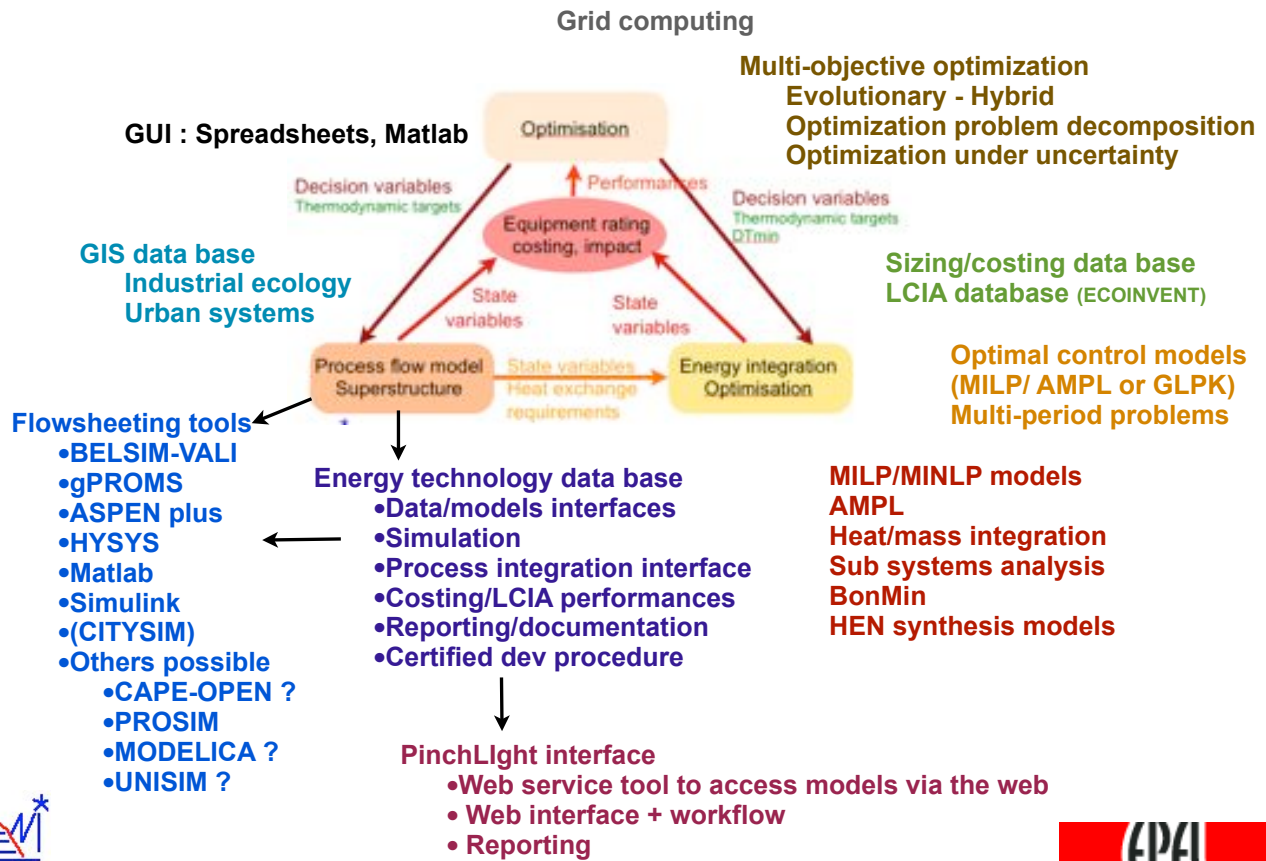
Motivations

7. Computer aided design framework

OSMOSE

developed by the LENISYSTEM group

OSMOSE : A process system design platform



Conclusions

- ▶ **Process integration and design methods for sustainable biofuel systems**
 - ▶ Energy system analysis
 - ▶ Thermo-economic models
 - ▶ Process integration techniques
 - ▶ Life cycle assessment methods
 - ▶ Multi-objective optimization techniques
 - ▶ Systems "thinking"
- ▶ from **multi-disciplinarity** to **inter-disciplinarity**

Thanks to my team and co-workers

**Dr Martin Gassner, Dr Matteo Morandin,
Dr Alexis Duret, Dr Raffaele Bolliger, Dr
Leandro Salgueiro**

**Leda Gerber, Suping Zang, Laurence
Tock, Luc Girardin, Emanuela Peduzzi,
Matthias Dubuis, Helen Becker**



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