



ÉCOLE POLYTECHNIQUE
FÉDÉRALE DE LAUSANNE

Numerical analysis of a near-to-real scale experiment of a deep geological repository

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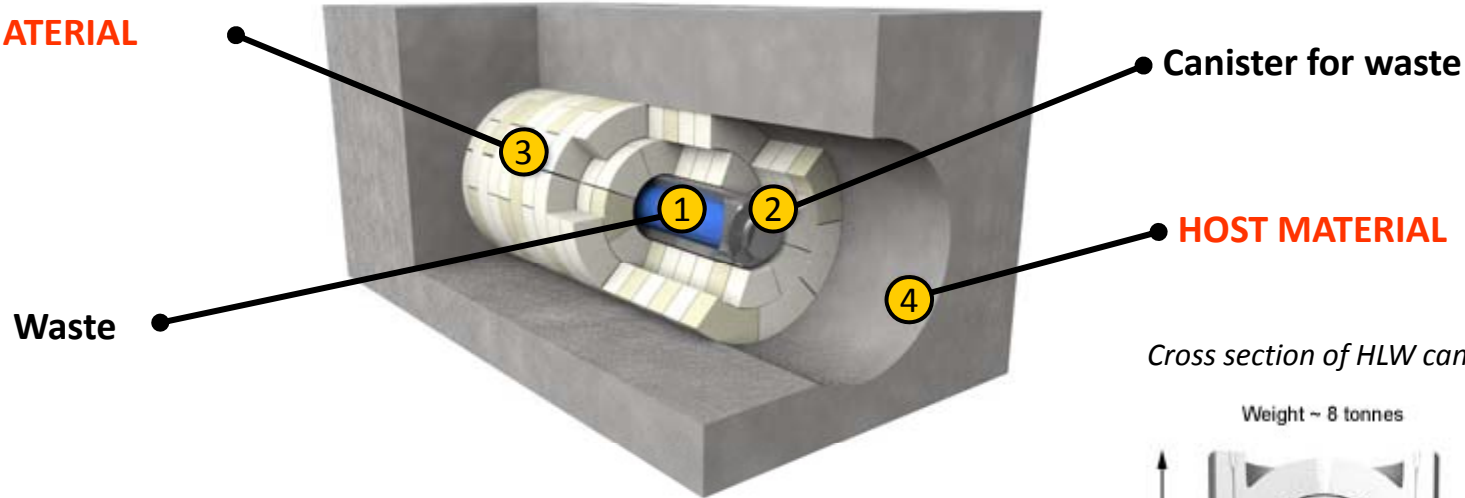
Outline

- Concept of EBS and FEBEX experiment
- Model and materials
- Comparison of results with the experiment

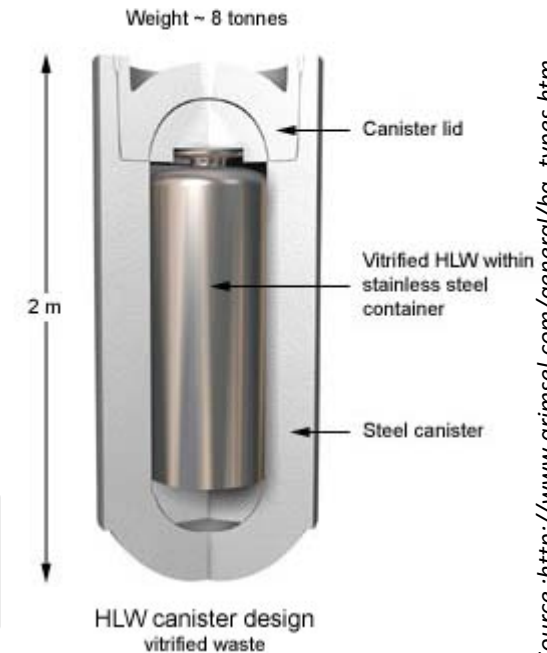
The concept of multi-barrier system (MBS)

Multiplying the number of barrier increases the safety

Source :http://www.grimself.com/febex/febex_intro_1.htm



Cross section of HLW canister



Source :http://www.grimself.com/general/bg_types.htm

Host material is **granite** or argillaceous material.

Buffer material is made of **argillaceous material (bentonite)**:

- restriction of the contact between groundwater and waste
- limitation of radionuclides migration after container failure

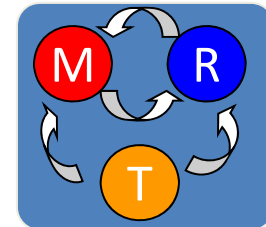
Adequate model for the THM behaviour of bentonite is a key to modeling the response of MBS

ACMEG-TS : Stress-strain framework in **non-isothermal** conditions

	Modelled behaviour	Stress variable	Strain variable	Constitutive Relation
M Mechanical		$\sigma'_{ij} = \sigma_{net\ ij} + S_r s$ <p>Generalised effective stress</p>	\mathcal{E} <p>Skeleton strain</p>	$d\sigma'_{ij} = \mathbf{D}_{ijkl} : d\epsilon_{kl}$ <p style="text-align: center;">↓</p> $d\sigma'_{ij} = \tilde{\mathbf{D}}_{ijkl}(T) : (d\epsilon_{kl} - \beta_{kl} dT)$
R Retention		$s = (p_a - p_w)$ <p>Matric suction</p>	S_r <p>Degree of saturation</p>	$ds = A \cdot dS_r$ <p style="text-align: center;">↓</p> $ds = \tilde{A}(T) \cdot dS_r$ <p>A: Retention properties</p>

+ **T**emperature T →

Thermo-hydro-mechanical couplings



ACMEG-TS : Non-isothermal unsaturated yield limits

Temperature effect

$$\tilde{p}'_c(T) = p'_{c0} \left[1 - \gamma_T \log \left(\frac{T}{T_0} \right) \right]$$

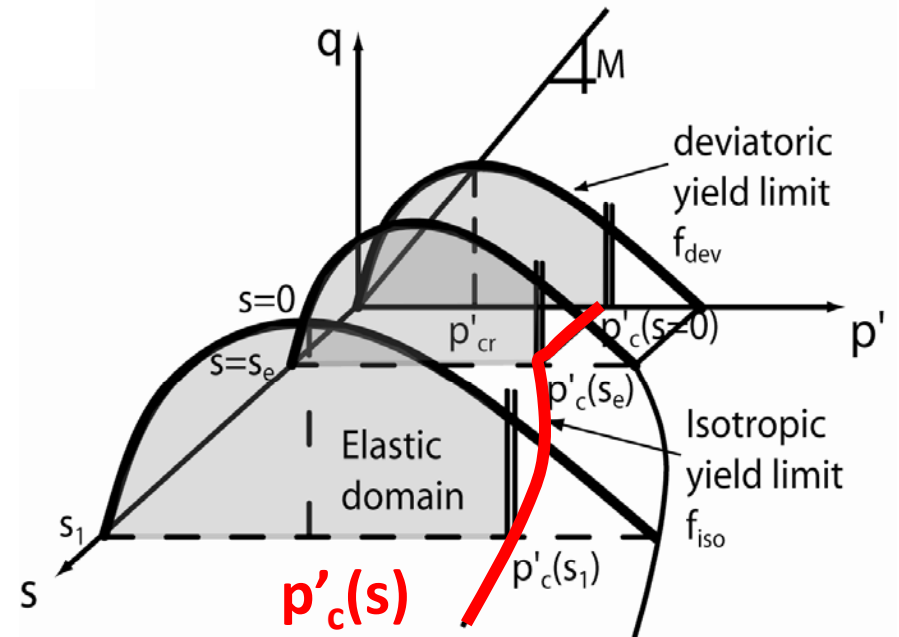
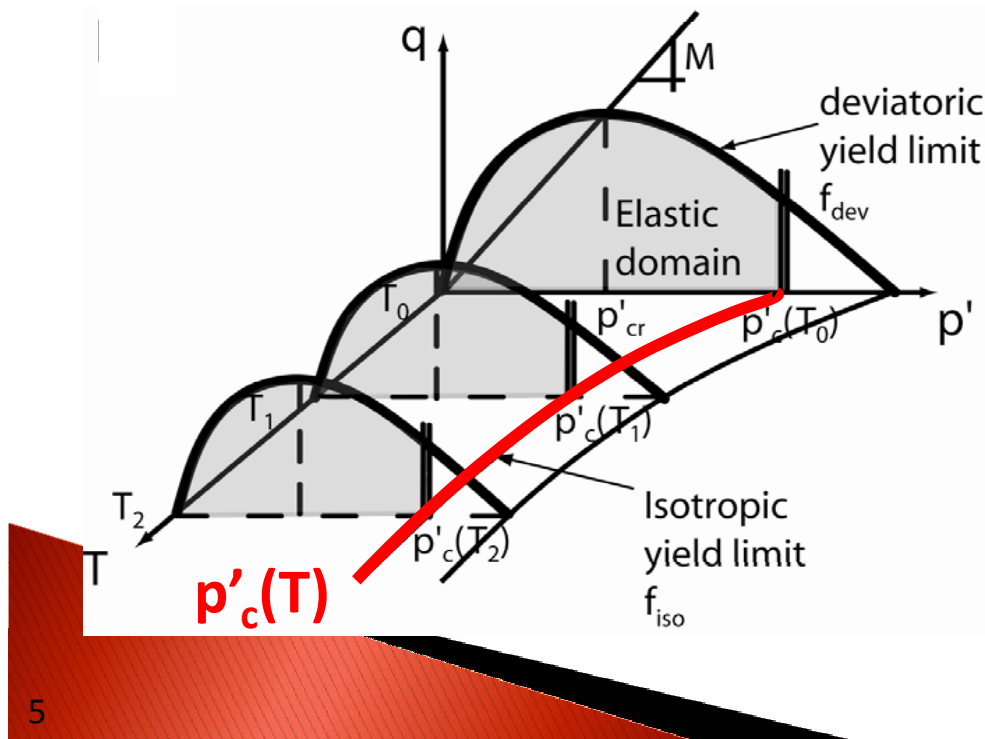
Suction effect

$$\tilde{p}'_c(s) = p'_{c0} \quad \text{for } s < s_e$$

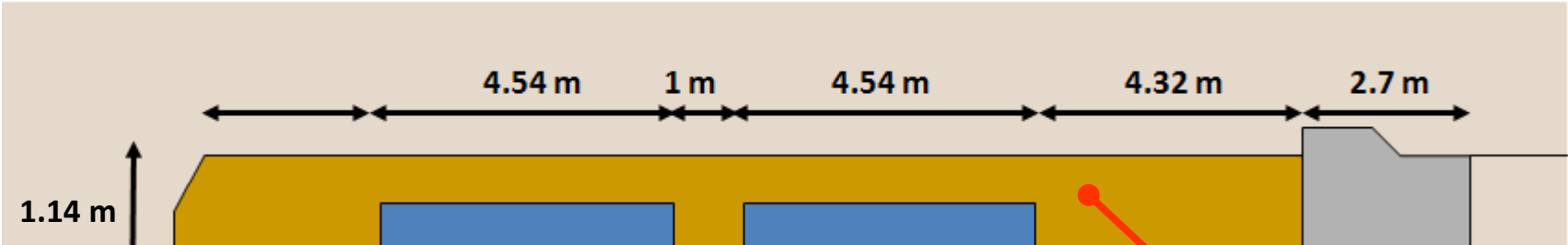
$$\tilde{p}'_c(s) = p'_{c0} \left[1 + \gamma_s \log \left(\frac{s}{s_e} \right) \right] \quad \text{for } s > s_e$$

$$\tilde{p}'_c(T, s) = p'_{c0} \left[1 - \gamma_T \log \left(\frac{T}{T_0} \right) \right] \quad \text{for } 0 < s < s_e$$

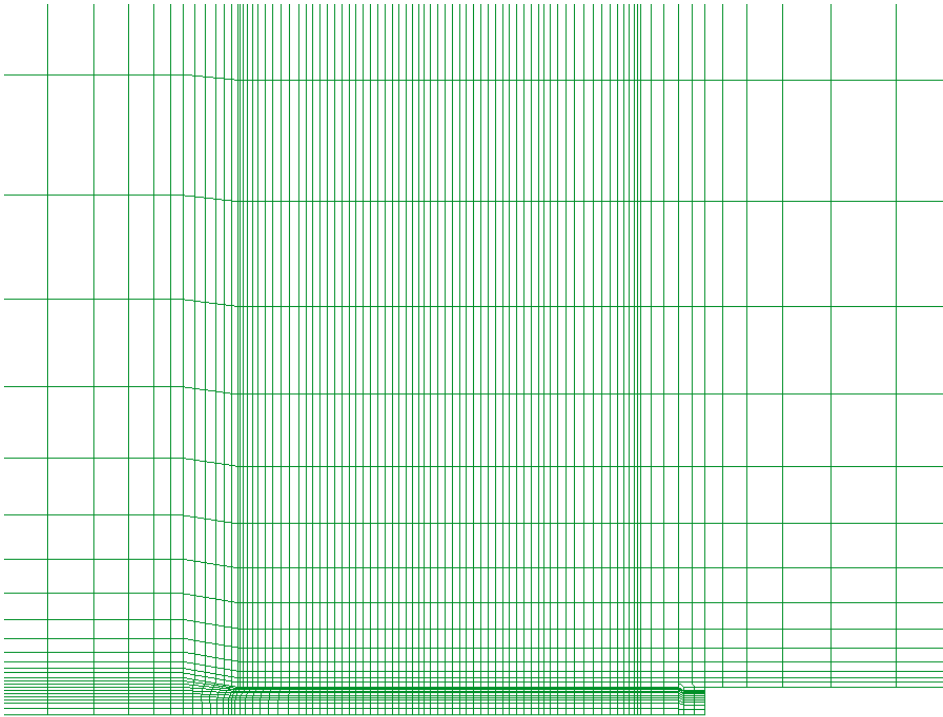
$$\tilde{p}'_c(T, s) = p'_{c0} \left[1 - \gamma_T \log \left(\frac{T}{T_0} \right) \right] \left[1 + \gamma_s \log \left(\frac{s}{s_e} \right) \right] \quad \text{for } s > s_e$$



Febex in-situ test : Model



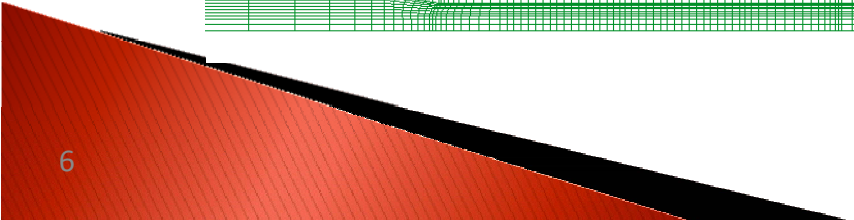
Dimensions



Mesh

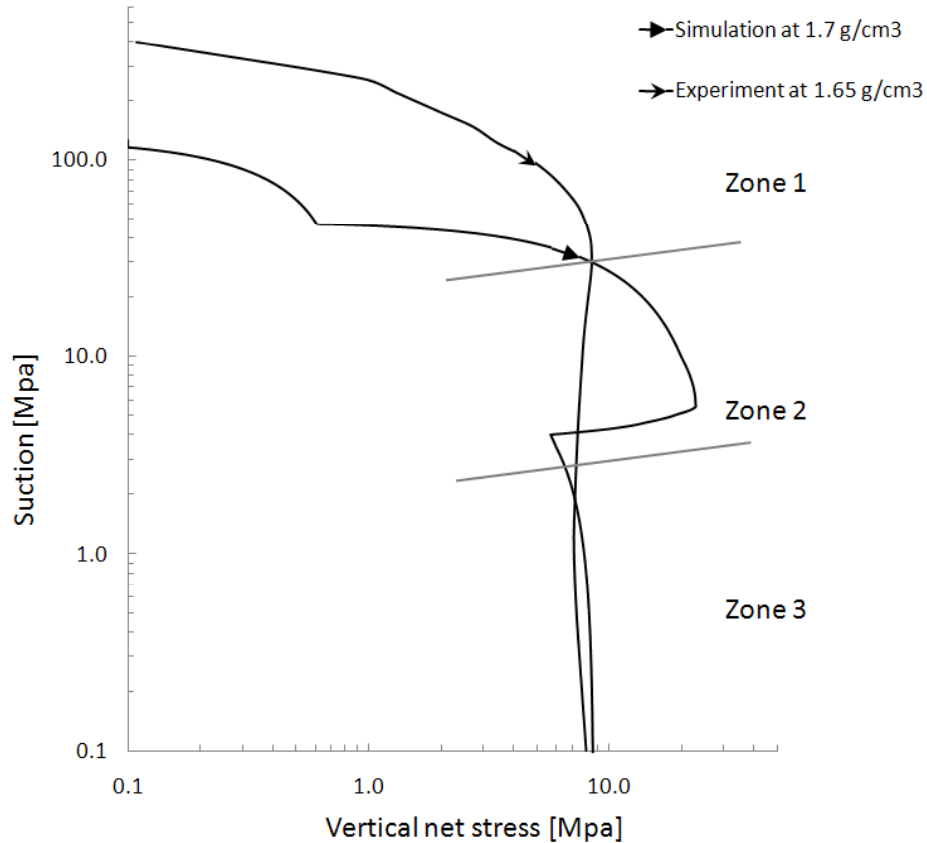
Buffer
Bentonite
Hardening plasticity
Thermal and suction effects

Other materials
Thermo-elasticity

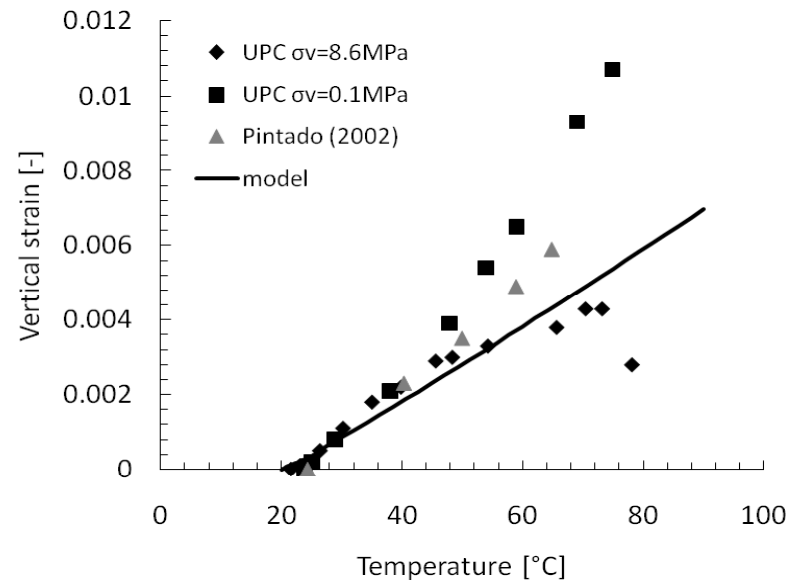


Febex in-situ test : Materials

Identification procedure



Constrained swelling behaviour



Thermal dilation

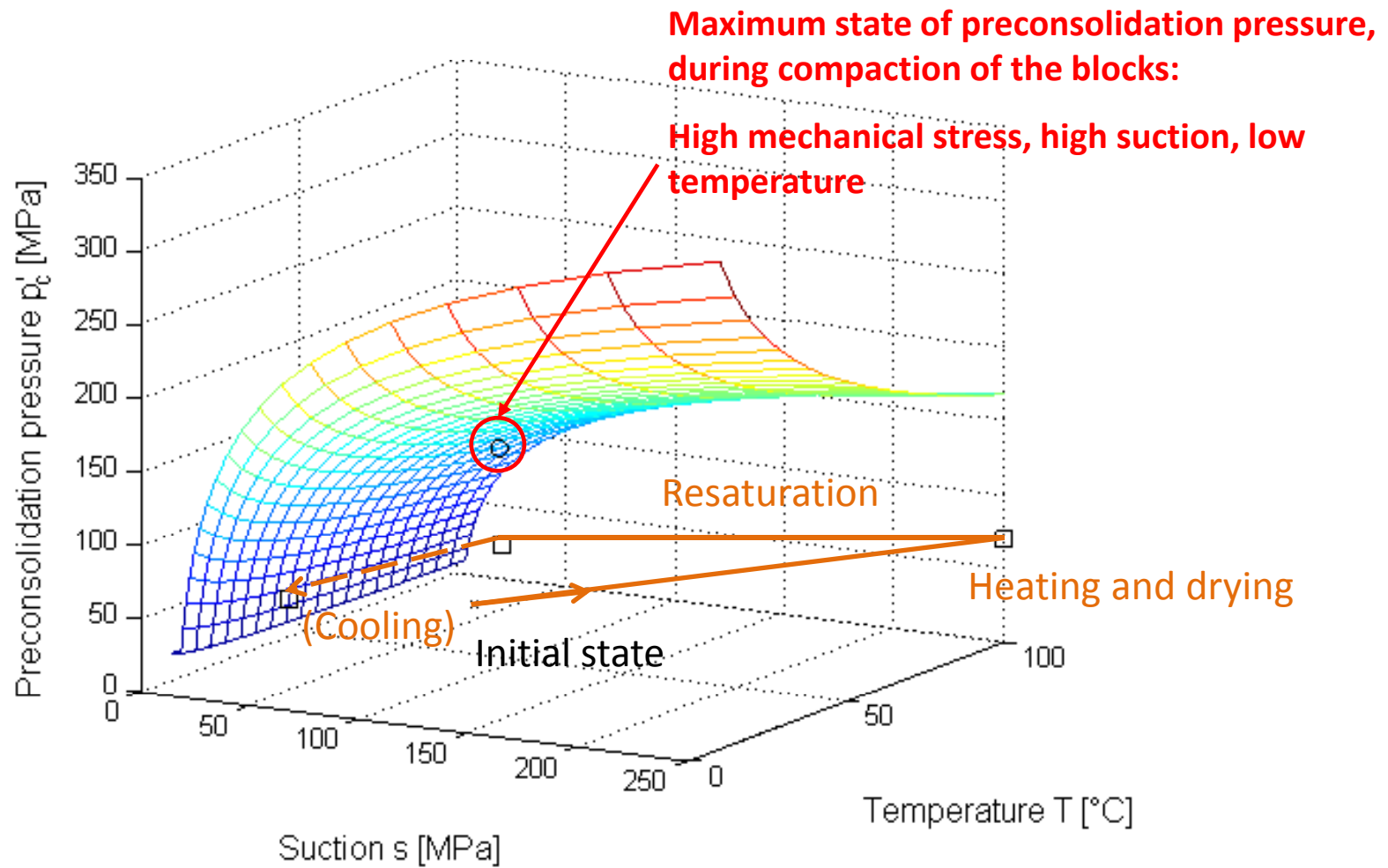
Experiments by Romero et al., Pintado et al.

F. Dupray, B. François and L. Laloui
 ComGeo II - 28 April, 2011



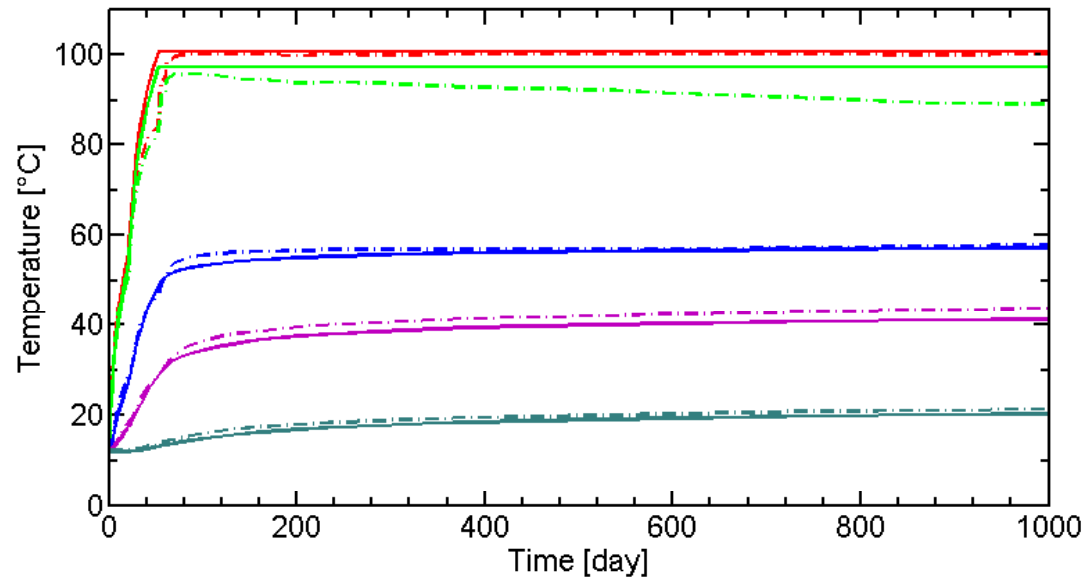
Febex in-situ test : Materials

Identification procedure



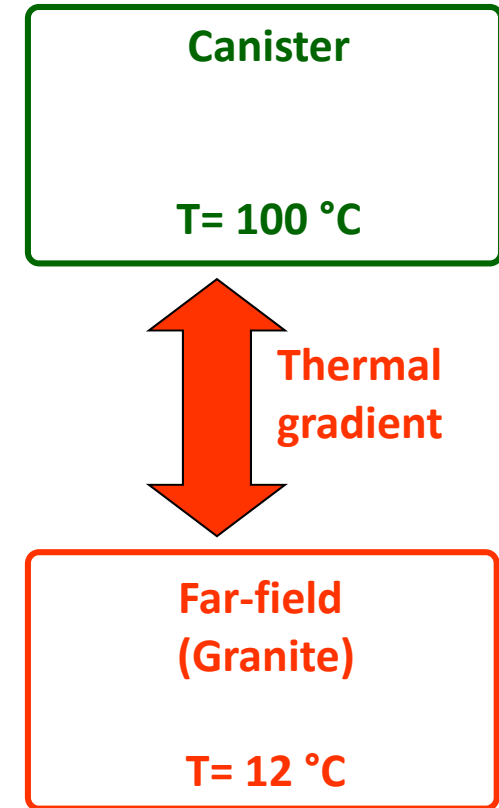
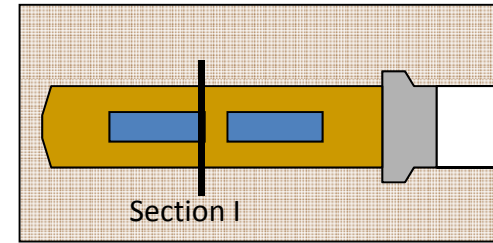
Febex in-situ test : Results

Temperature in bentonite



— Numerical simulation
- - - Experiment

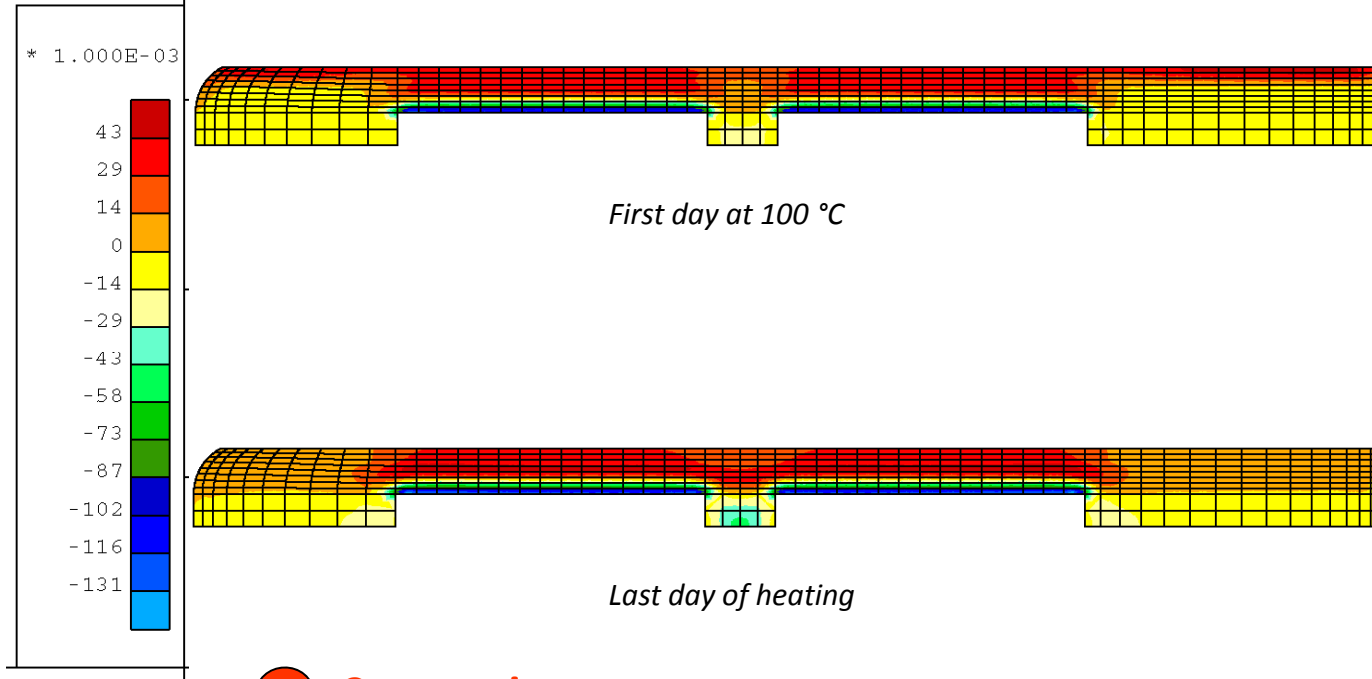
Experimental data from ENRESA



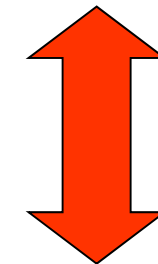
Febex in-situ test : Results

Strains and stresses

Radial strains



Granite-bentonite Interface
Swelling
Higher radial stress



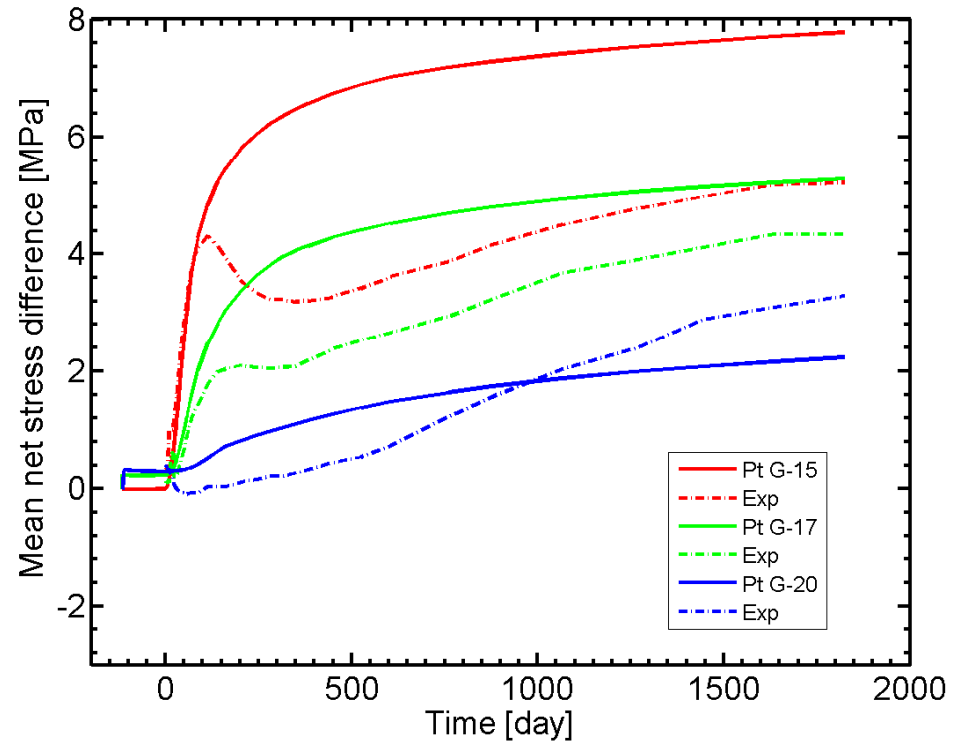
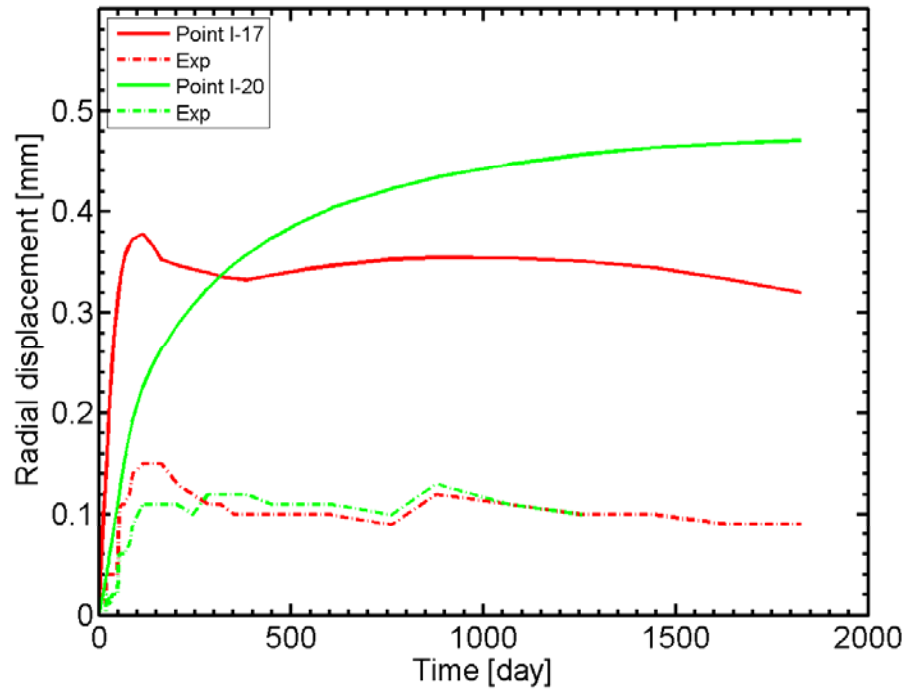
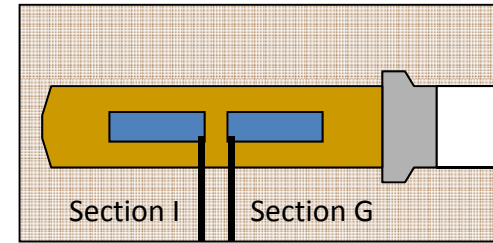
Stress gradient

Canister-bentonite Interface
Shrinkage
Lower radial stress

- 1 Contraction**
Thermo-plasticity + hydraulic shrinkage
- 2 Dilatation**
Thermal expansion + hydraulic swelling
- 3 Consequence**
Displacement of bentonite towards heater

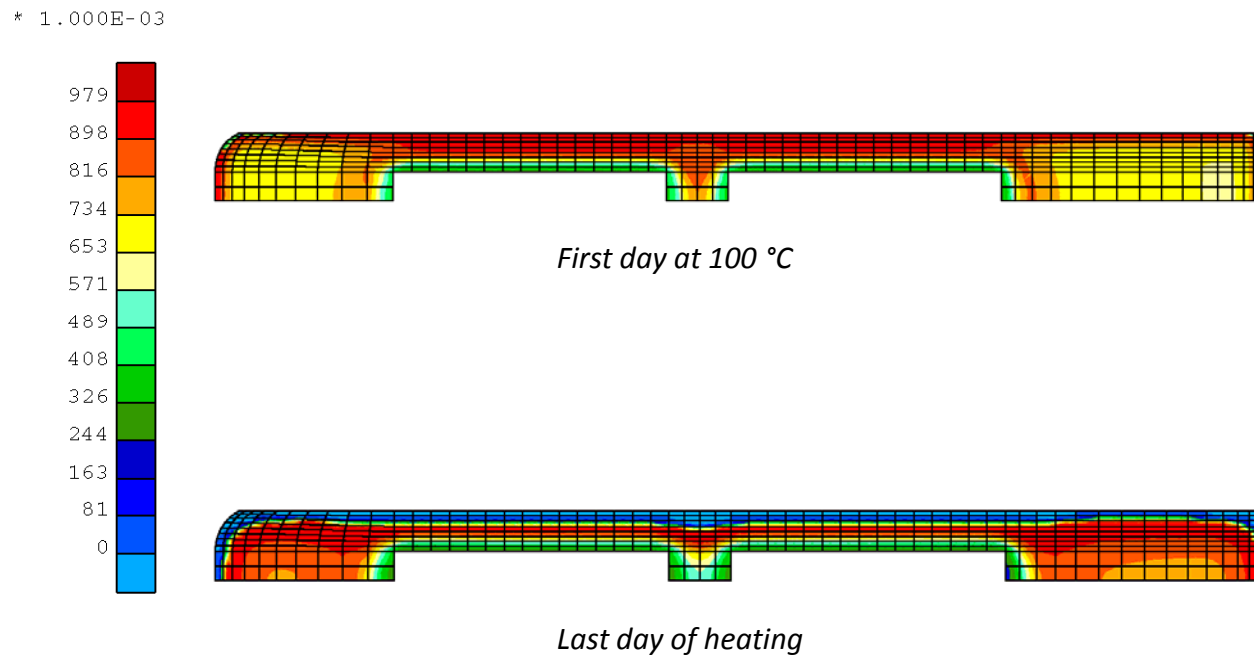
Febex in-situ test : Results

Strains and stresses

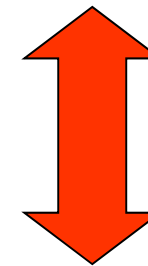


Febex in-situ test : Results

Relative humidity



**Granite-bentonite
Interface**
Resaturation
of the bentonite

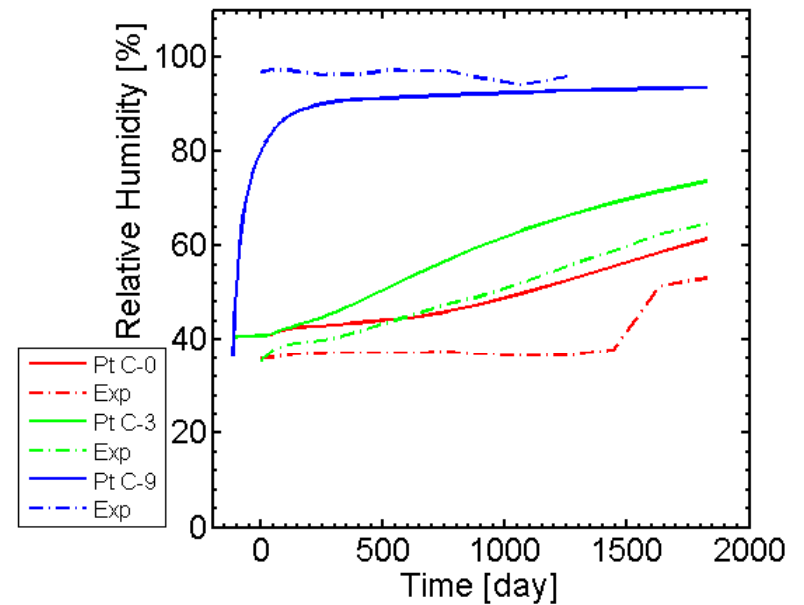
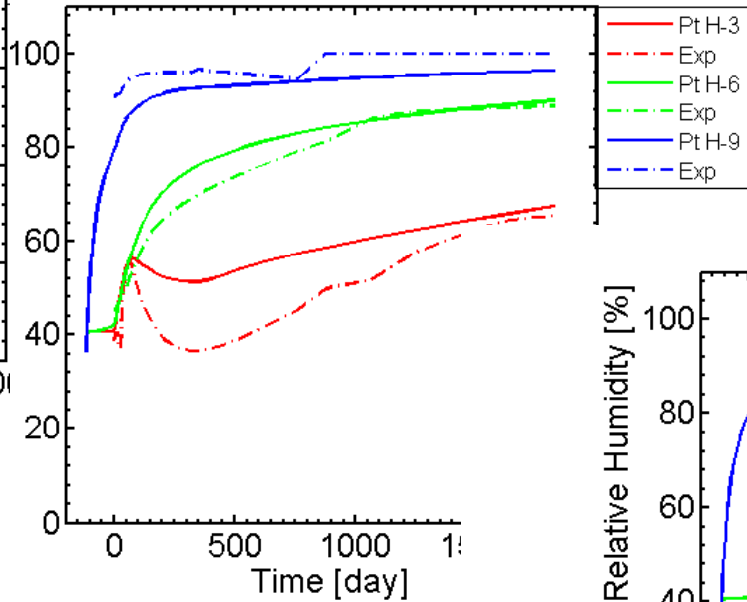
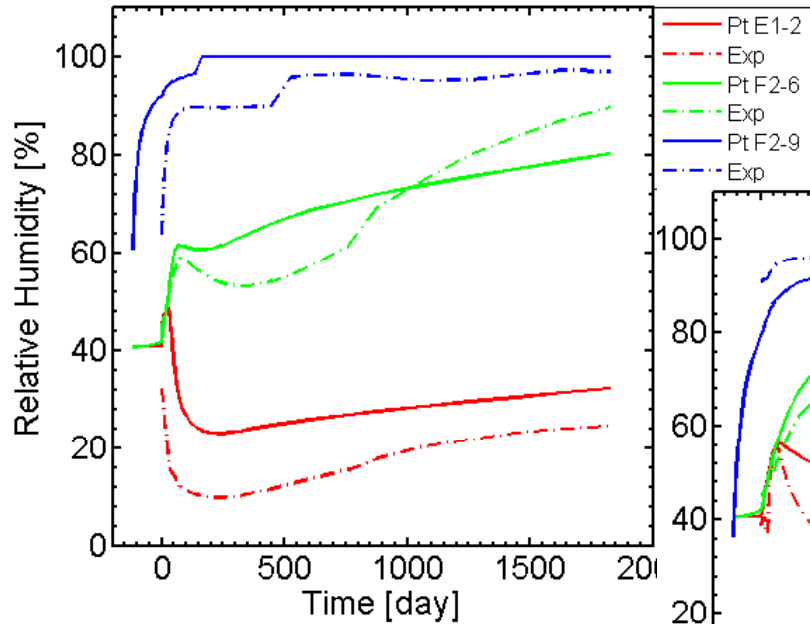
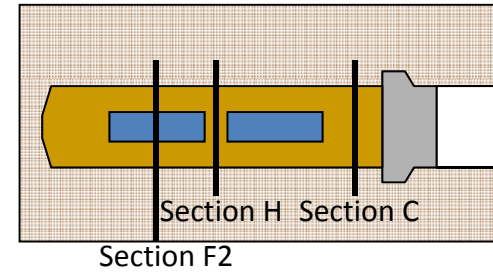


**Hydraulic
gradient**

**Canister-bentonite
Interface**
Drying
of the bentonite

Febex in-situ test : Results

Relative humidity



Febex in-situ test : Results

Degree of saturation and suction

Non univocal S_r - s relation

Interface canister-bentonite

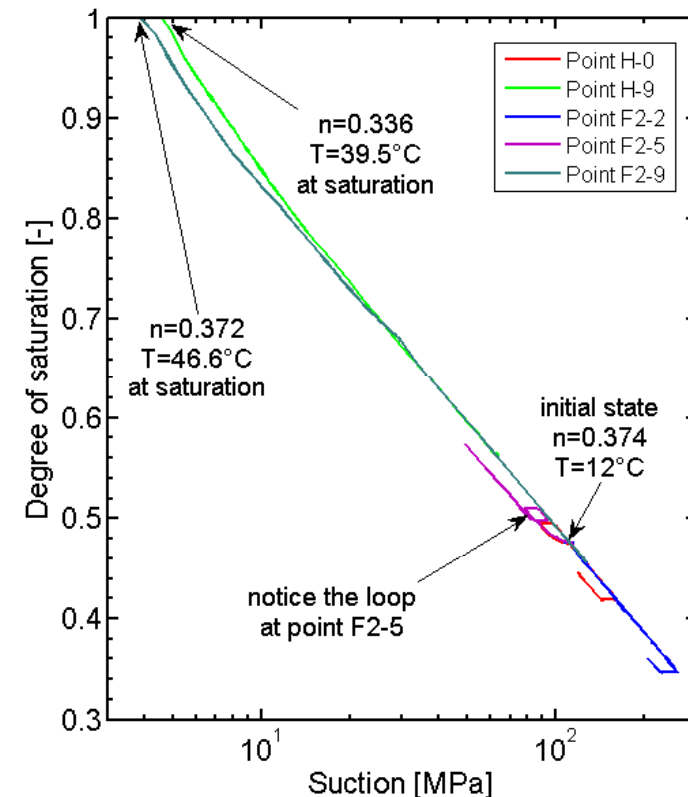
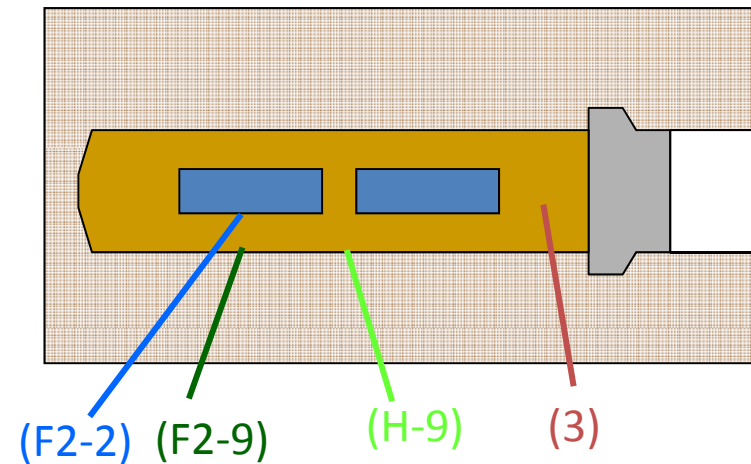
- (1) Contraction
Increase of retention capacity
But hardly visible due to drying

Interface granite-bentonite

- (2) Swelling followed by thermal collapse
Contraction (strong for H-9)
Visible difference between H-9 and F2-9

Far field

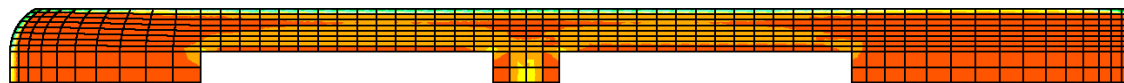
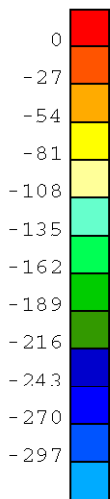
- (3) No significant strain
No significant effect on water retention curve



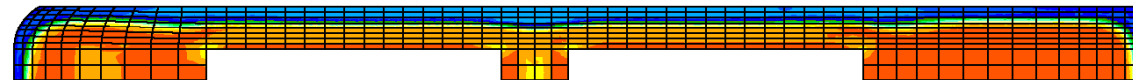
Febex in-situ test : Results

Plasticity due to heat or suction change

* 1.000E-04

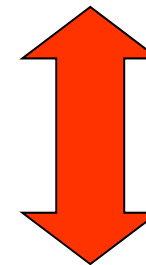


First day at 100 °C



Last day of heating

**Granite-bentonite
Interface**
Resaturation
High plastic strains

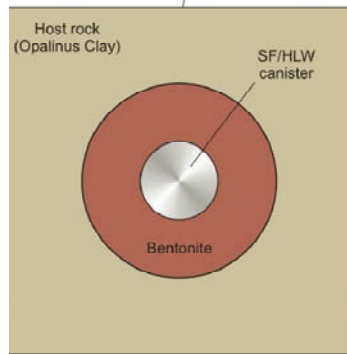
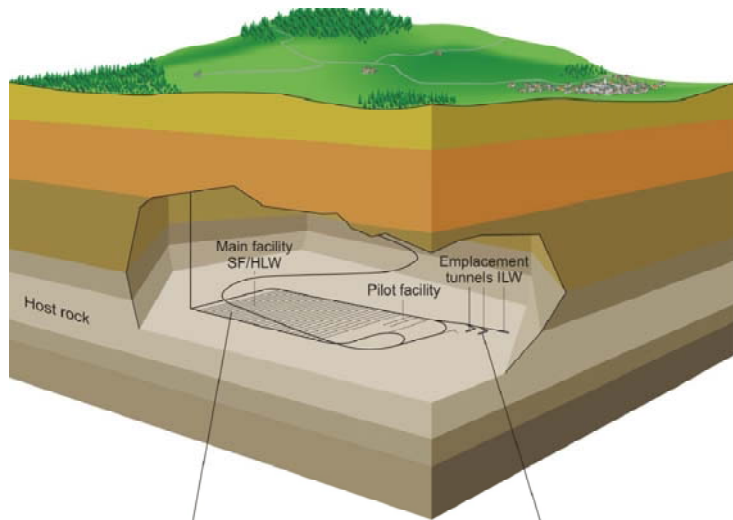


**Canister-bentonite
Interface**
Drying
Little plastic strains

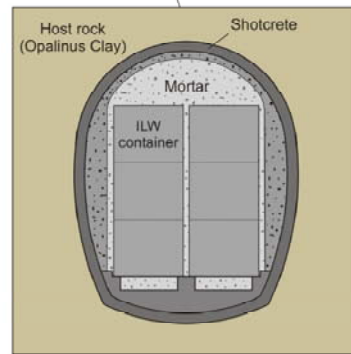
Conclusions

- **Unsaturated soils mechanics** is significantly contributing to the field of radioactive waste disposal and **generalized effective stress approach** gives adequate results in this field.
- The proposed **THM ACMEG framework**, in which attention is given to the **basic phenomena** and to their governing laws, is motivated by **its universality**.
- The comparison of this simulation with **actual experiment** reveals excellent agreement in most quantitative aspects, and explains qualitatively observed data that could not be simulated with other models, such as the peak in swelling pressure.

This research was made possible by the FEBEXe consortium, , and .



Emplacement tunnel SF/HLW



Emplacement tunnel ILW

Thank you for your attention
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