

Research Article

From Laboratory Studies to the Field Applications of Advanced Oxidation Processes: A Case Study of Technology Transfer from Switzerland to Burkina Faso on the Field of Photochemical Detoxification of Biorecalcitrant Chemical Pollutants in Water

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The Fenton and photo-Fenton detoxification of non-biodegradable chemical pollution in water was investigated under simulated UV light in the laboratory and under direct sunlight in Ouagadougou, Burkina Faso. The laboratory experiments enable one to make a systematic diagnosis among three types of wastewaters, identifying a biorecalcitrant wastewater containing the Chloro-hydroxy-Pyridine (CHYPR). The application of the photo-Fenton process on effluent containing the CHYPR showed not to stimulate the generation of biodegradable by-products. Optimal conditions for detoxification of effluent containing the CHYPR were found at pH = 2.8, $[\text{Fe}^{2+}] = 5.2 \text{ mM}$, initial $[\text{H}_2\text{O}_2] = 768 \text{ mM}$, for an effluent concentrated at 2.2 mM of CHYPR. The application of the photochemical process on a field pilot solar photoreactor for the detoxification of water polluted with a pesticide made with Endosulfan showed very promising results, with potential biodegradable effluents obtained at the end of the photochemical treatment. Optimal conditions of the applied study were found at pH = 3, $[\text{H}_2\text{O}_2] = 8 \text{ mM}$ and $[\text{Fe}^{2+}] = 0.18 \text{ mM}$ for an initial concentration of 0.36 mM of Endosulfan.

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1. Introduction

An estimation of the global world water pollution reveals that 60%–70% of the total pollution is due to the agricultural activities, 25% to 30% by industries, and the remaining 5% to 10% due to the domestic uses [1]. The report showed that, in the most optimistic cases, the water pollution from agricultural origin is mostly consisted of the residues of pesticide and contributes to at least 50% on the deterioration of the quality of natural waters (surface and subsoil waters). This is closely followed by the pollution of chemical industrial origin. In fact, more than 1000 new substances

are marketed each year in the world whereas up to now the toxicological information on only 1000 to 2000 of these products is accessible [2].

Most of these substances are xenobiotic (c.a. foreign to life), and very often they are synthetic products. Indeed, xenobiotic substances are in general not easily biodegradable, and they cross the biological water treatment systems without being completely degraded or even sometimes not degraded at all.

Some of these substances such as the pesticides are recognized as cause of carcinogenic, mutagen effects, or of hormonal disruptions to the fauna, wild life, and human beings.

To face these problems, waste treatment techniques such as incineration, wet oxidation, and activated carbon adsorption are often used. Unfortunately, these techniques are very expensive, and the environmental virtues of some of them are discussed.

However, biological processes remain the most economical and environmentally compatible alternative for wastewater treatment. Thus, it would be important to confirm the biorecalcitrancy of a wastewater before the application of a photocatalytic treatment. Moreover, biorecalcitrant wastewater could only be photocatalytically treated up to the point where its biodegradability is enough to let the phototreated water follows a biological treatment. Two case studies are reported in this paper to illustrate the strategy of enhancing the biodegradability of biorecalcitrant wastewaters throughout a photocatalytic process. These studies are representative of two problem solving approaches: one in an industrial developed country (Switzerland) and the other in a tropical developing country (Burkina Faso).

1.1. The Laboratory Solving Problem Approach in Switzerland versus the Field Applied Approach in Burkina Faso

1.1.1. Case Study 1: The Chemical Pollution in Wastewater in a Swiss Manufacture. In June 2004, a Swiss chemical company started the manufacture of a new significant chemical, following a three-step process. Three types of effluent of a specific composition were generated at each step, and all the three effluents were mixed to other effluents of the manufacture and treated in an activated sludge wastewater treatment plant. Before the new production, the yield of the wastewater treatment plant was efficient, and it could respect the legal rejection norms. But since the production of the new chemical has started, the yield has fallen down and the plant could not any more respect the standards, even when the hydraulic capacity overshooting of the treatment plant was still very low. The laboratory study aimed at making a diagnosis identifying the biorecalcitrant effluent and studied its degradation using the photoFenton treatment process.

1.1.2. Case Study 2 The Problem of Persistent Organic Pollutants and Obsolete Pesticides in Burkina Faso. In order to implement the national plan of the Stockholm's Convention on the persistent organic pollutants (POPs), the government of Burkina Faso carried out in 2001 and 2004 two inventories of stocks of POPs pesticides available on the extent territory of Burkina Faso. Table 1 reports the results of these inventories.

It was noticed that 90% of these pesticides were formulated with Cypermethrin (67%) and Endosulfan (3%) which are classified in the categories II and III (from the toxic to very toxic) by the WHO. The same report revealed that 13 contaminated sites of major importance are available in Burkina Faso. Since there is neither incinerator in Burkina Faso nor a specialized hazardous waste treatment plant, the experimental approach developed at the EPFL, Switzerland, was tested for the degradation of a pesticide containing Endosulfan, one of the chemicals which is known to generate toxic metabolites after a first step biological degradation [4].

2. Experimental

2.1. Materials and Apparatus. At the LBE-EPFL, the photocatalytic studies were performed using a 50 mL Pyrex flask with a cut-off at $\lambda = 290$ nm placed into a Hanau Suntest (Figure 1).

The radiation source was a Xenon lamp where the radiant flux ($80 \text{ mW} \cdot \text{cm}^{-2}$) was measured with a power meter of YSI Corporation. The lamp had a regular distribution of wavelengths with about 0.5% of the emitted photons at wavelengths shorter than 300 nm (UV-C range) and about 7% between 300 and 400 nm (UV-B range). The profile of the photons emitted between 400 and 800 nm (UV-A range) followed the solar spectrum.

Experiments were done at the light intensity of $560 \text{ W} \cdot \text{m}^{-2}$, which corresponds to a relative UVA (300–400 nm) intensity of $\text{W} \cdot \text{m}^{-2}$. All the chemicals (FeSO_4 , $7\text{H}_2\text{O}$), HCl and H_2O_2 (30% w/w) were bought from Fluka (Switzerland), and all were analytical grade (p.a.).

Three types of wastewaters (see Table 1) containing pyridine compounds were received from DLK Technology S.A, a Swiss company specialized in the developing specific technical plants for water and wastewater treatment.

The pilot plant, a SOLARDETOX ACADUS-2003 device model delivered by Ecosystem SA, Barcelona, Spain, is a one plate Compound Parabolic Concentrator (CPC) module (collector useful surface: 2.12 m^2 , photoreactor active volume 15.1 L within a total volume of 16.07 L) made of sixteen borosilicate cylindrical glass tubes. Each tube lies on a CPC aluminum mirror with one sun of concentration.

The reactor is mounted on a two-position fixed platform inclinable at 10° and 35° allowing operating at the approximate local latitude of Ouagadougou-Burkina Faso (12.2° N), at 10° angle position most of the time. A picture and the technical design of the CPC photoreactor used are shown in Figure 2.

From the operational point of view, the plant behaves a plug-flow reactor in the collector zone, connected to a 50 L polypropylene stirred tank (recirculating tank or buffer tank) for wastewater preparation: pH adjustments, catalyst, and oxidant feeding. The ensemble constituted by a plug-flow reactor in the collector zone plus a tank and a recirculation system is equivalent to a batch photoreactor.

2.2. Procedures. In the laboratory, a systematic diagnosis including the characterization of each of the three effluents received was first made, followed by the photoassisted studies on the effluent containing chloro-2-pyridin. 2 liters of the raw effluent were first acidified at $\text{pH} = 3$. For the photodegradation processing, 50 mL of this preparation was put into a 60 mL of a Pyrex flask glass, and reactants (iron and peroxide) were added. The flask glass was placed into the Suntest photoreactor for a determined time of illumination. Samplings were made every 10 minutes for TOC, HPLC, and spectrophotometric analyses, and during the Zahn Wellens tests sampling were made daily.

The field application took place at the International Institute of Water and Environmental Engineering (2iE), Ouagadougou, Burkina Faso ($12^\circ 21' \text{ N}$, $1^\circ 31' \text{ W}$). It is an

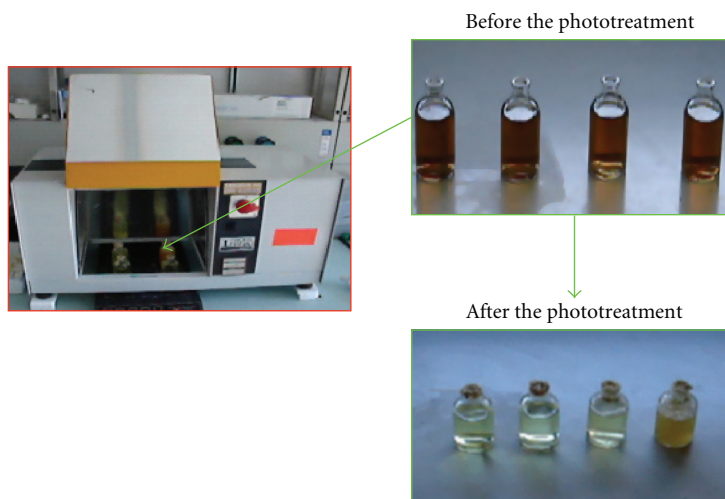


FIGURE 1: A Hanau Suntest Simulator containing 04 Pyrex flask samples during a laboratory processing at the BE-EPFL, Lausanne, Switzerland.

TABLE 1: Results of the surveys of POPs and obsolete pesticides in Burkina Faso (2001 and 2004) [3].

Form	Quantity		Nature of the pesticide in 2004	
	2001	2004		
Contaminated empty containers (—)	1450000	120'000		
Powder (kg)	26000	3000	Cypermethrin	Endosulfan
Liquid (Liters)	250000	130000	85700	4000

ideal place where solar applied researches can be carried out with more than 300 days—2500 sunny hours per year (e.g., in Almería, Spain, it is estimated up to 3000 sunny hours per year) [3].

At the beginning of an experiment, the mixture is homogenized to achieve a fixed concentration in the system, by circulating the preparation in a closed loop circuit (Tank-pump-photoreactor-tank). A desired stock of pesticide solution was first dissolved in 2 liters of tap water and stirred for at least 2 hours in the laboratory. Afterward, the solution was poured into the conditioning tank of the photoreactor in which 20 liters of tap water were previously added. Three more liters of tap water were used to rinse the predissolved Pyrex flask and added to the conditioning tank. The pH of the solution was adjusted to 3 with HCl, and the catalyst (FeCl_3) was added. The entire system was homogenized by closing the valves (1) and (3) and circulating the polluted water in a closed loop circuit for 15 minutes (see Figure 2).

Once the solution is ready, the required amount of hydrogen peroxide was added, and the feeding valve (1) was opened according to the water circulation speed needed for the operation. The water flow was varied by regulating the valve (1) to: 0.3, 0.4, and 0.5 $\text{m} \cdot \text{s}^{-1}$.

The solar ultraviolet radiation was determined during the experiments through a UVA radiometer ACADUS 85 UV mounted on the reactor, at the same angle (10°) as its plate part. It provides data in terms of incident UVA radiation per

area unit ($\text{W} \cdot \text{m}^{-2}$) and the accumulated energy $E_{(t)}$ on the 2.12 m^2 surface of the photoreactor (in Wh). $E_{(t)}$ is linked to the instantaneous irradiance flux (\overline{UV}), the reactor total active area (A), the water volume (V), and the experiment duration (t) by the following relation:

$$E_{(t)} = E_{(t_0)} + \Delta t \times \overline{UV} \times \frac{A}{V}. \quad (1)$$

2.3. Analytical Methods. At the LBE, HPLC analyses were carried out in a Varian 9065 unit provided with a Varian 9012 solvent delivery system, an automatic injector 9100 and a Varian Pro Star Variable (200–400 nm) diode array detector: 9065 Polychromic. All modules were piloted with a computer on which the Varian Star 5.3 software is installed for liquid chromatography data delivery. A reverse phase spherisorb silica column ODS-2 and a (70/30) (v/v) mixture of acetonitrile/water mobile phase were used to run the chromatography in isocratic mode at a flow rate of 1 $\text{mL} \cdot \text{min}^{-1}$. This technique allows the measuring of the main pollutant concentration in the solution and to follow the overall formation and decay of the aromatic and aliphatic by-products during the process.

A Hitachi UV-vis U-3010 and a Biomate 3 model spectrophotometers were used, respectively, at the LBE and at the 2iE, with a 1.0 cm quartz cell. The Hitachi UV-vis U-3010 spectrophotometer allowed generating the

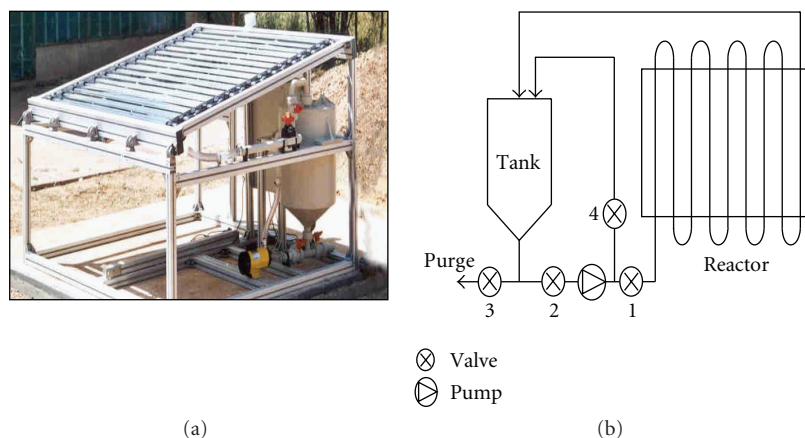
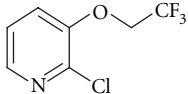
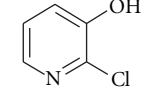


FIGURE 2: A Picture and the technical design of the CPC photoreactor.

TABLE 2: Synthesis of the characteristics of the three effluents.

Type of effluent	Main pollutant	Molecular structure	pH	TOC ($\text{g} \cdot \text{L}^{-1}$)
WW ₁	CTFEP		8.3	45
WW ₂	LQV	Confidential	6	43.5
WW ₃	CHPYR		5.8	6.5

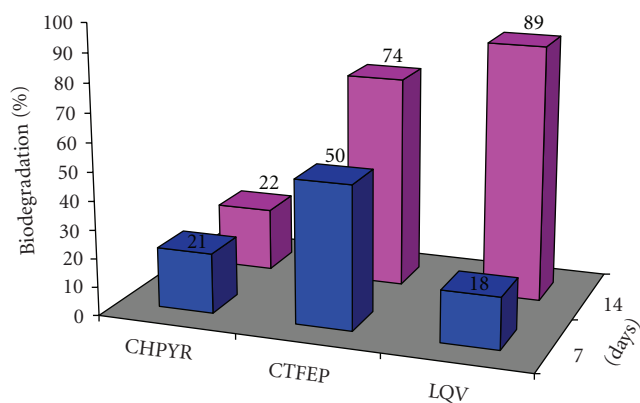


FIGURE 3: Percentage of biodegradation respectively 07 (■) and 14 days (■).

characteristic spectra of phototreated samples in the wavelength range of 200–600 nm, so that all the chemicals and/or complexes in the solutions can be signalled at their maximum absorption wavelength. Once we identified the specific absorption wavelengths through the spectra, we chose these particular wavelengths for the analyses on the multiwavelengths *Biomate 3* spectrophotometer during the field's application at the 2iE at Ouagadougou, Burkina Faso.

The biological Zahn Wellens tests were carried out on the phototreated samples after 60% degradation of the TOC, following the OCDE standard method [5].

The Chemical Oxygen Demand (COD) analyses were carried out via a Hach-2000 spectrophotometer using the dichromate solution as the oxidant in a strong acid medium. 2 mL of the samples were put into the low range kits ($0\text{--}150 \text{ mg} \cdot \text{L}^{-1}$) and digested at 150°C for two hours. Once the digested samples were cooled, their optical density was determined at $\lambda = 430 \text{ nm}$, in comparison to a blank, prepared with 2 mL of distilled water. The Biological Oxygen Demand for five days (BOD_5) was measured by means of an Hg-free WTW 2000 Oxytop unit thermostated at 20°C according to the standard method.

3. Results

3.1. A Systematic Study of the Photocatalytic Removal of the Chemical Pollution of the Industrial Wastewater in Switzerland

3.1.1. *Diagnosis: Physicochemical and Biological Characterization of Different Types of Effluents Resulting from the Processing of LQV.* Table 2 presents the characteristics of three effluents (WW_i) from the production of the LQV (its molecular

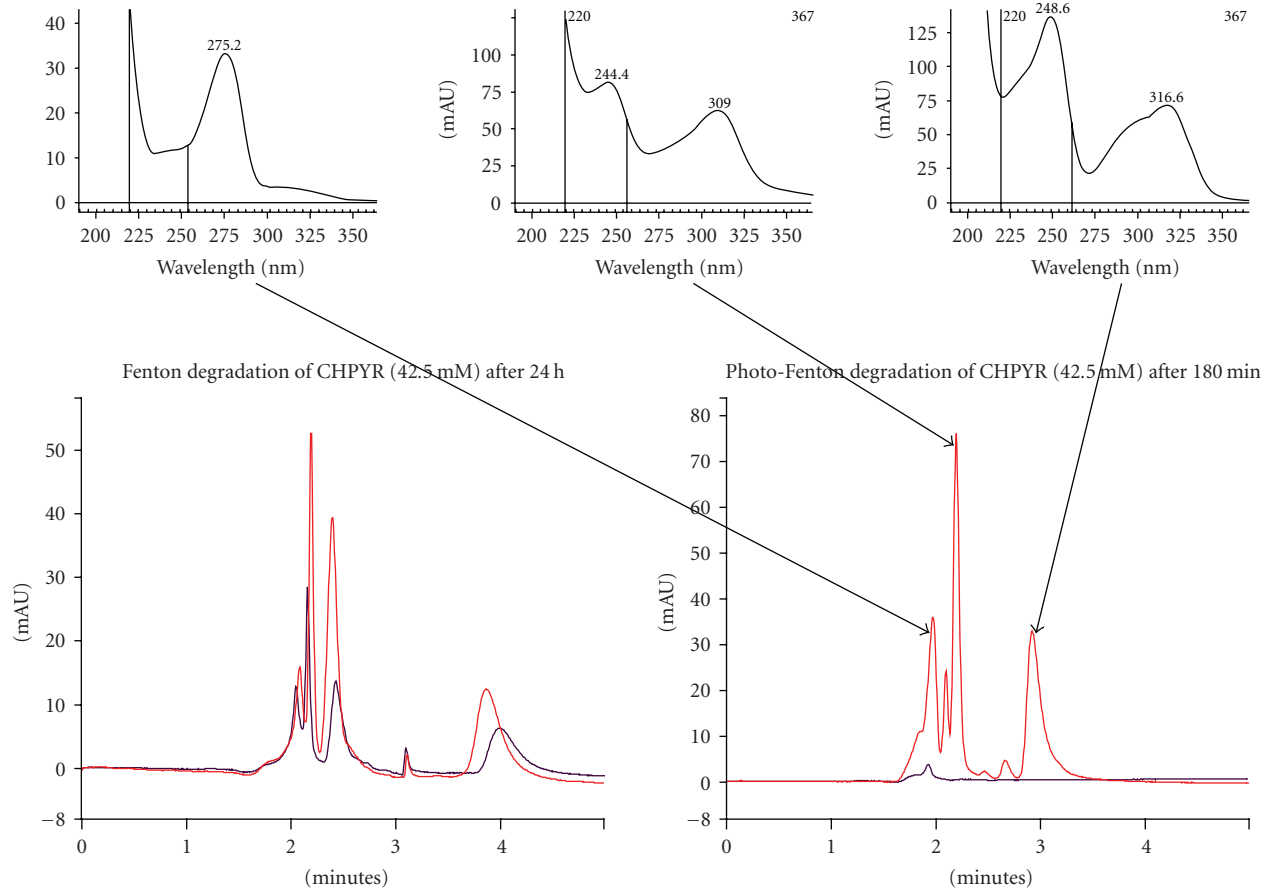


FIGURE 4: HPLC chromatograms of the CHPYR effluent before and after the Fenton (a) and the photoFenton (b) processes.

formula is confidential), and Figure 3 shows the results of the Zahn wellens tests carried out on the three effluents.

From these results, one can conclude the following.

- (i) The wastewater mainly containing CTFEP is easily biodegradable and that with LQV is biodegradable after a certain period for bacteria adaptation.
- (ii) The wastewater mainly containing CHPYR is biorecalcitrant. No change in the degradation rate was observed at the 7th, 14th, and up to the 28th day. The Fenton and photoFenton processes were applied to WW₃, and the experimental conditions were optimized for the catalyst (Fe^{2+}) and the electron acceptor (H_2O_2).

3.1.2. Fenton and PhotoFenton Treatment of the CHPYR Polluted Wastewater. Figure 4 shows the chromatograms of the CHPYR effluent carried out at the beginning and after 24 hours of Fenton treatment on 50% diluted effluent on the one hand compared to the photoFenton treatment on the same effluent for 1 h30. The UV spectra of three significant peaks are observed on the raw effluent (nontreated). The two most important peaks of the chromatograms completely disappeared in case of the photoFenton treatment, and the one

at 275.2 nm is 90% degraded; all the other peaks regressed relatively for 50% in case of the Fenton process after 24 hours.

3.1.3. Optimization of the H_2O_2 and Fe^{2+} Concentrations. Figure 5 shows that the optimal conditions for the photoFenton treatment of the CHPYR effluent are obtained in 2 hours with an initial concentration of the solution of $\text{TOC} = 2200 \text{ mg} \cdot \text{L}^{-1}$, $\text{Fe}^{2+} = 5.2 \text{ mM}$, $\text{H}_2\text{O}_2 = 768 \text{ mM}$. Under these conditions, 60% of the organic pollutants (main pollutants and their degradation intermediates) are mineralized when the CHPYR is completely exhausted in the solution within the two hours of photoFenton treatment.

3.1.4. Biodegradability of the PhotoTreated Effluent. Figure 6 shows the results of the OECD's Zahn Wellens test carried out on the phototreated CHPYR effluent under the optimal photoFenton degradation conditions ($\text{Fe}^{2+} = 5.2 \text{ mM}$; $\text{H}_2\text{O}_2 = 768 \text{ mM}$; $\text{pH} = 2.8$), with a decrease of 60% of total organic carbon. This shows that, relatively less than 15% to 18% of biological degradation is reached at the end of the first weeks followed by a fold down to 12% and stagnation until the 28th day. It is assumed that the photogenerated intermediates of degradation of the CHPYR are also biorecalcitrant or toxic. Hence a total mineralization following the Fenton or photoFenton process is necessary.

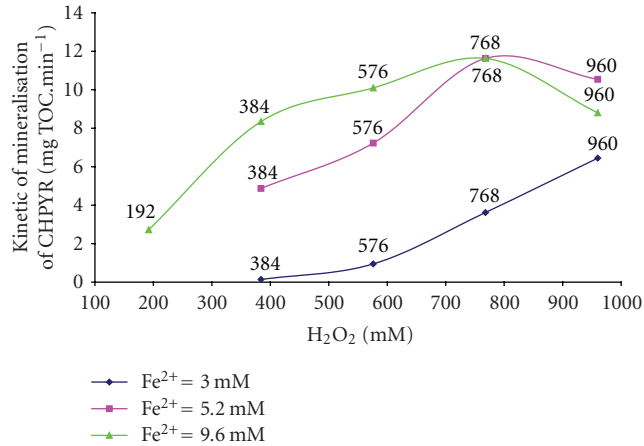


FIGURE 5: Kinetic of mineralisation of the CHPYR at various H₂O₂ concentration: (■) for 3mM; (▲) for 5.2 mM and (●) for 9.6 mM, as a function of the H₂O₂ concentration during the PhotoFenton process in a 50% diluted effluent (42.5 mM).

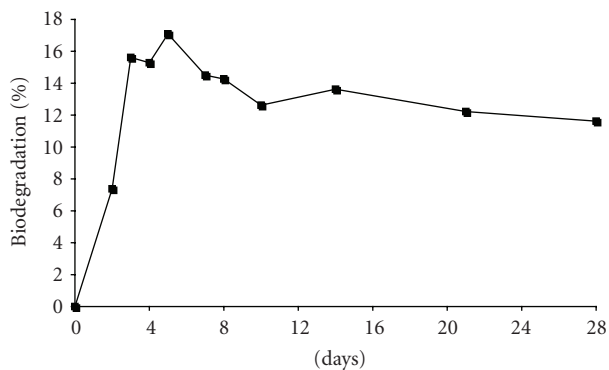


FIGURE 6: Evolution of the biodegradability following the Zahn Wellens process carried out on the CHPYR phototreated effluent.

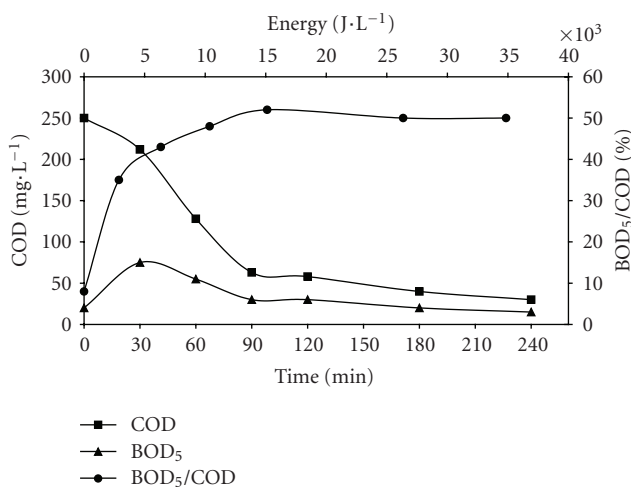


FIGURE 7: Evolution of biochemical parameter of the Endosulfan polluted water during the helio-photoFenton treatment, (■) for the COD, (▲) for BOD₅, and (●) for the BOD₅/COD ratio.

3.2. *Application of the Helio-PhotoFenton Process for the Degradation Wastewater Polluted with Endosulfan.* The monitoring of the biodegradability of the solar-treated effluent was conducted on 30 minutes sampled effluents. The results in Figure 7 show that the BOD₅ increases during the first 30 minutes of the treatment and decreases during the next hour; after that it remains constant. At the same time, the COD is continuously decreasing during one and half hour after which it remains constant. As a consequence of the evolution of these two parameters, the intrinsic biodegradability defined as the ratio BOD₅/COD is continuously increasing up to 50% where it became constant when the energetic treatment factor of the process is $15 \times 10^3 \text{ J} \cdot \text{L}^{-1}$.

4. Discussions

4.1. *Study of the Management of the Chemical Industry Effluents.* Figure 4 confirmed the presence of biorecalcitrant pollutant (CHPYR) with maximum UV absorption at 309 nm. The studies carried out on the three types of effluents also showed that the effluents mainly containing LQV and of the CTFEP were biodegradable and only that of CHPYR was biorecalcitrant. However, the CHPYR effluent can be degraded through the Fenton and photoFenton processes, within the optimal conditions: $[\text{Fe}^{2+}] = 5.2 \text{ mM}$; $[\text{H}_2\text{O}_2] = 768 \text{ mM}$ for effluent concentrated at $2.2 \text{ g} \cdot \text{L}^{-1}$ of CHPYR. However, the Fenton process was not timely efficient.

The Zahn Wellens tests carried out on the phototreated effluent up to 60% TOC reduction did not show any significant biodegradability meaning that the remaining carbonic components in the treated effluent still were biorecalcitrant. It would be preferable to phototreat the effluent totally (i.e., up to more than 90% mineralization).

For a better management of the effluents resulting from that manufacture, the following diagram in Figure 8 would be recommendable.

4.2. *The Scaling up Approach from Laboratory Studies to the Field Application.* Studies in the laboratory and within very high-tech experimental device potential, made it possible to highlight the applicability of the Fenton and photoFenton processes for the detoxification of non biodegradable pollution in water. However, since the aim of this research is to undertake this process for solving real problems, its scaling up applicability (on more significant volumes) still to be evaluated, particularly when operating using the sunlight and not the lamps which of course, are cost expensive. The example of the artificial contamination of water by Endosulfan in Burkina Faso approaches more the reality since cases of contamination of water of the ground water by the pesticides had been reported in Burkina [6].

It's possible that, by submitting the commercial pesticide which composed of the active component: the endosulfan (water solubility $0.325 \text{ mg} \cdot \text{L}^{-1}$) and other additives such as emulsifiers and adhering agents (which stabilizes the product on the plant once it is pulverized) to the Fenton and photoFenton processes, some of these additives would

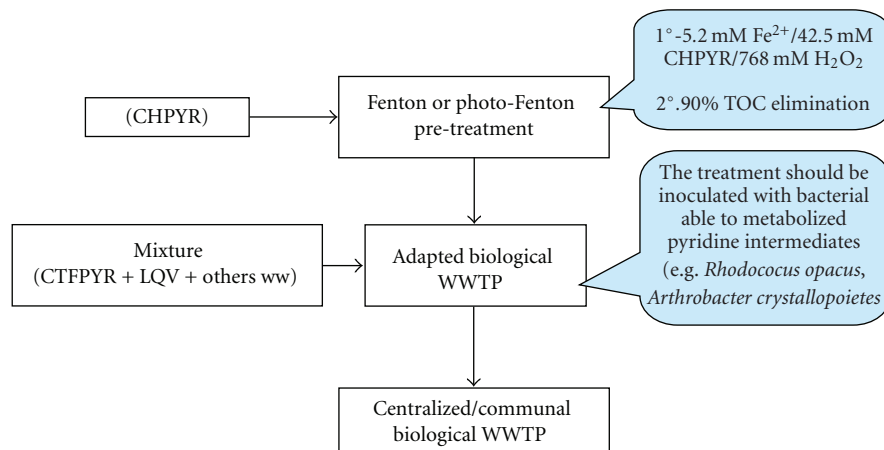


FIGURE 8: A proposed scheme of a diagram for the management of the studied effluents.

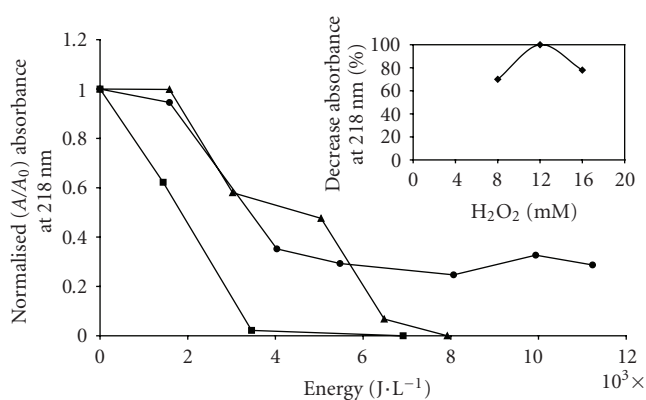


FIGURE 9: Relative absorbance of the phototreated Endosulfan contaminated water as a function of the specific energy. The H_2O_2 is varied from: (●) 8 mM, (■) 12 mM to (▲) 16 mM. The insert is percentage of relative degradation of the Endosulfan (monitored at 218 nm) when $6 \times 10^3 \text{ J} \cdot \text{L}^{-1}$ energy is accumulated in the photoreactor for the three H_2O_2 values tested.

be destroyed by photolysis and/or oxidation with oxygen from air [7]. The decrease of 40% of the absorbance at 218 nm as observed in Figure 9, does not inevitably mean that the Endosulfan is degraded, since it was shown that the molecule of Endosulfan is stable when exposed to solar radiation and the tests of stabilization for the commercial formulation of pesticides, taking into account the sunlight exposition aspects [8]. The effect of photolysis and aeration on the Endosulfan solution could be put into account of the degradation of the additives (emulsifiers and adherents).

Since the photocatalytic treatment is not considered as a cost effective process when compared to biological treatment [9–12], when taken into account the cost of hydrogen peroxide on the one hand, the technical choice of a treatment, total photochemical mineralization or coupling photochemical-biological processes, on the other hand, it is necessary to make a compromise over the optimal concentration of H_2O_2 and the duration of the treatment, by

considering the biodegradability of the phototreated effluent. In the case of this study, the choice was made on the lowest concentration of the peroxide (8 mM) with 0.18 Fe^{2+} mM for an initial concentration of 0.36 mM of Endosulfan, conditions within which, is that 50% of the biodegradability of the phototreated effluent is reached after 1 h30.

Assuming the relatively high value of the BOD_5/COD ratio noticed in Figure 7, one can conclude that the phototreated pesticide effluent containing Endosulfan can become biodegradable in the natural environment. However, it would be necessary to send such effluents into a biological wastewater treatment plant before they could be reused for any purpose or be rejected in the natural media (river, dam, or lake) following the scheme proposed in Figure 8. Otherwise, more studies need to be carried out, that is, by coupling photochemical and a biological process to oversee the complete degradation of endosulfan polluted water.

5. Conclusion

The difficulty and the complexity of treating real biorecalcitrant wastewaters were observed within the two studied cases. The increase of the biodegradability was observed after the photoFenton treatment of the effluent contaminated with Endosulfan but not with the CHPYR effluent. Thus, a total mineralization process is recommendable in the second case and rather an improvement of the biodegradability of the Endosulfan effluent.

The study on the pesticide effluent enables one to notice that the photolysis could lower by 30% the COD of the effluent (Figure 9) by contrast to the absence of COD decrease for a simple aeration.

In the two case studies, the helio-photoFenton process is effective proportionally to the amount of hydrogen peroxide added; but for economic reasons, a compromise should be made between the highest kinetics of the treatment process of the Endosulfan effluent and the overall objective (or strategy)

of the treatment, namely, the coupling of photochemical and biological processes which is a cost minimization option in the treatment strategies of biorecalcitrant wastewaters.

Is the high DBO₅/DCO ratio in the case of the photodegradation of Endosulfan effluent necessarily a good indicator to confirm the biotreatability of the phototreated effluent? Such a request could be looked out through very concise chemical analyses of the components of the effluents.

Eventually, this study shows a soft approach of transferring a laboratory high-tech context study to a field applied context within a North-South cooperation.

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