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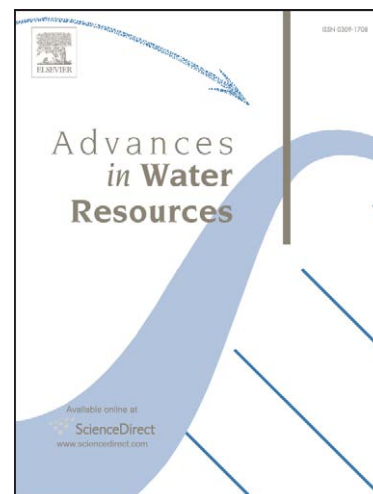
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3 **Effects of crab burrows on pore water flows in salt marshes**
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Abstract

24 Macro-pores such as crab burrows are found commonly distributed in salt marsh sediments.
25 Their disturbance on the soil structure is likely to influence both pore water flows and solute trans-
26 port in salt marshes; however, the effects of crab burrows are not well understood. Here, a
27 three-dimensional model simulated tidally driven pore water flows subject to the influence of crab
28 burrows in a marsh system. The model, based on Richards' equation, considered variably saturated
29 flow in the marsh with a two-layer soil configuration, as observed at the Chongming Dongtan wet-
30 land (Shanghai, China). The simulation results showed that crab burrows distributed in the upper
31 low-permeability soil layer, acting as preferential flow paths, affected pore water flows in the marsh
32 particularly when the contrast of hydraulic conductivity between the lower high-permeability soil
33 layer and the overlying low-permeability soils was high. The burrows were found to increase the
34 volume of tidally driven water exchange between the marsh soil and the tidal creek. The simulations
35 also showed improvement of soil aeration conditions in the presence of crab burrows. These effects
36 may lead to increased productivity of the marsh ecosystem and enhancement of its material ex-
37 change with coastal waters.

38 **Key words:** Coastal wetland; Plant growth; Numerical modelling; Preferential flow; Richards'
39 equation; Tidal forcing

40 **1. Introduction**

41 Salt marshes are important intertidal wetlands vegetated by herbs, grasses and/or low shrubs
42 [3,7,35]. Bordered with tidally dynamic coastal water bodies, salt marshes are affected by various
43 physical and biogeochemical processes that are associated with periodic submersions of marsh soils
44 by the tidal water. Among these processes, subsurface flow and solute transport largely determine
45 the marsh soil condition and material exchange with coastal waters [9,31,33,36]. The plant's
46 rhizosphere is within the intertidal zone, which undergoes cycles of immersion and emersion driven
47 by the tides. This leads to complex aeration conditions (for root aerobic respiration), which are cru-
48 cially important for plant growth [3,7,9,23]. Furthermore, the tidal inundation induces solute ex-
49 change across the marsh soil-water interface, which in turn influences the material budget of coastal
50 water ecosystems [34].

51 Recent hydrological studies on salt marshes based on numerical simulations focused on the
52 pore water circulation near tidal creeks. These studies have demonstrated links of tidally driven
53 subsurface flows with both marsh soil aeration and solute exchange [13,21,33,39]. The simulation
54 results suggested that during early stages of tidal submergence, surface water infiltrates almost ver-
55 tically through the marsh platform and decreases the soil aeration condition. The marsh soils may
56 then become depleted in oxygen. Such a condition would impact the plant root respiration and
57 hence plant growth [28]. As the tide recedes, a considerable amount of pore water seeps out of
58 marsh sediments near the creek bank. In contrast, little drainage takes place in the marsh interior.
59 Therefore, the optimal soil aeration condition tends to occur near the tidal creek. These simulation
60 results seem to give an explanation for previous observations that salt marsh plants such as *Spartina*
61 *alterniflora* often grow better near tidal creeks than in the inner areas [9,23]. The flow dynamics

62 with dominant infiltration through the marsh platform and drainage across the creek bank lead to a
63 net pore water flow in the form of circulation near the creek (Fig. 1). This pore water circulation at
64 the local scale provides a mechanism for more rapid solute exchange between the marsh soil and the
65 tidal creek than that given by diffusive processes through the marsh surface. The circulation ulti-
66 mately affects the overall material exchange between the marsh and coastal water.

67 Among the previous numerical studies, the Richards' equation-based model of Ursino et al.
68 [33] showed that if the soil's saturated hydraulic conductivity was relatively low (less than 10^{-6} m/s),
69 an unsaturated zone away from the creek would persist below the soil surface even after the tide had
70 flooded the marsh platform. Wilson and Gardner [38] pointed out that the boundary conditions
71 adopted by Ursino et al. [33] in their numerical simulations were unrealistic. However, Li et al. [21]
72 also revealed this persistent unsaturated zone in simulations using a two-phase model and more re-
73 alistic boundary conditions. Furthermore, they showed that the Ursino et al. [33] model could
74 over-predict infiltration in areas with trapped air. In other words, the persistent unsaturated zone
75 away from the creek could be more extensive than that calculated by Ursino et al. [33]. Such per-
76 manently aerated zones would allow a prolonged presence of oxygen for aerobic root respiration of
77 local plants in the marsh system.

78 These modelling studies [21,33,39] were all based on homogeneous soils. In reality, most
79 marshes possess soil strata. Commonly, low-permeability mud or silt loam are found to overlie
80 sands or sandy deposits in marsh systems, for example, the marsh at Carter Creek in Virginia [17],
81 the Manukau Harbour marsh in New Zealand [10], the Tomago South wetlands in Australia [19],
82 the North Inlet basin in Carolina [12] and the Bahía Blanca Estuary in Argentina [27]. Gardner [15]
83 reported perhaps the first numerical study on tidal dynamics of pore water flows in heterogeneous

84 marsh soils with a two-layer structure – a sand (high-permeability) layer underlying a mud
85 (low-permeability) layer. The study examined the effects of the soil structure on the spatial distribu-
86 tion and volume of seepage from marsh soils to the tidal creek. Simulation results showed that the
87 total seepage from the mud-sand marsh to the creek is larger than that from a muddy marsh. The
88 underlying sand layer enhances the pore water circulation through the marsh. As the contrast of hy-
89 draulic conductivity between the lower (sand) and upper (mud) layer increases, the total seepage
90 from the mud-sand marsh increases nonlinearly. The findings of this study also imply that the pres-
91 ence of an underlying sand layer with a higher permeability leads to lowering of the water table in
92 the upper mud layer during the ebb tide and hence improves local aeration conditions.

93 The other type of marsh soil heterogeneity is due to macro-pores produced by invertebrates
94 commonly found in salt marshes. For example, crab burrows are typically distributed in marsh
95 sediments [5,12,19,24,27]. The presence of invertebrates has implications for biogeochemical proc-
96 esses in marsh sediments. Through burrowing and feeding activities, the invertebrates are known to
97 increase sediment-water interface (surface area exposed to overlying water or air) and mixing be-
98 tween pore water and overlying surface water, thus affecting chemical reactions and transport in
99 marsh sediments [1,20]. Previous studies of marsh subsurface flows have developed hypotheses
100 about the roles of macro-pores like crab burrows. Nuttle [26] considered that the saturated hydraulic
101 conductivity of the marsh soil is controlled by its macro-pore structure, which is itself biotically
102 controlled. Montalto et al. [25] further suggested that preferential flow may be facilitated by
103 macro-pores. These hypotheses were tested indirectly by Harvey and Nuttle [18] through tracer ex-
104 periments.

105 Despite these previous studies, the effects of macro-pores on the marsh system and underlying

106 mechanisms are not fully understood. With considerable disturbance on the soil structure, how crab
107 burrows may affect pore water flows and associated soil aeration conditions in the marsh remains
108 an important question; as discussed above both factors control a large extent the soil's biogeo-
109 chemical condition and hence plant growth. To address this question, we conducted a field investi-
110 gation on a salt marsh at the Chongming Dongtan wetland (Shanghai, China) where a sandy loam
111 layer with relatively high hydraulic conductivity underlies a surface mud layer, similarly to the
112 model configuration considered by Gardner [15]. However, the difference is that, at this field site,
113 there is a relatively large number of crab burrows down to the bottom of the upper mud layer
114 (around 60 cm below the marsh surface). While the reason why the crabs tunnel to this depth is un-
115 clear, the burrows penetrating the mud layer may act as preferential flow paths for water. These
116 burrows may change not only the behaviour of pore water flows but also associated aeration condi-
117 tions and solute exchange in the marsh soil. For example, the permanently unsaturated zones sug-
118 gested by Ursino et al. [33] may not exist in marsh soils in the presence of crab burrows. Moreover,
119 the pore water circulation demonstrated by previous studies [13,15,21,33] is likely to be altered by
120 widespread macro-pores like crab burrows.

121 The aim of this study is to develop a three-dimensional model to investigate pore water flows
122 in marsh soils affected by crab burrows. The model was based on a simplified tidal marsh configu-
123 ration using data collected from the Chongming Dongtan wetland. In the model, a low-permeability
124 soil layer overlies a high-permeability soil layer. Crab burrows were distributed in the upper soil
125 layer according to the measured density at the field site. Numerical simulations were conducted to
126 generate insight into effects of crab burrows on pore water flows and associated water exchange,
127 soil aeration and tidal signal propagation under different conditions of varying hydraulic conductiv-

128 ity contrast between the lower and upper soil layer (K_{lower}/K_{upper}).

129 **2. Field investigation**

130 The field site is located at the Chongming Dongtan wetland (between $31^{\circ}25' \sim 31^{\circ}38' \text{ N}$ and
131 $121^{\circ}50' \sim 122^{\circ}05' \text{ E}$) on the eastern part of the Chongming island (Shanghai, China), the largest is-
132 land in the Yangtze delta area (Fig. 1a). The tidal flats at the site are dominated by various marsh
133 plants, such as *Phragmites australis*, *Scirpus mariqueter* and *Spartina alterniflora* [11]. The Yang-
134 tze estuary experiences semidiurnal and mixed tidal fluctuations with a maximum range around
135 4.64 m [8]. The tidal signal is attenuated significantly due to friction as it propagates along the tidal
136 creek at the study site and exhibits high degree of asymmetry with a much more rapid rising phase
137 than falling phase. During spring tides, the maximum range of creek water level fluctuations at the
138 study site is about 1.0 m (mainly depending on the elevation of the creek bottom). For this condition,
139 the local marsh platform is inundated at high tide with a water depth around 0.1 m (this depth vary-
140 ing with the marsh topography, wind and vegetation coverage).

141 As discussed in the introduction, macro-pores such as crab burrows are a dominant feature of
142 soils in the intertidal zone. At the field site, burrows near creeks are often dug by *Uca arcuata* (crab
143 species shown at the lower left corner of Fig. 1b). According to our observations, the crabs can dig
144 burrows up to 10-cm deep in no more than 2 h without interference. We collected data at the site
145 during a neap tide (9 July 2007). Along a cross-creek transect (dashed line in Fig. 1b), 109 crab
146 burrows of diameters between 1 and 2 cm were found over an area of $14 \text{ m} \times 1.5 \text{ m}$. The areal bur-
147 row density (number of burrows per square meter area) for this size range was $5.2/\text{m}^2$. Another 68
148 crab burrows of diameters between 2 and 4 cm were also found. The corresponding areal burrow
149 density was $3.2/\text{m}^2$. There were many smaller burrows not included in the survey. These burrows

150 are likely to have less important effects on the pore water flow compared with those described al-
151 ready. Therefore, these small burrows were neglected in the study.

152 The morphological structures of these burrows were determined by means of polyester resin
153 casting, a technique often used in the marine industry [4,32]. At low tide, randomly selected bur-
154 rows were filled with resin. The polyester resin is denser than seawater and can harden even in wet
155 conditions; therefore, water inside the burrow was pumped out before pouring the resin in order to
156 create a complete cast of the burrow. The cast was later excavated by hand and with small shovels
157 after resin solidified, and then cleaned and examined.

158 When the burrow casts were excavated, the difference in soil texture between two layers was
159 evident. Black, odoriferous soils were found underneath the 60-cm surface mud layer (Fig. 1c,
160 varying spatially and temporally). Soil samples were collected from each layer and later analysed in
161 the laboratory for the hydraulic conductivity (falling head method), porosity (oven drying) and par-
162 ticle size distribution (laser diffraction particle analysis). The soil particle size distribution ranged
163 from 0.36 μm to 140.58 μm . The soils from the lower layer contained larger particles than the upper
164 layer soils. The average hydraulic conductivity and porosity of the upper soils were determined to
165 be 1.18×10^{-6} m/s and 0.51, respectively (6 soil samples), and 6.25×10^{-6} m/s and 0.51 respectively
166 for soils from the lower layer (also 6 samples). Such a layered soil structure was the focus of Gard-
167 ner's [15] numerical study on pore water flows in heterogeneous marsh soils. The crab burrows dis-
168 tributed extensively at the field site represent important, additional heterogeneity of marsh soils.
169 According to our measurements, the average length of the burrows is about 40 cm. Nearly half of
170 the surveyed burrows are, however, longer than 60 cm with the maximum length reaching 70 cm
171 (Fig. 1d). Deep burrows penetrate through the upper soil layer and may act as preferential flow

172 paths, affecting pore water flows and associated aeration conditions in marsh soils.

173 Crab burrows were not distributed regularly in the marsh; nor did they possess regular shapes
174 (Fig. 1d). Moreover, the dimensions of the burrows varied both spatially and temporally due to
175 crabs' continuing activities of burrowing and feeding. Therefore, it is difficult to deploy pressure
176 transducers in these burrows to measure water pressure fluctuations in response to tides. Quantita-
177 tive analyses based on mathematical models with precise information about burrows (location, size
178 and layout) would not be feasible as it is impractical to acquire such information and use it to create
179 the mesh required by the simulations. Here, we adopted an alternative approach by developing a
180 representative model of the marsh system with simplified configurations assuming vertical burrows
181 of a constant length (equal to the thickness of the upper soil layer) and regular distribution in the
182 upper soil layer (Fig. 1e). This approach reflects key features of the marsh system and serves the
183 purpose of the study to examine general effects of crab burrows as potentially important preferential
184 flow paths.

185 **3. Conceptual and mathematical models**

186 *3.1. Physical conditions*

187 Based on the field site configuration, the three-dimensional model developed here was as-
188 sumed to lie between two parallel tidal creeks and extend in the along-creek (y) direction by a width
189 of $W = 0.5$ m (Fig. 1e). The model domain, with a simplified geometry as indicated by the central
190 vertical cross-section **ABCDEFG** (reference point coordinates are given in Table 1), reflects the
191 topography of the field site. **DE** shows the marsh platform and **AG** is for the impermeable base. **BD**
192 represents the creek bank with a slope similar to that of the creek profile measured at the field site.
193 No creek bottom section is present in the model, i.e., a triangular creek cross-section was assumed

194 (based on the configuration at the field site). The domain is divided into two zones (Zone A and
 195 Zone B shown in Fig. 1e) separated by a horizontal interface **CF** at the depth of 0.6 m from the
 196 marsh platform.

197 Crab burrows were assumed to be distributed along the centreline of the model domain as
 198 shown in Fig. 1e and penetrate straight through the upper soil layer (Zone A). The spatial interval of
 199 crab burrows L was set to 0.5 m, giving an areal crab burrow density of $4/\text{m}^2$. Because not all
 200 measured burrows were deep enough to penetrate the upper soil layer, the burrow density set in the
 201 model was approximately half of that measured at the field site. To generate a 3-D rectangular fi-
 202 nite-element mesh that can be used in SUTRA (the modelling software used in the study), each crab
 203 borrow was assumed to be a cube with the size of $4 \text{ cm} \times 4 \text{ cm} \times 60 \text{ cm}$. The size of simulated bur-
 204 rows reflects the upper end of the size range measured in the field.

205 For the purpose of comparison with previous modelling work [15,21,33], we adopted a sinu-
 206 soidal tide as the forcing condition in the model instead of using the measured tidal signal at the
 207 field site, i.e.,

$$208 \quad h(t) = Z_{MSL} + A \cos(\omega t), \quad (1)$$

209 where $h(t)$ is the water level in the creek [L], t is the time [T], Z_{MSL} is the mean water level in
 210 the creek [L], A is the amplitude of tide-induced water level oscillations in the creek [L] and ω
 211 is the tidal angular frequency [T^{-1}].

212 In all simulations, the same tide with amplitude of 0.5 m and period of 12 h ($\omega = \pi/6 \text{ rad/h}$)
 213 was set. The mean creek water level was set to 1.6 m, which allowed the marsh platform to be in-
 214 undated with a water depth of 0.1 m at high tide.

215 3.2. Mathematical description and numerical method

216 The variably saturated pore water flow in the marsh soil is governed by Richards' equation:

$$217 \quad \nabla \cdot [K(\psi) \nabla \Phi] = \frac{\partial \theta}{\partial t}, \quad (2)$$

218 where Φ is the total hydraulic head, and $\Phi = \psi + z$ [L]; ψ is the capillary pressure head [L]; z
 219 is the elevation [L]; $K(\psi)$ is the relative hydraulic conductivity [L/T]; and θ is the volumetric
 220 moisture content, $= \phi_w$ (ϕ is the soil porosity and S_w is the soil saturation). The relationship be-
 221 tween the hydraulic conductivity, soil saturation and capillary pressure head is given below accord-
 222 ing to Gardner [16]:

$$223 \quad K(\psi) = K_s \exp(\alpha \psi), \quad (3)$$

$$224 \quad S_w = (1 - S_{wres}) \exp(\alpha \psi) + S_{wres}, \quad (4)$$

225 where K_s is the saturated hydraulic conductivity [L/T], α is the inverse of the mean capillary
 226 rise [L^{-1}] and S_{wres} is the residual water saturation.

227 It is worth recalling that Richards' equation is valid when pressure gradients in the air phase
 228 are insignificant compared with those in the water phase. Due to the large viscosity difference be-
 229 tween air and water, this condition is reasonable except when the air becomes trapped [21]. For all
 230 the cases modelled in the present study, no persistent unsaturated zone with air trapped was present
 231 due to crab burrows which provide the means for air to be easily displaced. Therefore, the use of
 232 Richards' equation is appropriate.

233 We assumed constant pore water density in the model, which is consistent with measurements
 234 of small density variations at the field site. Also we neglected in equation (2) the change of aquifer
 235 storage due to the compressibility of fluid and soil matrix. The standard formulation of the com-
 236 pressibility terms is based on the assumption of constant total stress on the porous medium and
 237 hence $\Delta \sigma$ (change of effective stress) = $-\Delta P$ (change of pore water pressure). When the salt marsh is

238 flooded at high tides, fluctuations of pore water pressure with varying depth of overlying water
239 would lead to changes of effective stress under the assumption of constant total stress, generating an
240 artificial pressure wave through the elastic soil. However, the total stress on the marsh soil is not
241 constant during flooding and varies in the same way as the pore water pressure, thus giving invari-
242 ant effective stress (i.e., no expansion or contraction of soil matrix). To account for the total stress
243 variation and remove the artificial pressure wave, a tidal loading term needs to be incorporated into
244 Richards' equation with the standard compressibility formulation [29]. Our numerical tests showed
245 that if the saturated hydraulic conductivity of soils is large than 10^{-6} m/s, the compressibility plays a
246 negligible role in governing the pore water flow in the marsh soil. Therefore, an alternative, simpler
247 approach is to neglect the compressibility terms in the governing equation, in which case the tidal
248 loading modification is no longer required [29]. This approach is valid only if the effect of fluid and
249 solid compressibility on the pore water flow in the marsh soil is negligible [14].

250 Crab burrows were included in the model as highly conductive zones with saturated hydraulic
251 conductivity $K_s = 10$ m/s and porosity $\phi = 1$. This enables simulations of the burrows' rapid re-
252 sponses to tidal water level fluctuations. Numerical tests showed that as long as the hydraulic con-
253 ductivity of the burrows is set high enough (≥ 10 m/s), its value does not affect the simulation re-
254 sults. Similar techniques have been previously used in groundwater models to simulate dynamic
255 conditions induced by surface water [2,22,30].

256 The governing equation was solved using the SUTRA code, a 3-D finite element computer
257 program that simulates partially saturated, variable-density fluid flow, and solute or energy trans-
258 port in porous media [37]. Modifications of the code were made in order to implement the tidally
259 influenced boundary condition along the creek bank (boundary **BD**) and marsh platform (boundary

260 **DE**).

261 *3.3. Initial and boundary conditions*

262 The initial condition was set according to the hydrostatic pressure determined by the water
263 level at the high tide. All the simulations were run for a relatively long period to ensure that the
264 numerical solutions reached a quasi-steady state (i.e., periodic solutions unaffected by the initial
265 condition).

266 Boundaries **AB**, **AG** and **EG** together with two side-boundaries in the along-creek direction
267 were treated as no flow boundaries. SUTRA was modified to simulate the tidally dynamic boundary
268 condition along the creek bank (**BD**) and marsh platform (**DE**). A subroutine was set up to deter-
269 mine the state of each node on these boundaries at every time step. On the marsh platform, the
270 nodal heads were prescribed by hydrostatic pressure given by depth of overlying water. These
271 nodes switched to no-flux boundaries in the absence of overlying water. In SUTRA, the pres-
272 sure-prescribed boundary condition was implemented by connecting the boundary node to a “res-
273 ervoir” with specified pressure through a “conduit” of very large conductance. This method gives a
274 simple switch between each boundary condition type by setting the conductance to zero when the
275 zero-flux condition applies. Similarly, the tidally dynamic boundary condition was implemented
276 along the creek bank, allowing also for the development of a seepage face defined by the rule: If the
277 nodes above the tidal water level were saturated at the previous time step, they were taken as seep-
278 age face nodes with the atmospheric pressure [39].

279 *3.4. Parameters values used in the simulations*

280 The parameter values used in the base simulation were set to reflect the field conditions at the

281 study site. The soil porosity was 0.51 for both layers. The hydraulic conductivities of upper and
282 lower soils were 1.18×10^{-6} m/s and 6.25×10^{-6} m/s, respectively. The inverse of mean capillary rise
283 and residual saturation were 1 m^{-1} and 0.3 respectively for both upper and lower soils. Although
284 these values were not directly from measurements, they are consistent with the soils types encoun-
285 tered at the field site [6]. Values of other model parameters concerning the simulation domain, bur-
286 rows and tidal forcing have been given in §3.1.

287 To compare with the base simulation, a set of numerical experiments were conducted to ex-
288 amine the effects of crab burrows on pore water flows in salt marshes under different soil layer
289 conditions. The hydraulic conductivity of the lower layer was varied between 1.18×10^{-6} m/s and
290 6.25×10^{-5} m/s, giving a range of hydraulic conductivity contrast between the two soil layers with
291 K_{lower}/K_{upper} varying from 1 to 53, thereby considering a range from a homogeneous soil to one with
292 a large hydraulic conductivity contrast.

293 For all simulations, the SUTRA code was run with a time step of a minute. The same mesh
294 generated with 135,408 nodes and 120,600 elements was used in all cases. Typically, the burrow
295 zones were refined so that each burrow was represented by 240 elements. Tests on the simulation's
296 independence of time step and mesh size were conducted. The results based on the present model
297 setting were found to agree well with those from models with a further refined mesh and smaller
298 time step. In other words, the results presented here are considered to be converged numerical solu-
299 tions to the mathematical model.

300 **4. Simulation results and discussions**

301 *4.1. Effects on pore water flow dynamics*

302 The simulated pore water flow is generally three-dimensional, especially in areas near the crab

303 burrows. However, due to symmetry, the flow on the vertical plane along the model's centreline
304 (ABCDEF) is two-dimensional. Since key flow characteristics are expected to be
305 two-dimensional in the vertical and creek-normal direction, the discussion below will first focus on
306 such two-dimensional flows. For the purpose of comparison, reference simulations were also con-
307 ducted without crab burrows distributed in the marsh.

308 Simulation results show that for the base condition, the pore water flow velocities at high tide
309 were very low in both cases (with and without burrows included; Fig. 2a). This indicates that the
310 pore water pressure in the marsh soil was largely hydrostatic. No unsaturated zone was present in
311 either case.

312 As the tide receded, pore water flow developed within 10 m from the creek. The flow activity
313 was weakened with increasing distance from the creek, consistent with the attenuation of associated
314 tidal groundwater waves (Fig. 2b). Overall the flow rate in the upper soil layer was small due to the
315 relatively low hydraulic conductivity. Significant downward flows appeared at the lower end of the
316 burrows near the interface between the two soil layers, suggesting that the burrows acted as prefer-
317 ential flow paths and enhanced locally the drainage of the upper soils with collected water dis-
318 charging to the lower soil layer. This effect can be seen more clearly in Fig. 3 where flow velocities
319 are plotted for two observation points in the upper layer near the burrow next to the creek: one be-
320 tween the burrow and the creek (left hand side of the burrow), and the other landward of the burrow
321 (right hand side of the burrow). The flows at both observation points were affected significantly by
322 the burrow when compared with the result from the reference simulation (without the burrows).
323 During the ebb tide (between elapsed time 4 and 8 h), the horizontal flow velocity at the left hand
324 side observation point reversed its direction while the magnitude of the vertical flow velocity was

325 reduced significantly (Fig. 3a in comparison with Fig. 3c). On the right hand side, the horizontal
326 flow velocity increased slightly with a relatively large reduction of the vertical flow for this period
327 (Fig. 3b in comparison with Fig. 3d). These changes of local flow patterns indicate that considerable
328 water from the upper soil layer was drained into the lower layer through the burrows.

329 At the low tide, the flows were intensified in both cases (Fig. 2c). As the outflow area moved
330 towards the low tide limit, the characteristics of dominant vertical and horizontal flows in the upper
331 and lower layers respectively became pronounced, and so did the effect of crab burrows on the
332 flows.

333 On the rising tide, inflow (from the creek to the marsh soil) occurred below the intersection of
334 the tidal water level with the creek bank (Fig. 2d). Relatively large upward pore water flows devel-
335 oped near the lower end of the burrows, suggesting that the burrows again acted as preferential flow
336 paths. Since the tidal signal propagated more quickly in the lower more permeable layer, the pres-
337 ence of the burrows with “large hydraulic conductivity” could lead to leakage of tidal energy to the
338 upper layer.

339 At the beginning of the flooding over the marsh platform, the flow velocities at the observa-
340 tion points on both sides of the near-creek burrow surged (Fig. 3). This indicates that the overtop-
341 ping water irrigated quickly the burrows and subsequently flowed into the surrounding marsh soils.
342 This has implications for the behaviour of local soil water saturation and aeration condition as dis-
343 cussed further in §4.3.

344 Focussing on the area around the burrow next to the creek, we examined flows on the y - z
345 plane across the centre of the burrow, which demonstrate the flow’s three-dimensionality (Fig. 4).
346 The effects of the burrow on flows in the y and z direction (Figs. 4a-c) were similar to those dis-

347 cussed above (Figs. 4e-g). In essence, the burrow acts like a drain for the upper soils during the ebb
348 tide and a recharge well during the rising tide. However, the drainage effect seems to be more pro-
349 nounced as indicated by the averaged flows over the tidal cycle (Figs. 4d and h; further discussion
350 on the averaged flows is given below).

351 4.2. *Effects on water exchange between marsh soils and creek*

352 Previous studies have suggested that the tide induces pore water circulation near the creek
353 with surface water infiltrating through the marsh platform and discharging from the creek bank. To
354 examine effects of crab burrows on the pore water circulation, we averaged the simulated pore wa-
355 ter flows over a tidal cycle. The tidally averaged flows exhibited circulation patterns as expected for
356 both cases (Fig. 5). While net inflow occurred over the upper part of the creek bank and across the
357 marsh platform, net outflow concentrated between the bank's intersection with the soil layer inter-
358 face and the low tide limit. The overall water passage was characterised by downward movement
359 through the upper soils followed by seaward flow in the lower soil layer prior to discharge to the
360 creek. Increased average downward flows at the bottom of the crab burrows again indicated prefer-
361 ential flow paths through these burrows, which enhanced downward water movement in nearby ar-
362 eas. This may result in increase of the overall circulation rate and hence exchange between the
363 marsh soil and the creek.

364 Based on the average flow velocities, we calculated the difference between the total volume of
365 inflow and outflow across the creek bank over a tidal cycle. This quantity represents the net ex-
366 change between the marsh soil and the creek. The net exchange was 0.015 m^3 (0.030 m^3 per meter
367 distance along the creek) for the case with crab burrows and 0.014 m^3 (0.028 m^3 per meter distance
368 along the creek) without crab burrows. The presence of crab burrows led to a slight increase of the

369 net exchange by 3.5%. Although the effect is small for the simulated base condition, the enhance-
370 ment of exchange may become more significant with increased burrow density and hydraulic con-
371 ductivity contrast between the soil layers. A series of simulations were conducted with the hydraulic
372 conductivity contrast between the layers varying as described above.

373 Simulation results showed that for a homogeneous soil ($K_{lower}/K_{upper} = 1$), the tide-induced
374 water exchange was only slightly affected by crab burrows. Although the burrows had much higher
375 hydraulic conductivity than that of the soil, they occupied a very small volume of the medium and
376 thus by themselves affected little the overall pore water flow. As K_{lower}/K_{upper} increased, the total
377 water exchange volume increased for both cases with and without crab burrows in a similar fashion
378 (Fig. 6). However, the increase of exchange for the marsh system with crab burrows was more sub-
379 stantial. The relative difference of total water exchange volume between the two cases was calcu-
380 lated and found to increase with K_{lower}/K_{upper} . The effects of crab burrows on the pore water flow
381 and exchange in the marsh were intensified as the hydraulic conductivity contrast between the two
382 soil layers increased. Compared with the homogeneous configuration, the additional water ex-
383 change induced by crab burrows was 15.4% for $K_{lower}/K_{upper} = 53$. This hydraulic conductivity con-
384 trast is not uncommon in natural salt marshes [15].

385 4.3. *Effects on soil aeration conditions*

386 To examine effects of crab burrows on water saturation in the marsh soil, we focussed on the
387 area near the burrow next to the creek on the vertical plane along the centreline. Results from the
388 base condition simulations are shown in Fig. 7. The marsh soil was largely fully saturated except for
389 the near-surface area where the saturation varied with the tidal stage. At high tide, the marsh soil
390 was fully saturated (result not shown). As the tide receded, the near-surface soil became partially

391 saturated in both cases with and without the burrow (Figs. 7a and f). However, the presence of the
392 burrow led to further reduction of the saturation around it with a down-coning profile evident (Fig.
393 7a). This is consistent with the drainage effect of the burrow on the pore water flow in the upper soil
394 layer as discussed in §4.2. This effect was intensified as the low tide approached (Fig. 7b). On the
395 rising tide, the saturation profile rebounded (Fig. 7c) due to increase of hydraulic head in the burrow
396 in response to the tide that propagated through the lower soil layer more quickly than in the upper
397 layer. As the tidal water level rose just above the marsh platform, the flooding water filled the bur-
398 row immediately and subsequently infiltrated the soil around the burrow over the depth, resulting in
399 increase of local saturation to 100% (Fig. 7d).

400 The opposing effects of the burrow on local soil saturation during the rising and falling tide
401 were not even. Tidally averaged soil saturation profiles showed that overall the burrow reduced lo-
402 cal soil saturation (Fig. 7e). The reduction was relatively small for the base condition. However,
403 more pronounced effects were observed in simulations with a large hydraulic conductivity contrast
404 between the layers, as shown in Fig. 8 for $K_{lower}/K_{upper} = 53$. On average, the depth of partially satu-
405 rated zone increased due to the presence of crab burrows. A reduction of local soil saturation oc-
406 curred in areas around all crab burrows although the effects were attenuated with increasing dis-
407 tance from the creek. This reduction of soil water saturation may be linked to improvement of soil
408 aeration and hence plant growth.

409 *4.4. Effects on pore water pressure fluctuations*

410 The effects of crab burrows on pore water flow and soil water saturation as discussed above
411 are fundamentally due to burrow-induced modifications of the pore water pressure (hydraulic head)
412 field. To examine such modifications, we again focussed on the area around the burrow next to the

413 creek where the burrow effects were the most profound. Pore water pressure (head) distributions
414 underneath the burrow were first examined. Results showed pressure increase and decrease around
415 the burrow's centre on the falling and rising tide, respectively (compare Figs. 9a,b with Figs. 9c,d).
416 These pressure profiles correspond to significant outflow from and inflow to the burrow previously
417 observed near the lower end of the burrow on these tidal stages (Fig. 4).

418 We also examined the hydraulic head fluctuations at two observation points: one inside the
419 burrow (Fig. 10a) and the other underneath (Fig. 10b). The hydraulic head at the observation point
420 inside the burrow declined more quickly with the receding tide compared with the signal from the
421 reference simulation (without burrows). The opposite trend, however, was found at the observation
422 point underneath the burrow, which exhibited a slower decline of the hydraulic head as the tide re-
423 ceded. These results are consistent with the local flow characteristics – the burrows collected pore
424 water in the upper layer and discharged it into the lower layer. The other distinctive modification of
425 the hydraulic head behaviour by the burrow was the instantaneous rise of the head to the tidal water
426 level at the instant of flooding over the marsh platform at both observation points, suggesting im-
427 mediate filling of the burrow by the flooding water. The subsequent changes of local soil saturation,
428 which have been discussed in the above section, suggest that if crab burrows exist in the marsh
429 sediments, the persistent unsaturated zones identified previously [33] may not exist in the marsh
430 soils due to increased surface water irrigation through the burrows during overtopping.

431 **5. Conclusions**

432 Crab burrows are a common feature of many salt marshes. Their effects on enhanced disper-
433 sion and bioturbation in marshes have been studied previously. Here, we have developed a
434 three-dimensional model to examine a new mechanism by which crab burrows may affect signifi-

435 cantly the marsh system in the exchange of the coastal water and the atmosphere. The Richards'
436 equation-based model simulates tidally driven, variably saturated pore water flow in the marsh soil
437 along with the disturbance due to crab burrows.

438 In parallel with numerical modelling, we have carried out a field investigation with measure-
439 ments of crab burrow density, distribution and size at the Chongming Dongtan wetland (Shanghai,
440 China). The marsh soil at the field site is characterised by a two-layer structure, also a common
441 feature of salt marshes: an upper mud layer (low hydraulic conductivity) and a lower sandy loam
442 layer (high hydraulic conductivity). Many of the surveyed burrows were found to penetrate the up-
443 per mud layer and could potentially be preferential flow paths between the two soil layers.

444 Model simulations based on field measurements and a wider range of conditions demonstrated
445 that crab burrows acted as a drain for the upper soil layer during the ebb tide and a recharge well on
446 the rising tide. However, the opposing effects did cancel each other out but instead resulted in an
447 increase of pore water circulation across the marsh soil-water interface and reduction of average soil
448 water saturation at shallow depths. Increased pore water circulation may lead to enhancement of
449 solute exchange between the marsh soil and tidal creek, and prevent overly high pore water solute
450 concentrations. At the same time, reduced soil water saturation is likely to improve soil aeration.
451 Therefore the presence of crab burrows is likely to be in favour of the plant growth and hence in-
452 crease the productivity of salt marshes.

453 Although we have not been able to measure the simulated crab burrow effects in our prelimi-
454 nary field investigation, the modelling study has provided important insight into the physical proc-
455 esses. A large hydraulic conductivity contrast between the shallow and deep soil layers has been
456 found to be an essential factor that underpins the role of crab burrows in modifying the conditions

457 and behaviour of water flow in salt marshes. The characteristics of pore water pressure under the
458 influence of crab burrows revealed here will provide a base for designing future experimental stud-
459 ies on crab burrow effects. It will be a challenge to collect detailed data of hydraulic head fluctua-
460 tions in and around crab burrows at the field site to validate model predictions. More complex mod-
461 els are needed to study further the effects of crab burrows coupled with other factors including the
462 marsh topography (e.g., a vertical creek bank), multiple tidal constituents (e.g., spring-neap tides),
463 long period seasonal water level oscillations, precipitation and evapotranspiration. Furthermore, the
464 effects caused by temporal and spatial variations in burrow sizes and their distribution may also be
465 important for pore water flows in salt marshes. All these challenges present useful directions for fu-
466 ture investigations on salt marshes.

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548 **Notation**

549	A	tidal amplitude [L]
550	H	crab burrow depth [L]
551	$h(t)$	tidal water level at time t [L]
552	K_{lower}/K_{upper}	hydraulic conductivity contrast between the lower and upper soil layer
553	K_s	saturated hydraulic conductivity [L/T]
554	$K(\psi)$	relative hydraulic conductivity [L/T]
555	L	interval of crab burrows [L]
556	S_w	water saturation
557	S_{wres}	residual water saturation
558	t	time [T]
559	W	width of the modelled salt marsh [L]
560	x	distance from the tidal creek [L]
561	y	distance along the tidal creek [L].
562	z	elevation [L]
563	Z_{MSL}	mean sea level [L]
564	α	inverse of the mean capillary rise [L ⁻¹]
565	ω	angular frequency [T ⁻¹]
566	ψ	capillary pressure head [L]
567	θ	water content

568

Table 1. Coordinates of reference points of the model domain (x, z).

A (m)	B (m)	C (m)	D (m)	E (m)	F (m)	G (m)
(0, 0)	(0, 1)	(1.8, 1.6)	(4.5, 2)	(24.5, 2)	(24.5, 1.6)	(24.5, 0)

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Figure Captions

- 570 Fig. 1. a) Location of the study area within the Chongming Dongtan wetland. b) Location of
571 the studied tidal creek. An *Uca arcuata* crab is shown at the lower left corner.
572 Dashed line indicates the surveyed area. c) Marsh soil stratigraphy. Soils with rela-
573 tively high hydraulic conductivity were found underneath overlying mud. d) Mor-
574 phology of a casted crab burrow. e) Three-dimensional schematic diagram of the
575 modelled salt marsh. **ABCDEFG** represents the central section across the creek
576 where crab burrows are distributed. The pore water circulation is also illustrated.
- 577 Fig. 2. Flow velocity at high tide (a, elapsed time 0 h), falling tide (b, elapsed time 3 h), low
578 tide (c, elapsed time 6 h) and rising tide (d, elapsed time 10 h). All figures show the
579 two-dimensional flows in the x and z direction on the central section where burrows
580 are distributed ($y = 0.25$ m). The upper panel is for the case without crab burrows;
581 and the lower panel is for the case with crab burrows. The ∇ symbol indicates the
582 water level in the tidal creek.
- 583 Fig. 3. Time series of flow velocity at two observation points. The plot on the left hand side
584 is for the observation point located on the left hand side of the nearest burrow to the
585 creek ($x = 4.693$ m, $y = 0.25$ m, $z = 1.725$ m). The right hand side plot is for the ob-
586 servation point located on the right hand side of the nearest burrow to the creek ($x =$
587 4.816 m, $y = 0.25$ m, $z = 1.725$ m). a) and b) are for the case without crab burrows. c)
588 and d) are for the case with crab burrows. The period between the two vertical dotted
589 lines represents the emersion period.
- 590 Fig. 4. Flows in the y and z direction on the vertical along-creek section through the centre

591 of the nearest burrow to the creek. Results are shown for three tidal stages: falling
592 tide (a, elapsed time 3 h), low tide (b, elapsed time 6 h) and rising tide (c, elapsed
593 time 10 h). For comparison, flows in the x and z direction on the vertical cross-creek
594 section through the centre of the burrow are also shown (e, f and g). Tidally averaged
595 flows are shown in d) and h).

596 Fig. 5. Tidally averaged flows on the central cross-creek section ($y = 0.25$ m) for the case
597 without burrows (upper panel) and with burrows (lower panel).

598 Fig. 6. Total water exchange volume per meter distance along the creek over a tidal cycle
599 versus the hydraulic conductivity contrast (K_{lower}/K_{upper}).

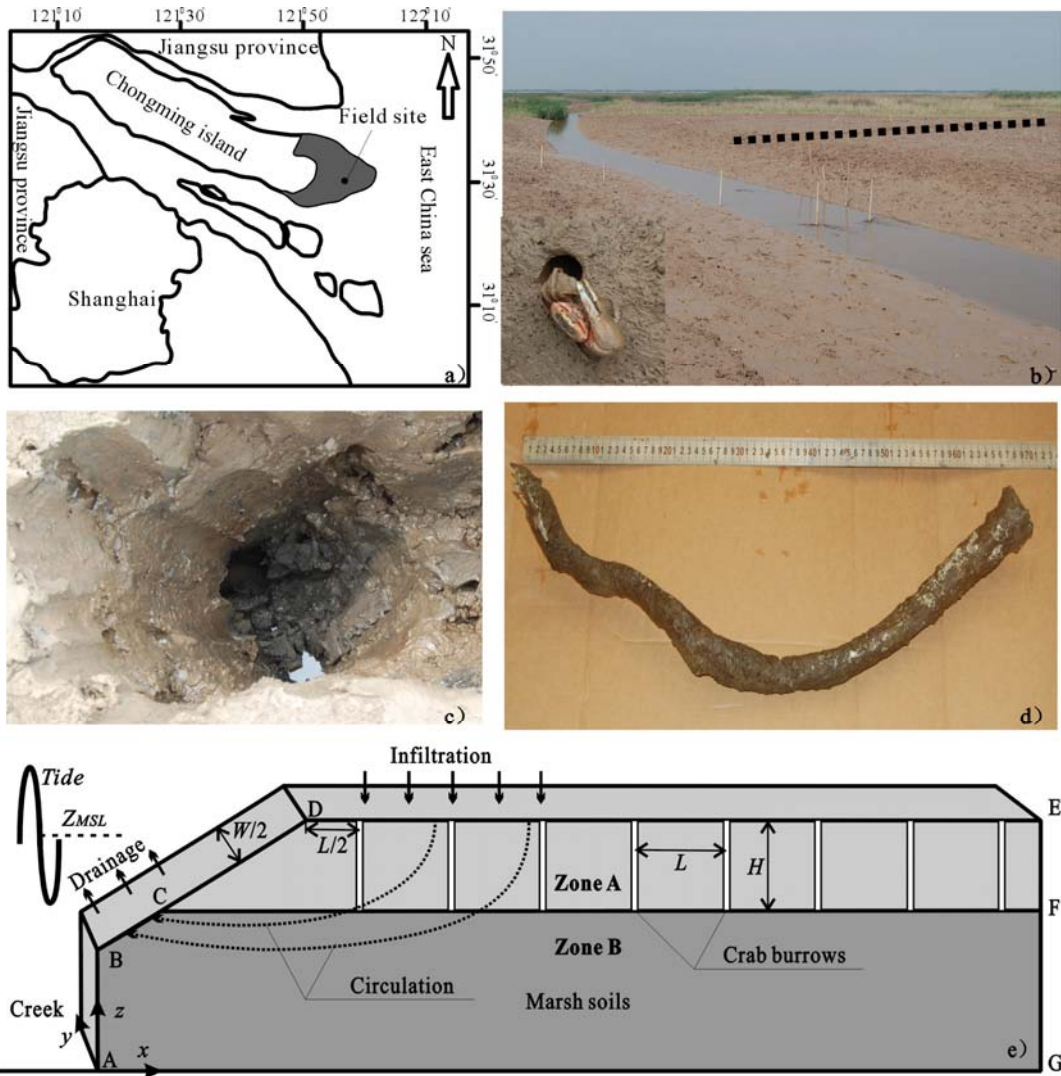
600 Fig. 7. Saturation profiles in areas near the burrow next to the creek (on the central section,
601 $y = 0.25$ m) at four different tidal stages: falling tide (a, elapsed time 3 h), low tide (b,
602 elapsed time 6 h), rising tide (c, elapsed time 9 h) and beginning of overtopping (d,
603 elapsed time 11 h). For comparison, results from the reference simulation without
604 crab burrows are also shown (f, g, h and i). Tidally averaged saturation profiles are
605 displayed in e) and j).

606 Fig. 8. Averaged saturation profiles over a tidal cycle (on the central section, $y = 0.25$ m) for
607 $K_{upper} = 1.18 \times 10^{-6}$ m/s and $K_{lower} = 6.25 \times 10^{-5}$ m/s ($K_{lower}/K_{upper} = 53$). The upper
608 panel is for the case without crab burrows; and the lower panel is for the case with
609 crab burrows.

610 Fig. 9. Pore water pressure (head) profiles in areas below the nearest burrow to the creek
611 (on the central section) at two different tidal stages: ebb tide (a, elapsed time 3 h) and
612 rising tide (b, elapsed time 10 h). For comparison, results from the reference simula-

613 tion without crab burrows are also shown (c and d). Results are for $K_{upper} = 1.18 \times$
614 10^{-6} m/s, $K_{lower} = 1.18 \times 10^{-5}$ m/s.

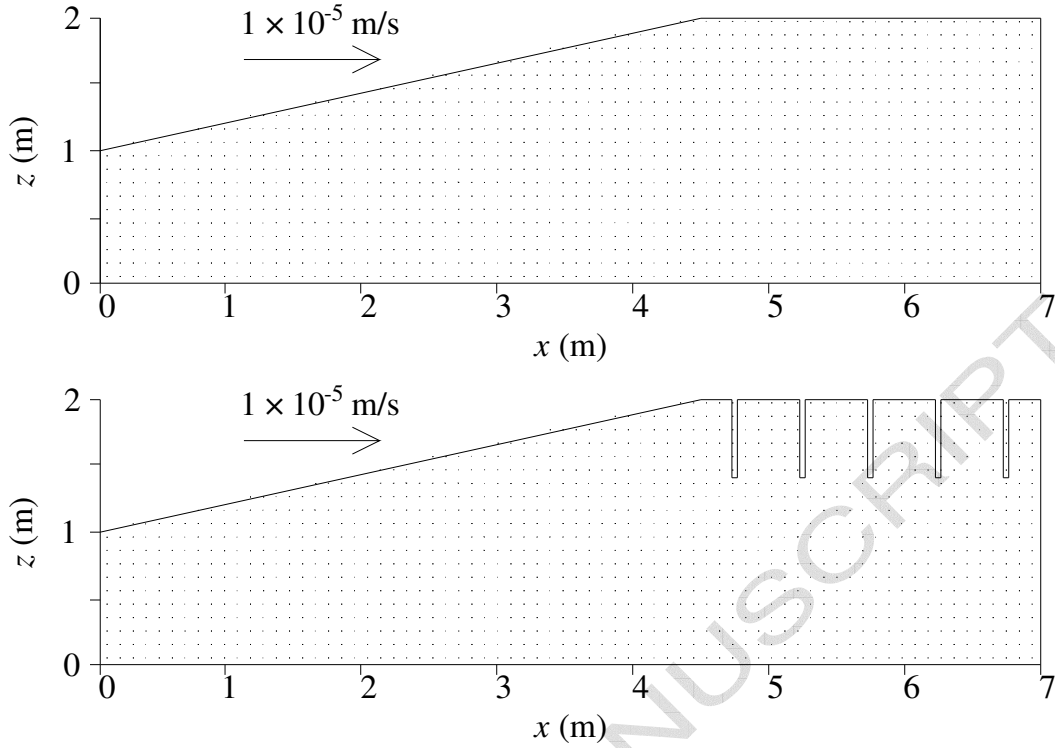
615 Fig. 10. Variations of pore water hydraulic head with time ($K_{upper} = 1.18 \times 10^{-6}$ m/s, $K_{lower} =$
616 1.18×10^{-5} m/s). a) is for the observation point in the upper layer ($x = 4.746$ m, $y =$
617 0.25 m, $z = 1.7$ m); and b) is for the observation point in the lower layer ($x = 4.746$ m,
618 $y = 0.25$ m, $z = 1.1$ m). The period between the two vertical dotted lines represents
619 the emersion period.



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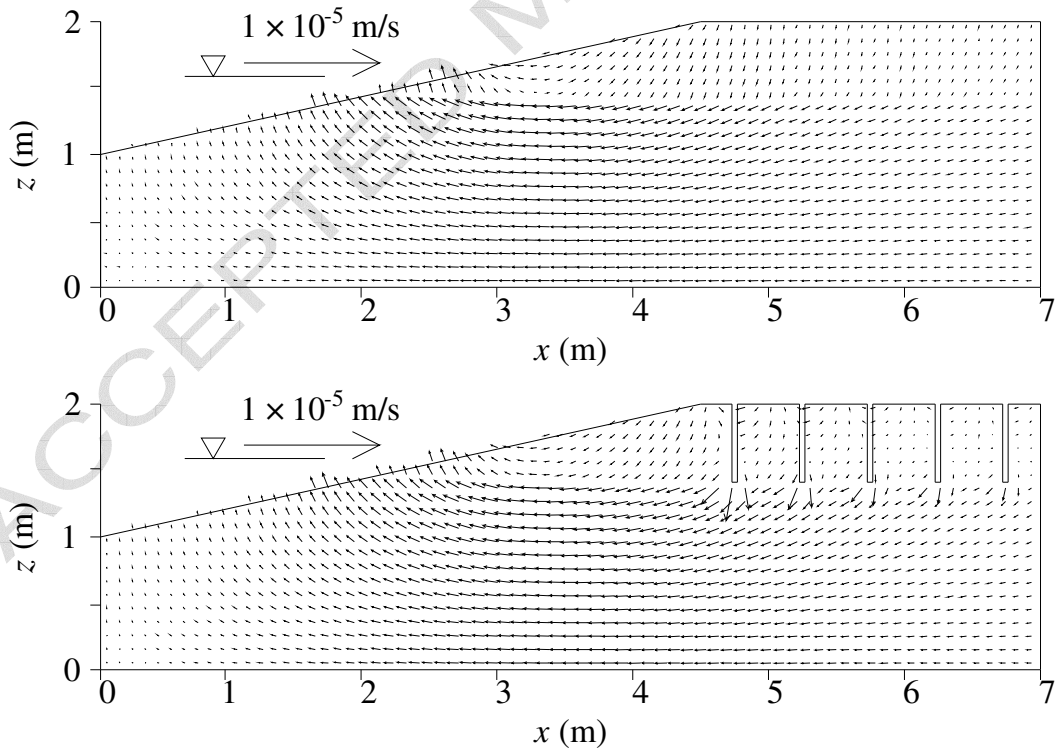
Fig. 1



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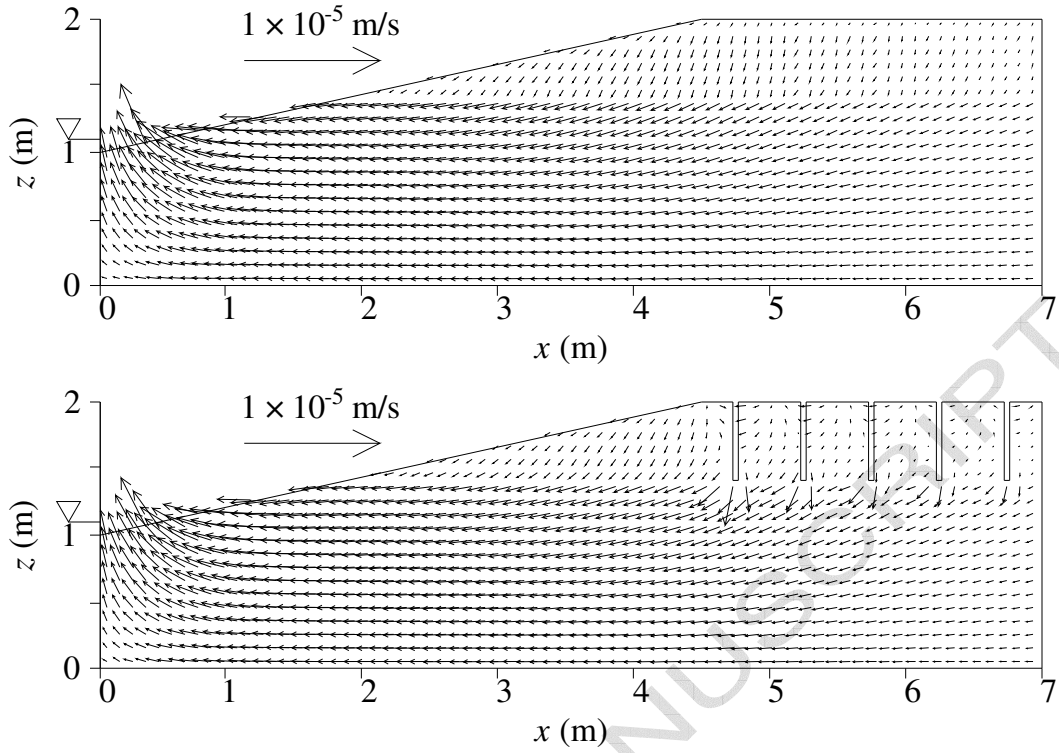
Fig. 2a



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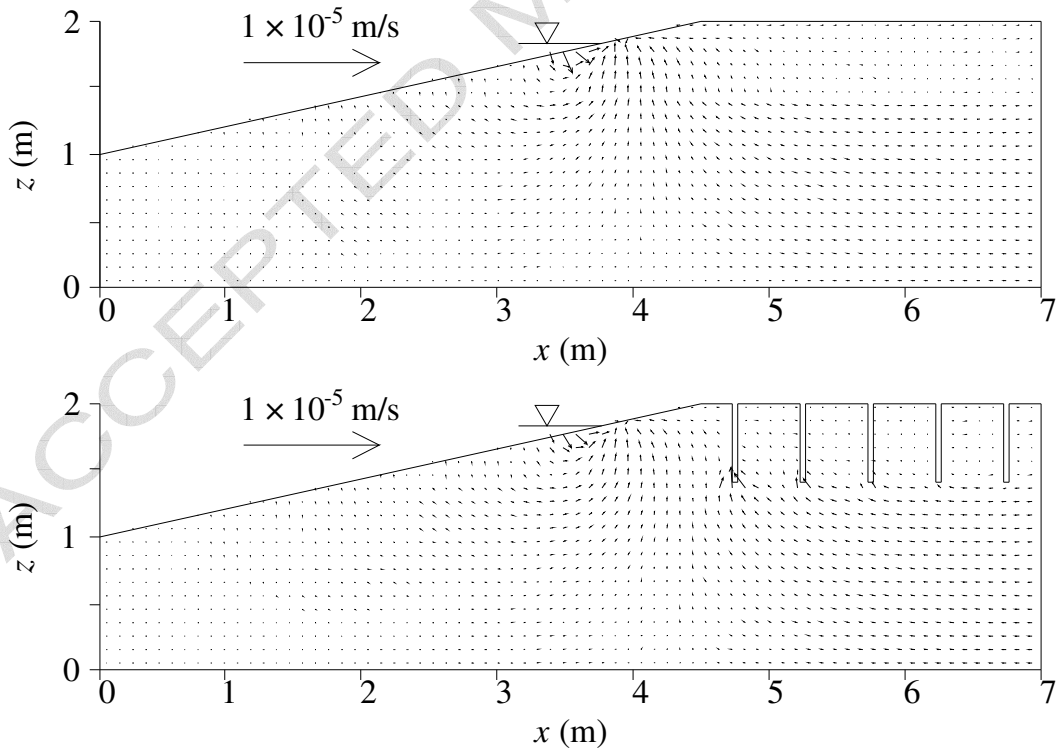
Fig. 2b



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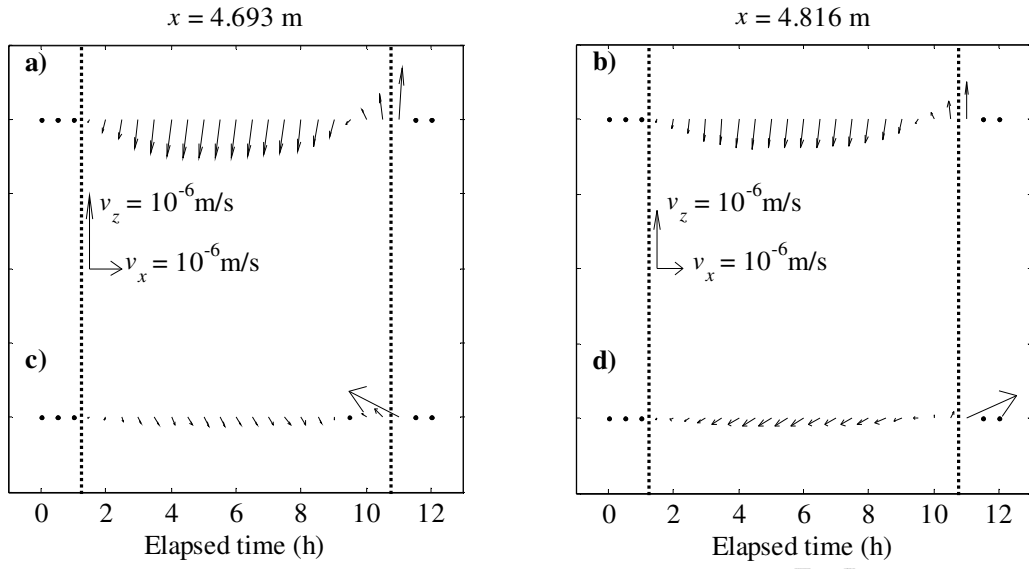
Fig. 2c



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Fig. 2d

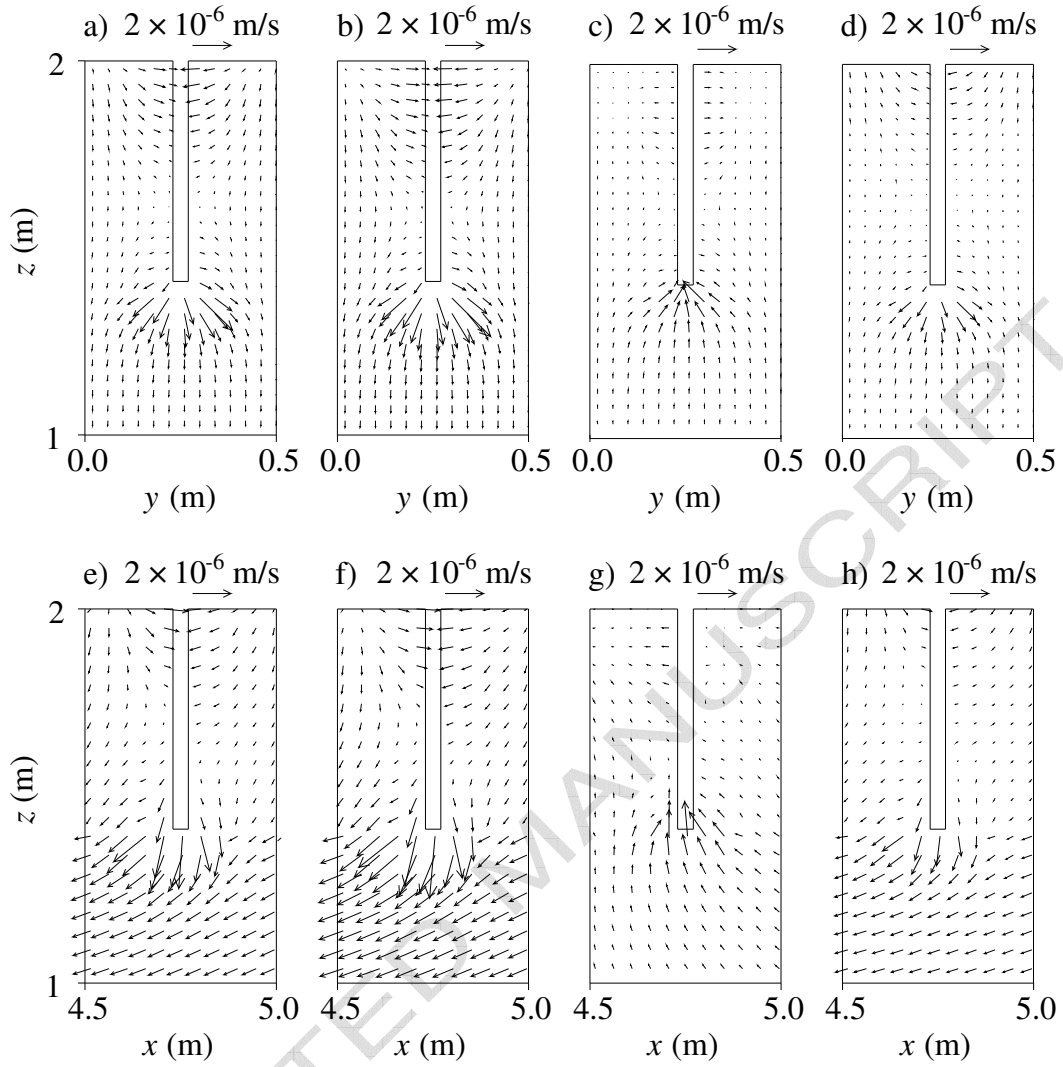


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Fig. 3

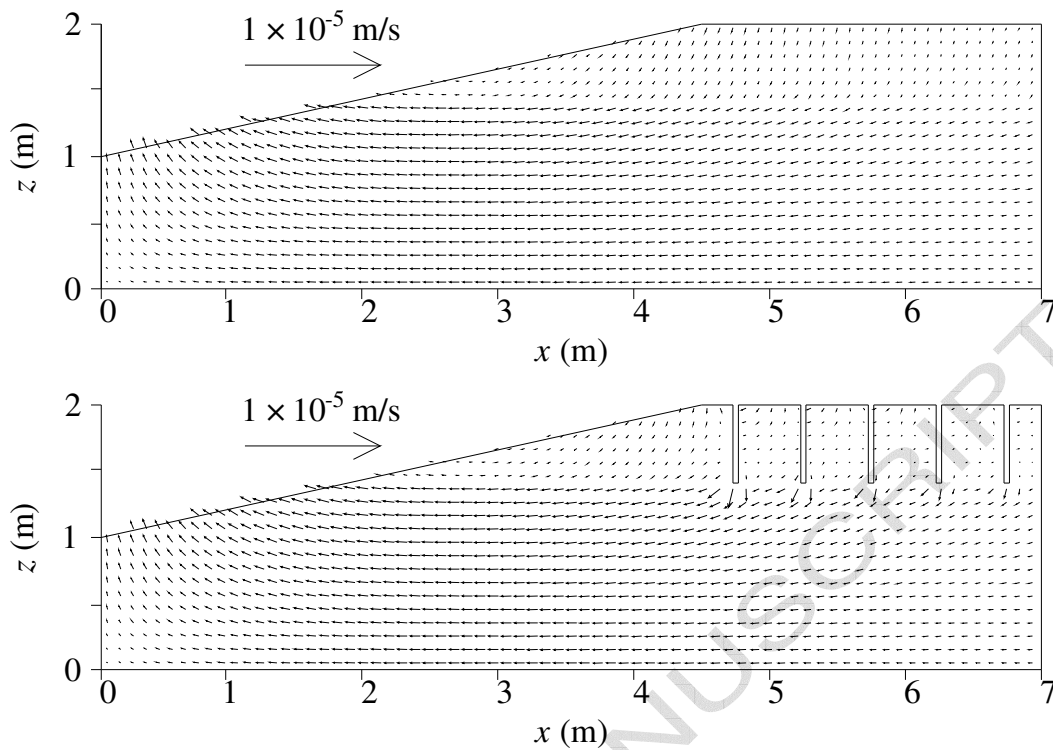
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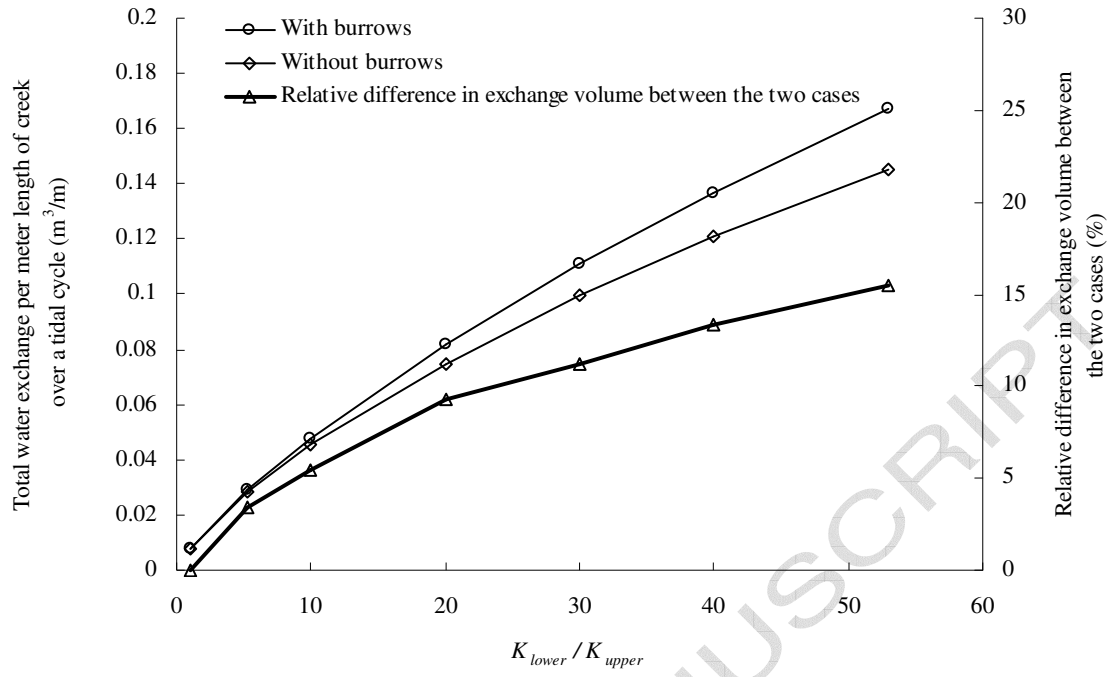
Fig. 4



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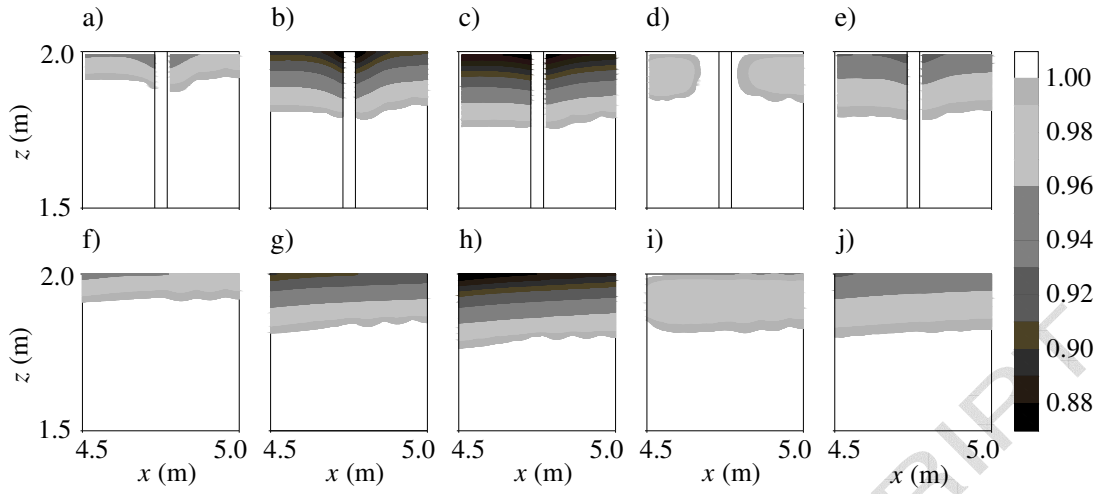
Fig. 5



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Fig. 6



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Fig. 7

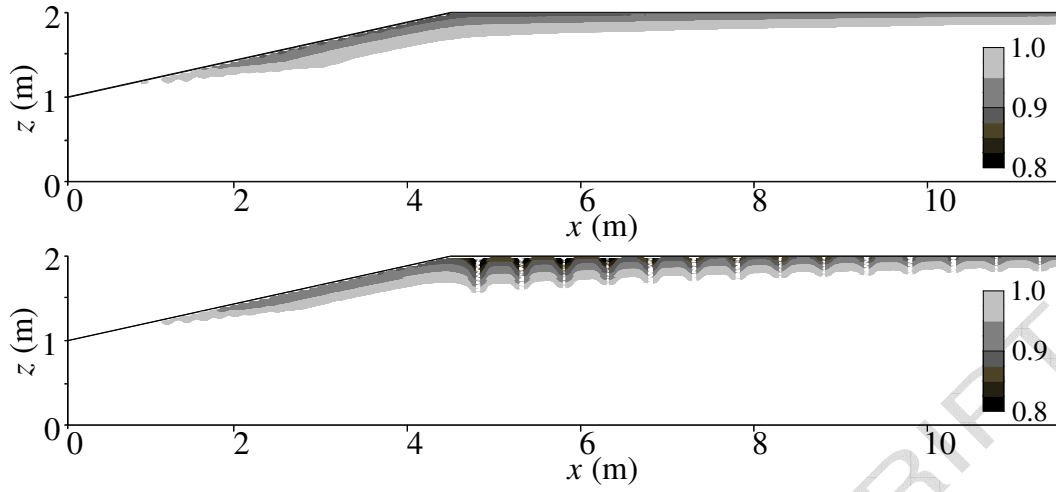
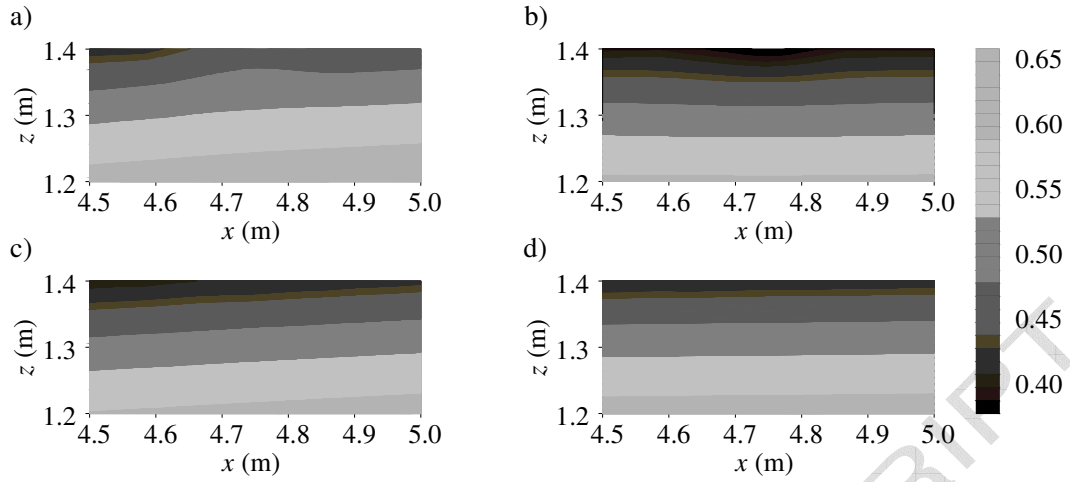


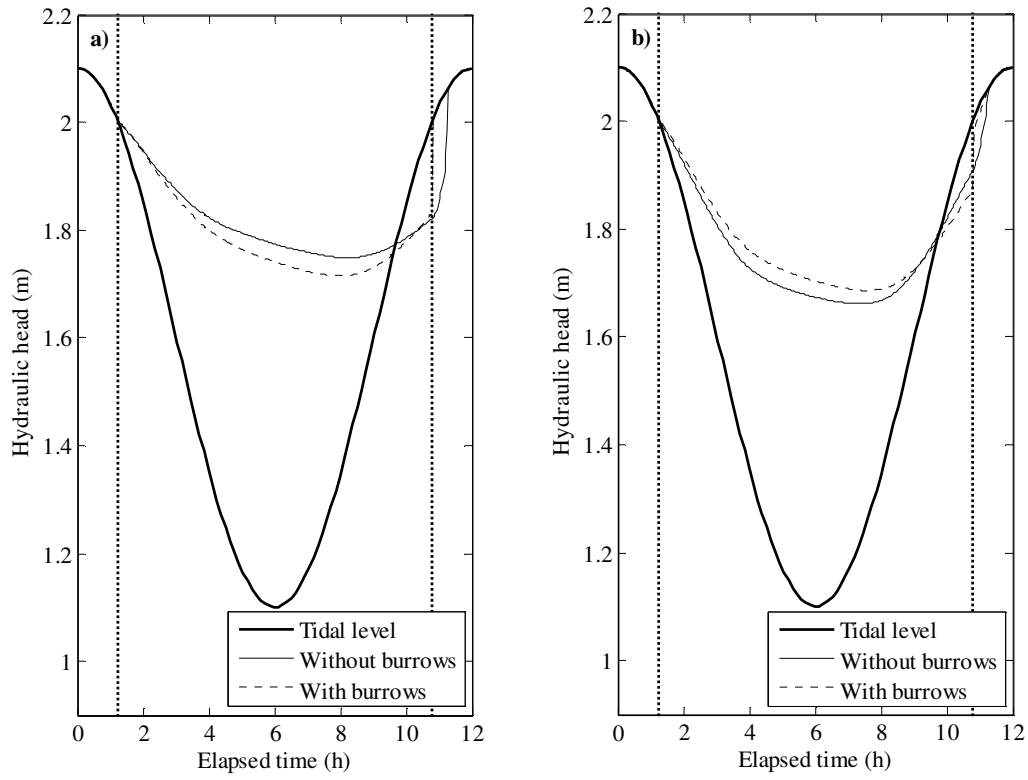
Fig. 8



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Fig. 9



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Fig. 10