

# The new TAE - Alfvén Wave Active Excitation System at JET

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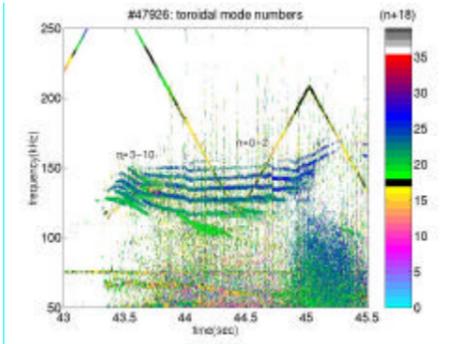
## INTRODUCTION

After many years of successful operation, the JET saddle coil system will be dismantled during the 2004-2005 shutdown. A new antenna system has been designed and is being installed to replace it and excite MHD modes in the Alfvén frequency range (10→500kHz), keeping similar operational capabilities ( $I_{ANT} \sim 30A$ ,  $V_{ANT} \sim 1kV$ , power  $\sim 5kW$ ). The new antenna system comprises two assemblies of four toroidally spaced coils each, situated at opposite toroidal locations, protected by CFC tiles.

### Why Study Alfvén Waves?

### Why Replace the Saddle Coils?

- fusion-born alpha particles ( $\alpha$ 's) resonate with Alfvén Waves (AWs) if  $\omega = k_{||} v_{\alpha}$ ;
- AW spectrum unstable if large-enough free energy in the fast ion pressure gradient;
- an unstable AW spectrum can lead to direct  $\alpha$ 's losses, possibly quenching the ignition process and damaging the first wall;
- due to their geometry, the saddle coils only drive low toroidal mode numbers,  $|n| < 2$ ;
- predictions for ITER: most unstable modes have  $n \sim 5 \rightarrow 20$  (already observed in JET).



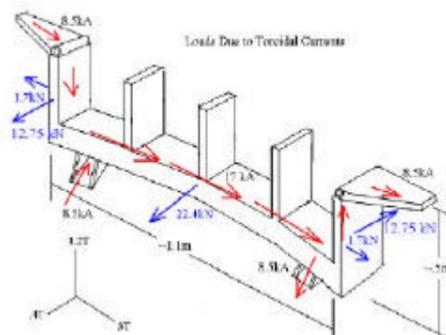
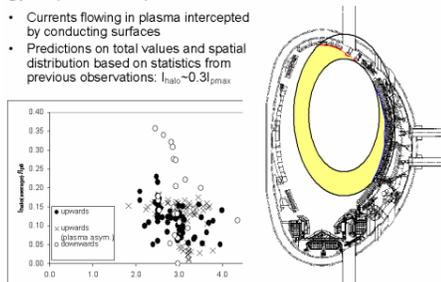
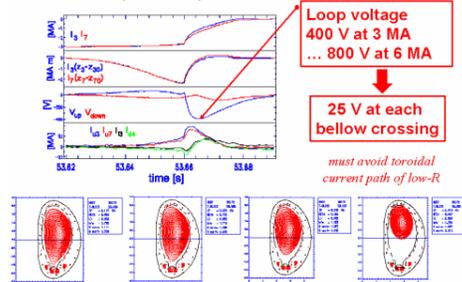
## ENGINEERING CONSTRAINTS AND ANALYSIS

In addition to the constraints imposed by halo current and disruption-induced voltages and currents, the design must comply with the requirements of a remote handling installation:

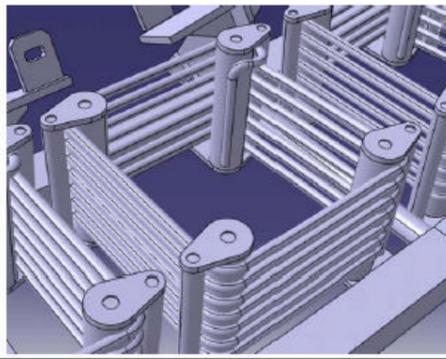
Location	$B_{  }$	$B_{\perp}$	$\partial B_{  }/\partial t$	$\partial B_{\perp}/\partial t$	$\tau_{  }$	$\tau_{\perp}$	$B_{\phi}$	$J_{HALO}$	$\Phi_{HEAT}$
Antennas	1.2T	0.4T	120T/s	80T/s	3ms	5ms	3T	600kA/m <sup>2</sup>	225kW/m <sup>2</sup>

Table 1. Specification for halo currents and magnetic field variations during disruptions.

- total halo current integrated over the antenna surface = 90kA ( $I_{p0}=6MA$ ,  $I_{HALO}/I_{p0}=30\%$ , TPF=1.4);
- loop voltage at disruptions: 800V/6MA,  $\sim 25V$  at each bellow (avoid close toroidal path of low R);
- radiative power up to 150kW/m<sup>2</sup> for >30sec; energy blip at disruptions  $\sim 1MJ/m^2$  over <1ms.



Mechanical loads due to toroidal current flowing in the antenna frame during a typical disruption, balanced up/down with the 3mΩ resistive straps.

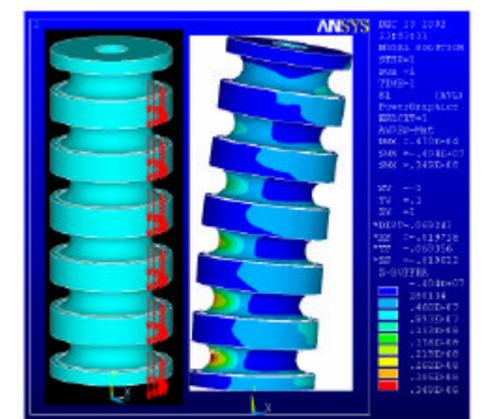


(above) close-up of one 18 turns coil.

Each coil is made using 18 turns of 4mm Inconel 718 wire, covers a toroidal and poloidal extent of  $\sim 25cm$ , and is individually insulated from the supporting frame with Shapal-M spacers. The first turn sits  $\sim 45mm$  behind the poloidal limiters, to achieve good coupling with adequate  $\omega L$ .

The coils are mounted on a 3mm-thick Inconel 625 open structure, to avoid a closed path for disruption-induced currents.

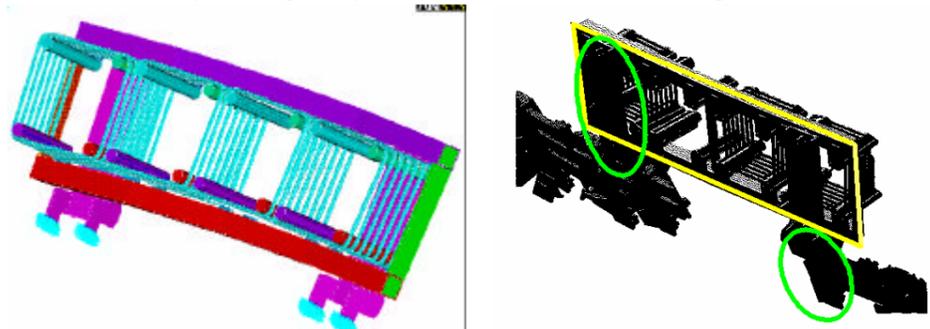
This structure is attached to the poloidal limiters and the remains of the saddle coils via 4 points isolated with Shapal-M spacers, bypassed with 3mΩ resistive straps to provide a reliable current path and optimise the load distribution.



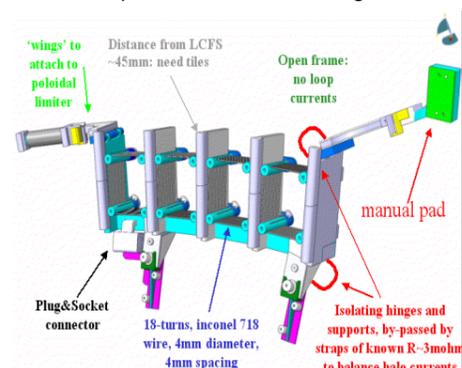
(right) stress deformation of ceramic posts.

## EVOLUTION OF ANTENNA DESIGN

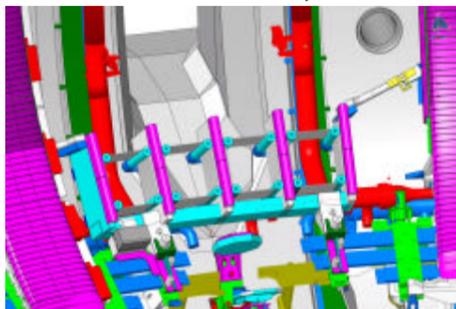
First antenna conceptual design completed in December 2002 based on original total  $I_{HALO} \sim 1kA$ .



- 7turns, 10mm Inconel 718 wire, 200x200x150mm,  $\sim 80-100mm$  from LCFS, no protection tiles;
- Inconel 600 frame, total weight <50kg, simple  $\sim$ one-step RH installation using MASCOT;
- MAIN PROBLEM: CONTINUOUS FRAME:**
  - large induced currents, radial displacement of 1.3cm;
  - some areas at yield, bottom brackets not strong enough;
  - antenna-plasma coupling is marginal.
- ALSO: REVISED DESIGN CONSTRAINTS INCREASING  $I_{HALO}$  TO 90kA FROM  $I_{HALO}=1kA$ :**
  - need limiters, protection tiles, wing supports to poloidal limiter, over MASCOT weight limit;
  - now need to isolate antenna block from vessel, provide link of known resistance;
  - complex RH installation: design of ad-hoc sub-frame, several in-vessel manipulations.

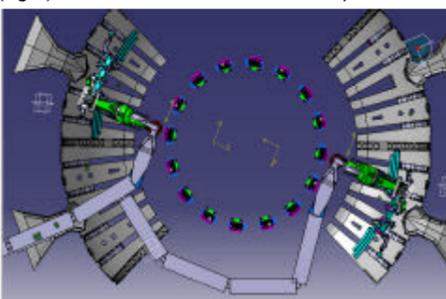


FINAL ANTENNA LAYOUT DESIGN AS COMPLETED IN JUNE 2003

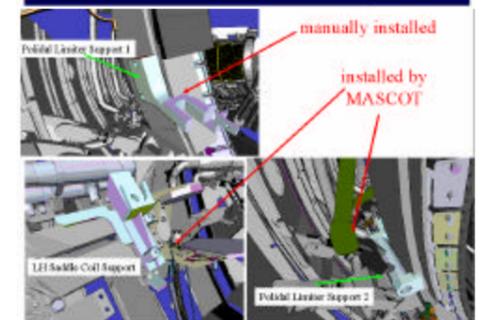


(above) front view of one block of four antennas.

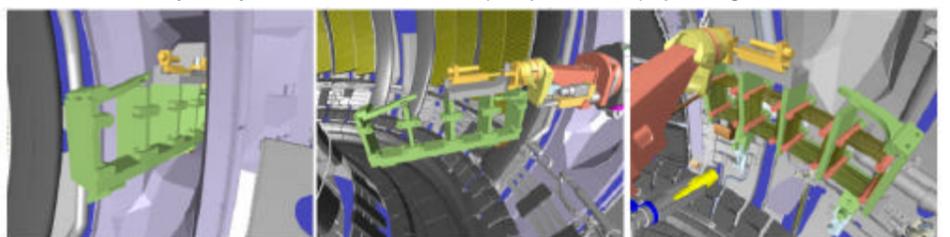
(left) close-up with various engineering details.



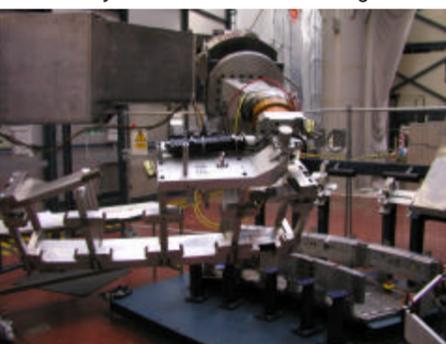
The BOOM is used to position MASCOT inside the vessel and carry heavy loads.



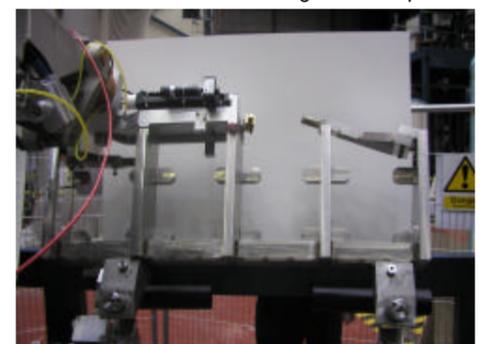
MASCOT is a force reflecting servo-manipulator (computer linked) operating as Master-Slave.



Virtual reality tour of the Remote Handling installation of one set of TAE antennas through Octant 5 port



Trial in-vessel assembly using the RH training facility



Detailed engineering work, the adaptable remote handling JET capability and virtual reality models were used to develop the installation procedure, successfully demonstrated in full mock-up trials. This work was conducted under the European Fusion Development Agreement. D.Testa and A.Fasoli were partly supported by the Fond National Suisse pour la Recherche Scientifique, Grant 620-062924. C.Boswell, J.A.Snipes and P.Titus were partly supported by the US DoE Contract DE-FG02-99ER54563.